

UNCLASSIFIED

APOLLO

GUIDANCE AND NAVIGATION

FOR OFFICIAL USE ONLY

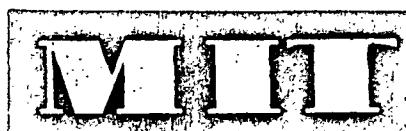
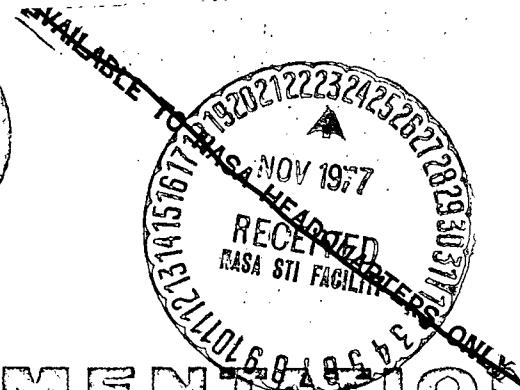
This document has been prepared for Instrumentation Laboratory use and for controlled external distribution. Reproduction or further dissemination is not authorized without express written approval of M.I.T. This document has not been reviewed by the Security Classifications Office, NASA, and therefore, is not for public release.

ACCESSION NUMBER	765 15368	(THRU)
(PAGES)	17	(CODE)
N78-70044		

(E-1388) SUMMARY OF ERROR PROPAGATION IN AN
INERTIAL SYSTEM (Massachusetts Inst. of
Tech.) 17 p

00/12 Unclas

33752



CAMBRIDGE 39, MASSACHUSETTS

INSTRUMENTATION
LABORATORY

UNCLASSIFIED

R87-14347

CASE FILE COPY

MASSACHUSETTS INSTITUTE OF TECHNOLOGY

APOLLO

GUIDANCE AND NAVIGATION

Approved: Milton B. Trageser Date: 8/12/63
Milton B. Trageser, Director
Apollo Guidance and Navigation Program

Approved: Roger B. Woodbury Date: 8/14/63
Roger B. Woodbury, Associate Director
Instrumentation Laboratory

E-1388

SUMMARY OF ERROR
PROPAGATION IN AN INERTIAL
SYSTEM
by
Janusz Sciegienny

August 1963



INSTRUMENTATION
LABORATORY

CAMBRIDGE 39, MASSACHUSETTS

COPY # 628

~~AVAILABLE TO NASA HEADQUARTERS ONLY~~

ACKNOWLEDGMENT

This report was prepared under DSR Project 55-191,
sponsored by the Manned Spacecraft Center of the National
Aeronautics and Space Administration through Contract
NAS 9-153.

The publication of this report does not constitute
approval by the National Aeronautics and Space Administration
of the findings or the conclusions contained therein. It is
published only for the exchange and stimulation of ideas.

E-1388

**SUMMARY OF ERROR PROPAGATION
IN AN INERTIAL SYSTEM**

ABSTRACT

This report contains the summary of analytical studies of error propagation in an inertial system during the orbital and during the suborbital flights. The error is caused by the initial condition errors and accelerometers' bias. The analysis is based on the linearization of the equations of error propagation and the analytical results were confirmed by computer simulation.

The tabulated results may be used to determine the propagation of position and velocity errors in the inertial system (1) with no external corrections during the orbits around a planet, (2) with no external corrections during the suborbital flight above a planet, or (3) with an altimeter during the suborbital flight above a planet.

by Janusz Sciegienny
August, 1963

Page intentionally left blank

Page intentionally left blank

CONTENTS
LIST OF ILLUSTRATIONS

<u>Figure</u>		<u>Page</u>
1	Sign Definition of Accelerometers' Bias During Near Circular Orbit	10
2	Sign Definition of Accelerometers' Bias During Suborbital Flight	11

LIST OF TABLES

<u>Table</u>		<u>Page</u>
I	Planetary Constants.	8
II	Propagation of Initial Condition Errors In Inertial System During Near Circular Orbit	12
III	Propagation of Error Caused by Accelerometers' Bias in Inertial System During Near Circular Orbit	13
IV	Propagation of Initial Condition Errors In Inertial System During Suborbital Flight	14
V	Propagation of Initial Condition Errors In Inertial System with Perfect Altimeter During Suborbital Flight	15
VI	Propagation of Errors Caused by Accelerometers' Bias and Altimeter Bias in Inertial System with Altimeter During Suborbital Flight	16
VII	Propagation of Track Errors in Inertial System	17
REFERENCES		18

Page intentionally left blank

Page intentionally left blank

SUMMARY OF ERROR PROPAGATION IN AN INERTIAL SYSTEM

The derivation of the equations of error propagation in an inertial system is given in References 1, 2, and 3. The analytical results presented in the tables in this report were confirmed by computer simulations. The flight starts at $t = 0$.
The angular orbital frequency is

$$\omega_o = \sqrt{\frac{K}{(R + h)^3}}$$

For $h \ll R$,

$$\omega_o = \sqrt{\frac{K}{R^3}} \left(1 - \frac{3h}{2R}\right)$$

where

K is the product of the universal gravitational constant and the mass of the planet.

R is the mean radius of the planet.

h is the mean vehicle altitude above the surface of the planet.

K, R, and ω_o are tabulated for the Solar System planets, the Sun, and the Moon in Table I.

TABLE I
PLANETARY CONSTANTS

Planet	$K \left[\text{km}^3/\text{sec}^2 \right]$	$R \left[\text{km} \right]$	$\omega_0 \left[\text{rad/sec} \right]$
Mercury	2.164×10^4	2,500	1.77×10^{-3}
Venus	3.243×10^5	6,200	1.167×10^{-3}
Earth	3.98603×10^5	6,371	1.2415×10^{-3}
Mars	4.305×10^5	3,310	1.090×10^{-3}
Jupiter	1.269×10^8	69,880	0.610×10^{-3}
Saturn	3.799×10^7	57,520	0.447×10^{-3}
Uranus	5.812×10^6	25,500	0.592×10^{-3}
Neptune	6.880×10^6	25,000	0.302×10^{-3}
Sun	1.325×10^{11}	696,500	0.6263×10^{-3}
Moon	4.8938×10^3	1,738	0.9655×10^{-3}

During a suborbital flight, the angular velocity of the vehicle with respect to the non-rotating planet is

$$\omega_1 = V/(R + h)$$

where V is the horizontal component of the vehicle velocity.

The errors are defined as the differences between the computed values and the true values. The tabulated errors are the altitude error, the range error, the track error and the velocity errors along the altitude, the range and the track.

The track errors are independent of the altitude and range errors. The effect of altitude error on the error in velocity along range and the range error on the velocity along the altitude are included in the tabulation.

Table II contains the summary of the propagation of initial condition errors in the altitude, the range, the velocity along altitude and the velocity along range in the inertial system during a near circular orbit.

Table III contains the summary of error propagation caused by the accelerometers' bias during a near circular orbit. The accelerometers are oriented either along the altitude and range or remain fixed in the inertial space with angle ϕ from the local vertical at time $t = 0$. The positive sense of direction of the accelerometers' bias is shown in Figure 1.

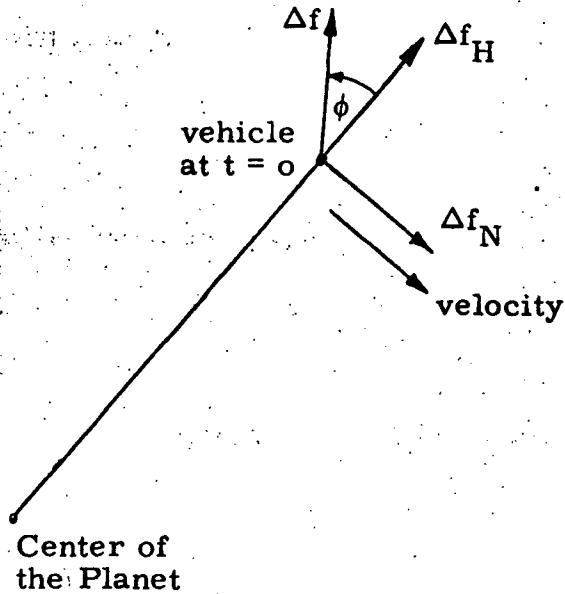


Fig. 1 Sign Definition of Accelerometers' Bias During Near Circular Orbit

Table IV contains the summary of the propagation of initial condition errors in the altitude, the range, the velocity along altitude and the velocity along range in the inertial system, with no external corrections, during a suborbital flight.

Table V contains the summary of the propagation of initial condition errors, during a suborbital flight, in a system consisting of an inertial system and a perfect altimeter. The altimeter is used to compute the precise magnitude of the distance from the center of the planet to the vehicle, $R + h$. This distance is used to compute the components of the gravitational acceleration acting on the vehicle.

Table VI contains the summary of the error propagation in the altitude, the range, the velocity along altitude and the velocity along the range, during a suborbital flight, in a system consisting of an inertial system and an altimeter. The errors are caused by the bias in the accelerometers fixed in inertial space (Fig. 2) and by the altimeter bias.

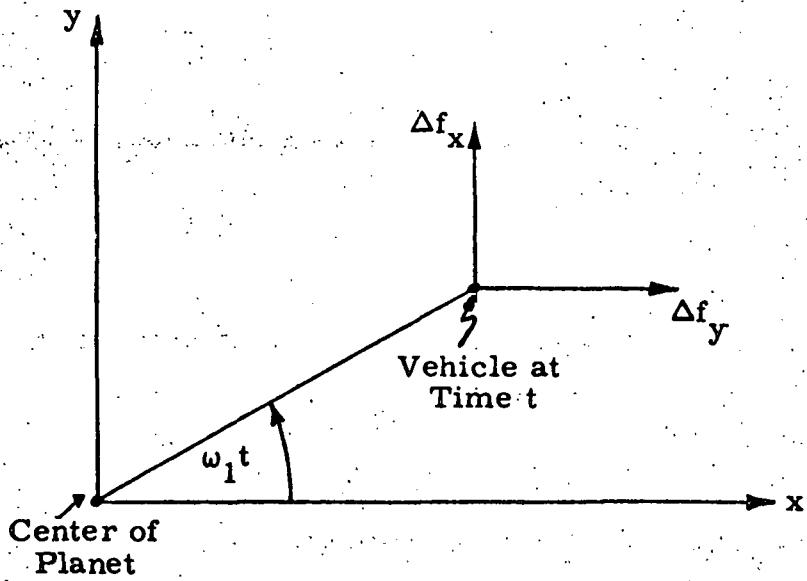


Fig. 2 Sign Definition of Accelerometers' Bias During Suborbital Flight

Table VII contains the summary of error propagation in the track and in the velocity along the track in an inertial system during the orbital or during the suborbital flights. The errors are caused by the initial condition errors in the track, the velocity along the track and by the accelerometer bias along the track direction. The track errors are independent of the altitude and the range errors.

TABLE II
PROPAGATION OF INITIAL CONDITION ERRORS IN INERTIAL
SYSTEM DURING NEAR CIRCULAR ORBIT

INITIAL CONDITION ERROR IN			
ALTITUDE ΔR_H	RANGE ΔR_N	VELOCITY ALONG ALTITUDE ΔV_H	VELOCITY ALONG RANGE ΔV_N
$R_{HE}(t)$	$\Delta R_H(2-\cos\omega_0 t)$	$\Delta R_N \sin\omega_0 t$	$\frac{2\Delta V_N}{\omega_0} (1-\cos\omega_0 t)$
RANGE $R_{NE}(t)$	$\Delta R_H(2\sin\omega_0 t - 3\omega_0^2 t)$	$\Delta R_N(2\cos\omega_0 t - 1)$	$\frac{\Delta V_N(4\sin\omega_0 t - 3\omega_0^2 t)}{\omega_0}$
VELOCITY ALONG ALTITUDE $V_{HE}(t)$	$\Delta R_H \omega_0(3\omega_0^2 t - \sin\omega_0 t)$	$\Delta R_N \omega_0(1-\cos\omega_0 t)$	$\Delta V_N(2-\cos\omega_0 t)$
VELOCITY ALONG RANGE $V_{NE}(t)$	$\Delta R_H \omega_0(\cos\omega_0 t - 1)$	$-\Delta R_N \omega_0 \sin\omega_0 t$	$\Delta V_N(2\cos\omega_0 t - 1)$

ω_0 [rad/sec] $\approx 0.966 \times 10^{-3}$ on lunar surface
 $\approx 1.242 \times 10^{-3}$ on earth surface

TABLE III
PROPAGATION OF ERROR CAUSED BY ACCELEROMETERS' BIAS IN
INERTIAL SYSTEM DURING NEAR CIRCULAR ORBIT

ACCELEROMETERS ORIENTED ALONG ALTITUDE		ACCELEROMETERS BIAS		ACCELEROMETER FIXED IN INERTIAL SPACE AT ANGLE Φ FROM LOCAL VERTICAL AT $t=0$
Δf_H	Δf_N	RANGE	FROM LOCAL VERTICAL AT $t=0$	
$\frac{\Delta f_H}{\omega_0^2} (1 - \cos \omega_0 t)$	$\frac{2\Delta f_N}{\omega_0^2} (\omega_0 t - \sin \omega_0 t)$		$\frac{\Delta f}{\omega_0^2} \left[\frac{3}{2} \omega_0 t \sin \omega_0 t + 2(\cos \omega_0 t - 1) \right] \cos \Phi$ $+ \frac{3}{2} [\omega_0 \cos \omega_0 t - \sin \omega_0 t] \sin \Phi$	
$\frac{2\Delta f_H}{\omega_0^2} (\sin \omega_0 t - \omega_0 t)$	$\frac{\Delta f_N}{\omega_0^2} \left[4(1 - \cos \omega_0 t) - \frac{3}{2} \omega_0^2 t^2 \right]$		$\frac{\Delta f}{\omega_0^2} \left[3 \left[\omega_0 t (1 + \cos \omega_0 t) - 2 \sin \omega_0 t \right] \cos \Phi$ $- 3 \omega_0 t \sin \omega_0 t + 5(\cos \omega_0 t - 1) \sin \Phi \right]$	
$\frac{\Delta f_H}{\omega_0} (2\omega_0 t - \sin \omega_0 t)$	$3\Delta f_N \left(\frac{\omega_0^2 t^2}{2} - 1 + \cos \omega_0 t \right)$	VELOCITY ALONG ALTITUDE	$\frac{\Delta f}{\omega_0} \left\{ \left[-\frac{3}{2} \omega_0 t (2 + \cos \omega_0 t) + \frac{11}{2} \sin \omega_0 t \right] \cos \Phi$ $+ \frac{3}{2} [\omega_0 t \sin \omega_0 t - 5(1 - \cos \omega_0 t)] \sin \Phi \right\}$	
$\frac{\Delta f_H}{\omega_0} (\cos \omega_0 t - 1)$	$\frac{\Delta f_N}{\omega_0} (2 \sin \omega_0 t - \omega_0 t)$	VELOCITY ALONG RANGE	$\frac{\Delta f}{\omega_0} \left\{ \left[\frac{3}{2} \omega_0 t \sin \omega_0 t + 1 - \cos \omega_0 t \right] \cos \Phi$ $+ \frac{1}{2} [-3\omega_0 t \cos \omega_0 t + \sin \omega_0 t] \sin \Phi \right\}$	

$$\omega_0 [\text{rad/sec}] \approx 0.966 \times 10^{-3} \text{ on lunar surface}$$

$$\approx 1.242 \times 10^{-3} \text{ on earth surface}$$

TABLE IV

PROPAGATION OF INITIAL CONDITION ERRORS IN INERTIAL SYSTEM
DURING SUBORBITAL FLIGHT

INITIAL CONDITION ERROR IN			
ALTITUDE, ΔR_H	RANGE, ΔR_N	VELOCITY ALONG ALTITUDE, ΔV_H	VELOCITY ALONG RANGE, ΔV_N
$\Delta R_H \cos(\sqrt{2}\omega_0 t) \cos\omega_1^t$	$\Delta R_N \cos\omega_0 t \sin\omega_1^t$	$\frac{\Delta V_H}{\sqrt{2}\omega_0} \sinh(\sqrt{2}\omega_0 t) \cos\omega_1^t$	$\frac{\Delta V_N}{\omega_0} \sin\omega_0 t \sin\omega_1^t$
$\Delta R_H \cos(\sqrt{2}\omega_0 t) \sin\omega_1^t$	$\Delta R_N \cos\omega_0 t \cos\omega_1^t$	$-\frac{\Delta V_H}{\sqrt{2}\omega_0} \sinh(\sqrt{2}\omega_0 t) \sin\omega_1^t$	$\frac{\Delta V_N}{\omega_0} \sin\omega_0 t \cos\omega_1^t$
$\Delta R_H \sqrt{2}\omega_0 \sin(\sqrt{2}\omega_0 t) \cos\omega_1^t$	$\Delta R_N \omega_0 \sin\omega_0 t \sin\omega_1^t$	$\Delta V_H \cosh(\sqrt{2}\omega_0 t) \cos\omega_1^t$	$\Delta V_N \cos\omega_0 t \sin\omega_1^t$
$\Delta R_H \sqrt{2}\omega_0 \sin(\sqrt{2}\omega_0 t) \sin\omega_1^t$	$-\Delta R_N \omega_0 \sin\omega_0 t \cos\omega_1^t$	$-\Delta V_H \cosh(\sqrt{2}\omega_0 t) \sin\omega_1^t$	$\Delta V_N \cos\omega_0 t \cos\omega_1^t$
VELOCITY ALONG ALTITUDE $V_{HE}(1)$	VELOCITY ALONG RANGE $V_{NE}(1)$		

$$\omega_0 [\text{rad/sec}] \approx 0.966 \times 10^{-3} \text{ on lunar surface}$$

$$\approx 1.242 \times 10^{-3} \text{ on earth surface}$$

$$\omega_1 = V/R [\text{rad/sec}]$$

$$R [km] \approx 1738 \text{ (Moon)}$$

$$\approx 6371 \text{ (Earth)}$$

V = average horizontal velocity

TABLE V
PROPAGATION OF INITIAL CONDITION ERRORS IN INERTIAL
SYSTEM WITH PERFECT ALTIMETER DURING SUBORBITAL FLIGHT

INITIAL CONDITION ERRORS IN			
ALTITUDE ΔR_H	RANGE ΔR_N	VELOCITY ALONG ALTITUDE ΔV_H	VELOCITY ALONG RANGE ΔV_N
$\Delta R_H \cos \omega_0 t \cos \omega_1 t$	$\Delta R_N \cos \omega_0 t \sin \omega_1 t$	$\frac{\Delta V_H}{\omega_0} \sin \omega_0 t \cos \omega_1 t$	$\frac{\Delta V_N}{\omega_0} \sin \omega_0 t \sin \omega_1 t$
$-\Delta R_H \cos \omega_0 t \sin \omega_1 t$	$\Delta R_N \cos \omega_0 t \cos \omega_1 t$	$-\frac{\Delta V_H}{\omega_0} \sin \omega_0 t \sin \omega_1 t$	$\frac{\Delta V_N}{\omega_0} \sin \omega_0 t \cos \omega_1 t$
$\Delta V_H \cos \omega_0 t \cos \omega_1 t$	$-\Delta R_N \sin \omega_0 t \sin \omega_1 t$	$\Delta V_H \cos \omega_0 t \cos \omega_1 t$	$\Delta V_N \cos \omega_0 t \sin \omega_1 t$
$-\Delta V_H \sin \omega_0 t \sin \omega_1 t$	$\Delta R_N \sin \omega_0 t \cos \omega_1 t$	$-\Delta V_H \cos \omega_0 t \sin \omega_1 t$	$\Delta V_N \cos \omega_0 t \cos \omega_1 t$
$\Delta V_N \cos \omega_0 t \sin \omega_1 t$	$-\Delta R_N \omega_0 \sin \omega_0 t \sin \omega_1 t$	$\Delta V_N \cos \omega_0 t \cos \omega_1 t$	$\Delta V_N \cos \omega_0 t \cos \omega_1 t$
$-\Delta V_N \sin \omega_0 t \cos \omega_1 t$	$\Delta R_N \omega_0 \sin \omega_0 t \cos \omega_1 t$	$-\Delta V_N \omega_0 \sin \omega_0 t \sin \omega_1 t$	$\Delta V_N \cos \omega_0 t \cos \omega_1 t$

$$\begin{aligned}\omega_0 [\text{rad/sec}] &\approx 0.966 \times 10^{-3} \text{ on lunar surface} \\ &\approx 1.242 \times 10^{-3} \text{ on earth surface}\end{aligned}$$

$$\begin{aligned}\omega_1 &= V/R [\text{rad/sec}] \\ R [\text{km}] &\approx 1738 \text{ (Moon)} \\ &\approx 6371 \text{ (Earth)}\end{aligned}$$

V = average horizontal velocity

TABLE VI

PROPAGATION OF ERRORS CAUSED BY ACCELEROMETERS' BIAS AND ALTIMETER
 BIAS IN INERTIAL SYSTEM WITH ALTIMETER DURING SUBORBITAL FLIGHT
 (X-Y AXIS SYSTEM FIXED IN INERTIAL SPACE WITH X-AXIS
 ALONG ALTITUDE AND Y-AXIS ALONG RANGE AT t=0)

SOURCE OF ERROR		ALTIMETER BIAS	
	X-AXIS Δf_x	Y-AXIS Δf_y	ΔR
ALTITUDE $R_{HE}(t)$	$\frac{\Delta f_x}{\omega_0^2} (1 - \cos \omega_0 t) \sin \omega_0 t$	$\frac{\Delta f_y}{\omega_0^2} (1 - \cos \omega_0 t) \sin \omega_0 t$	$\frac{3\Delta R}{1 - (\omega_1/\omega_0)^2} \left[-\frac{\omega_1}{\omega_0} \sin \omega_0 t \sin \omega_1 t - \cos \omega_0 t \cos \omega_1 t \right]$
RANGE $R_{NE}(t)$	$-\frac{\Delta f_x}{\omega_0^2} (1 - \cos \omega_0 t) \sin \omega_0 t$	$\frac{\Delta f_y}{\omega_0^2} (1 - \cos \omega_0 t) \cos \omega_0 t$	$\frac{3\Delta R}{1 - (\omega_1/\omega_0)^2} \left[\cos \omega_0 t \sin \omega_1 t - \frac{\omega_1}{\omega_0} \sin \omega_0 t \cos \omega_1 t \right]$
VELOCITY ALONG ALTITUDE $V_{HE}(t)$	$\frac{\Delta f_x}{\omega_0} \sin \omega_0 t \cos \omega_0 t$	$\frac{\Delta f_y}{\omega_0} \sin \omega_0 t \sin \omega_0 t$	$\frac{3\Delta R}{1 - (\omega_1/\omega_0)^2} \left[\omega_1 \cos \omega_0 t \sin \omega_1 t + \omega_0 \sin \omega_0 t \cos \omega_1 t \right]$
VELOCITY ALONG RANGE $V_{NE}(t)$	$-\frac{\Delta f_x}{\omega_0} \sin \omega_0 t \sin \omega_0 t$	$\frac{\Delta f_y}{\omega_0} \sin \omega_0 t \cos \omega_0 t$	$\frac{3\Delta R}{1 - (\omega_1/\omega_0)^2} \left[\omega_0 \sin \omega_0 t \sin \omega_1 t + \omega_1 \cos \omega_0 t \cos \omega_1 t \right]$

$$\omega_0 \left[\text{rad/sec} \right] \approx 0.966 \times 10^{-3} \text{ on lunar surface}$$

$$\omega_1 = V/R \left[\text{rad/sec} \right]$$

V = average horizontal velocity

$$R[\text{km}] \approx 1738 \text{ (Moon)}$$

$$R[\text{km}] \approx 6371 \text{ (Earth)}$$

TABLE VII
PROPAGATION OF TRACK ERRORS IN INERTIAL SYSTEM

INITIAL CONDITION ERROR IN		ACCELEROMETER
TRACK	ΔR_M	BIAS ALONG TRACK Δf_M
TRACK	$\Delta R_M \cos \omega_0 t$	$\frac{\Delta f_M}{\omega_0^2} (1 - \cos \omega_0 t)$
$R_{ME}(t)$	$\frac{\Delta v_M}{\omega_0} \sin \omega_0 t$	$\frac{\Delta f_M}{\omega_0} \sin \omega_0 t$
VELOCITY ALONG TRACK $v_{ME}(t)$	$-\Delta R_M \omega_0 \sin \omega_0 t$	$\frac{\Delta f_M}{\omega_0} \sin \omega_0 t$

ω_0 [rad/sec] $\approx 0.966 \times 10^{-3}$ on lunar surface
 $\approx 1.242 \times 10^{-3}$ on earth surface

REFERENCES

1. Pace Advanced Inertial Guidance System, Technical Report R-278, Section III, 3.2.3.A, MIT-IL, June 24, 1959 -- February 24, 1960.
2. Pace Advanced Inertial Guidance System, Technical Report R-329, Section II A, MIT-IL, October 24, 1960 -- February 24, 1961.
3. Pace Advanced Inertial Guidance System, Final Engineering Report, Technical Report R-371, Vol. I, Appendix B, MIT-IL, March 1963.

E-1388

DISTRIBUTION LIST

Internal

J. Arnow (Lincoln)
R. Battin
P. Bryant
E. Coppers
J. Dahlen
J. Flanders
E. Frey
F. Grant
D. Hanley
W. Heintz
D. Hoag
A. Hopkins
F. Houston
J. Hursh
M. Johnston
B. Katz
A. Koso
D. Lickly
R. Magee
W. Markey
J. McNeil

James Miller
John Miller
J. Nevins
J. Nugent
E. Olsson
C. Parker
N. Polner
J. Potter
R. Scholten
J. Sciegienny
N. Sears
B. Smith
E. Stirling
W. Tanner
R. Therrien
L. Wilk
R. Woodbury
W. Wrigley
Apollo Library (2)
MIT/IL Library (6)

External

(ref. APCAN; 2 July 1963)

P. Ebersole (NASA/MSC) (2)

W. Rhine (NASA/RASPO) (1)

S. Gregorek (NAA S & ID/MIT) (1)

AC Spark Plug (10)

Kollsman (10)

Raytheon (10)

WESCO (2)

Capt. W. Delaney (AFSC/MIT) (1)

NAA RASPO: National Aeronautics and Space Administration (1)
Resident Apollo Spacecraft Project Officer
North American, Inc.
Space and Information Systems Division
12214 Lakewood Boulevard
Downey, California

CAPE: National Aeronautics and Space Administration (3)
Atlantic Missile Range Operations
Port Canaveral, Florida
Attn: Mr. B. P. Brown

HDQ: NASA Headquarters (6)
1520 H Street
Washington, D. C.
Attn: Mr. G. M. Low, MD(P)

AMES: National Aeronautics and Space Administration (2)
Ames Research Center
Moffett Field, California
Attn: Mr. Matthews

LEWIS: National Aeronautics and Space Administration (2)
Lewis Research Center
Cleveland, Ohio

FRC: National Aeronautics and Space Administration (2)
Flight Research Center
Edwards AFB, California

JPL: National Aeronautics and Space Administration (2)
Jet Propulsion Laboratory
Pasadena, California
Attn: Mr. H. R. Lawrence

LRG: National Aeronautics and Space Administration (2)
Langley Research Center
Langley AFB, Virginia
Attn: Mr. A. T. Mattson

GSFC: National Aeronautics and Space Administration (2)
Goddard Space Flight Center
Greenbelt, Maryland

MSFC: National Aeronautics and Space Administration (2)
George C. Marshall Space Flight Center
Huntsville, Alabama
Attn: Dr. Kuettner

GAEC: Grumman Aircraft Engineering Corporation (1)
Bethpage, Long Island
New York
Attn: Mr. A. Whitaker

NAA: North American Aviation, Inc. (1)
Space and Information Systems Division
12214 Lakewood Boulevard
Downey, California
Attn: Mr. R. Berry

GAEC RASPO: National Aeronautics and Space Administration (1)
Resident Apollo Spacecraft Project Officer
Grumman Aircraft Engineering Corporation
Bethpage, L. I., New York
Attn: Mr. Jack Small

WSMR: National Aeronautics and Space Administration (2)
Post Office Drawer D
White Sands Missile Range
White Sands, New Mexico

MSC: National Aeronautics and Space Administration (45)
Manned Spacecraft Center
Apollo Document Control Group (SDG)
Houston 1, Texas

UNCLASSIFIED

UNCLASSIFIED