



Mission Planning and Analysis Division
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
MANNED SPACECRAFT CENTER
HOUSTON, TEXAS 77058

IN REPLY REFER TO: 70-FM/7-243

MEMORANDUM TO: See list below

FROM : FM/Assistant Chief, Mathematical Physics Branch
SUBJECT : Modifications to the RTUC offline star-horizon observation processor for Apollo 14

1. Reference: MSC Internal Note 69-FM-326, "RTUC Offline Requirements for H-2: Star-Horizon Observation Processor," by Paul Plantagen, MTP, and Robert Kidd, TRW Systems Group, February 24, 1970.
2. The modifications to the RTUC offline star-horizon observation processor for Apollo 14 are of two types. The first is the inclusion of additional quantities which will aid in the analysis of the sightings. In addition to calculating new quantities, a statistical summary of several parameters for each star is required. The second modification is to change the computer format so that the desired information is more readily available.

Emil R. Schiesser

The Flight Software Branch concurs with the above recommendation and requests IBM to proceed accordingly.

James C. Stokes, Jr., Chief
Flight Software Branch

APPROVED BY:

John P. Mayer
Chief, Mission Planning
and Analysis Division

Enclosure
Addressee: (See attached list)
FM:RTS/evly:rmr

RELEASE APPROVAL

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Change sheet to Internal Note

2. Identification 69-7M-326 dated

February 26, 1970

Page 1 of 1 Pages

TO:

3. FROM:

Division Mission Planning and Analysis

Branch Mathematical Physics

Section

4. Title or Subject

HSC OFFLINE REQUIREMENTS FOR S-2:
STAR-SHIFTON OBSERVATION PROCEDURE

Date of Paper

October 6, 1970

5. Author(s)

Paul Flanagan, MFS, and Robert Kidd, TSW Systems Group
Change 1 by Ronnie R. Leulier, MSC, and Sam Crigler, TSW

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CHANGE SHEET

FOR

MSC INTERNAL NOTE 69-PM-326 DATED FEBRUARY 24, 1970

STOC OFFLINE REQUIREMENTS FOR S-2:
STAR-HORIZON OBSERVATION PROCESSOR

By Paul Flanagan, MFB, and
Robert Kidd, TRW Systems Group

Change 1

By Ronnie R. Lanier, MSC, and
Sam Crigler, TRW

October 8, 1970


James C. McPherson, Chief
Mathematical Physics Branch


John P. Meyer, Chief
Mission Planning and Analysis Division

Page 1 of 13
(with enclosures)

NOTE: A black bar in the margin indicates the area of change.

After the attached enclosures, which are replacement pages, have been inserted, place this CHANGE SHEET between the cover and title page and write on the cover, "CHANGE 1 inserted".

1. Replace pages 13, 14, 21, and 22.

CHANGE HISTORY FOR 69-FM-326

Number	Date	Description
1		<p>Replace pages 13, 14: Eliminated some original parameters and added some new parameters. Expanded original pages to include additional discussion.</p> <p>Replace pages 21, 22: Flow charts added to define new computation logic for parameters mentioned above.</p>

A priori b_{T0} (MRD), b_0 (KM)
 a_{bT0} (MRD), a_{b0} (KM), ρ_0 (correlation coefficient)

For each iteration:

Solution b_T (MRD), b (KM)
 a_{bT} (MRD), a_b (KM), ρ (correlation coefficient)

Iteration number, N

For each observation processed by method 2, five additional quantities will be computed to isolate sources of sighting errors and to evaluate the sighting.

SPOV (DEG)

NROT (DEG)

PLANE ERROR (DEG)

POINT ERROR (MINUTES OF ARC)

TERM ANG (DEG)

These variables are illustrated in the two figures on the following page.

Equations required to define this output are as follows. The star field-of-view error is given by

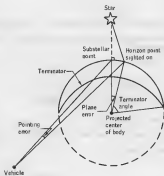
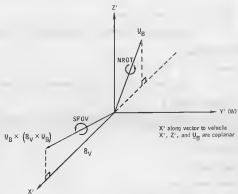
$$\text{SPOV} = \sin^{-1}(\underline{u} \cdot \underline{U}_D)$$

The normal rotation error is given by

$$\text{NROT} = \sin^{-1} \left\{ \underline{u} \cdot [\underline{U}_D \times \text{unit}(\underline{E}_V \times \underline{U}_D)] \right\}$$

The measurement plane error is given by

$$\begin{aligned} \text{PLANE ERROR} = \sin^{-1} \left\{ R_v \left[\cos(\text{SPOV}) \sin(\text{SPOV}) \cos^2(\text{NROT})(1 - \cos \tau_r) \right. \right. \\ \left. \left. - \sin(\text{NROT}) \sin \tau_r \right] \right\} \end{aligned}$$



The pointing error is given by

$$\text{POINT ERROR} = 2 \sin^{-1} [1/R_v \sin \{\text{PLANE ERROR}/2\}]$$

The determination of the terminator angle requires a series of calculations as follows.

$$\underline{L} = \underline{R}(U_{sp})$$

where U_{sp} is the vector from the planet to the sun.

$$\underline{R} = \underline{R}(R_v)$$

$$\underline{R} = \left(\frac{L_x}{L_x R_x - L_x R_z}, \frac{L_x}{L_y R_z - L_x R_y}, \frac{L_x}{L_z R_y - L_y R_z} - \frac{L_x}{L_x R_x - L_x R_z} \right)^T$$

$$\underline{E} = \left(\frac{L_x}{L_x R_x - L_x R_z}, 0, \frac{L_x}{L_x R_z - L_x R_x} \right)^T$$

$$D_1 = \left(\frac{Q_x}{aQ_z} \right)^2 + \left(\frac{Q_y}{bQ_z} \right)^2 + \left(\frac{1}{c} \right)^2$$

$$D_2 = 2 \left[\left(\frac{Q_x}{aQ_z} \right)^2 (Q_x - F_x) - \left(\frac{Q_y}{bQ_z} \right)^2 P_x \right]$$

$$D_3 = \left(\frac{Q_x P_x - Q_x P_x}{aQ_z} \right)^2 + \left(\frac{Q_y P_x}{bQ_z} \right)^2$$

If $D_2^2 - D_1 D_3 < 0$, then the terminator is not visible from the spacecraft, and the terminator angle calculations for the batch are not performed. In this case, TERM ANG should be set greater than 1000 to cause an overflow for printout and asterisks should be printed. Otherwise,

$$Z_1 = \frac{-D_2 + \sqrt{D_2^2 - 4D_1 D_3}}{2D_1}, \quad Z_2 = \frac{-D_2 - \sqrt{D_2^2 - 4D_1 D_3}}{2D_1}$$

$$X_i = \frac{Q_x}{Q_x} (X_i - P_x) + P_x \quad i = 1, 2$$

$$Y_i = \frac{Q_y}{Q_y} (X_i - P_y) + P_y \quad i = 1, 2$$

$$S_i = (X_i, Y_i, Z_i)^T \quad i = 1, 2$$

$$Q = R_v \left(1 - \frac{|R_v - R_R|^2}{|R_v|^2} \right)$$

$$\alpha_i = \cos^{-1} \left[\text{UNIT} (R_v - Q) \cdot \text{UNIT} (S_i - Q) \right] \quad i = 1, 2$$

TERM ANG = smaller of α_1, α_2

The effective height for each observation is given by

$$H_j = h + \Delta m_j / \frac{\partial m_j}{\partial h}$$

Statistics on several parameters listed below are required, and the equations for computing these statistics are the same for each parameter. The weighted statistical mean is given by

$$\mu = \frac{1}{N} \sum K_j c_j$$

The weighted statistical standard deviation is given by

$$\sigma = \left[\frac{\sum (K_j c_j)^2 - N \mu^2}{N - 1} \right]^{1/2}$$

where N is the number of sightings in the set and ϵ is the required parameter. The mean and standard deviation are to be computed for each star and each batch for the following parameters.

Method 1: Effective height
Residual

Method 2: Effective height
Residual
SFOV
MFOV
PLANE ERROR
POINT ERROR

The statistics will not be calculated for a star when fewer than two observations on that star have a non-zero weight for K_j .

In figure 1, the format of the desired program output is illustrated. New pages of data should be initiated by subtitles "Launch Time", "Option 1 Processing Summary", and "Option 2 Processing Summary". In table I, the output is described in detail, and the units for the output variables are specified.

TABLE I.- VARIABLES NEEDED FOR OUTPUT

Variable name	Units	Format	Remarks
Launch time			G.m.t.
Years	Years	14	Year of launch
Month	Months	12	Month of launch
Day	Days	13	Day of launch
H:M:S	Hr:min:sec	13,18;12,18; F5.2	Time of launch
Position	Earth radii	F14,10,4X,F14,10, 4X,F14,10	Vehicle anchor vector for batch
Velocity	Earth radii per hour	F14,11,4XF14,11, 4X,F14,11	Vehicle anchor vector for batch
Time	Hr:min:sec	13,18;12,18; F5.2	Time associated with anchor vector (g.e.t.)
REFORMAT	None	3(3(F11.8,3X)/)	
Mark time	Hr:min:sec	13,18;12,18; F5.2	Time of observation (g.e.t.)
Range	Earth radii	F5.2	Distance from vehicle to observation planet (always positive)
N	None	A1	N for near horizon; F for far horizon
STAR	None	03	Star identification number (always posi- tive)
O2	Degrees	F6.2	Outer gimbal angle (always positive)
I2	Degrees	F6.2	Inner gimbal angle (always positive)
M2	Degrees	F6.2	Middle gimbal angle (always positive)
SHAFT	Degrees	F6.2	Shaft angle (always positive)

Change 1, October 8, 1970

TABLE I.- VARIABLES NEEDED FOR OUTPUT - Continued

Variable name	Units	Format	Remarks
TRUN	Degrees	F6.3	Trunnion angle
WT	None	F4.2	Relative measurement weighting (usually 1 or 0); never negative
Eff Alt	Kilometers	F5.1	Option 1 solution for altitude; statistics required
Eff Resid	Milliradians	F6.4	Option 1 residual; statistics required
Act Alt	Kilometers	F5.1	Option 2 solution for altitude; statistics required
Act Resid	Milliradians	F6.4	Option 2 residual; statistics required
SPOV	Degrees	F5.3	Statistics required
NRGT	Degrees	F5.3	Statistics required
Plane Error	Degrees	F5.2	Statistics required
Point Error	Minutes of arc	F5.1	Statistics required
Term Ang	Degrees	F4.1	Always positive

Row 1 of final solution

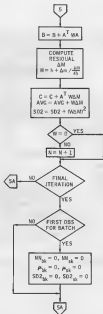
Eff Ht.	Kilometers	F5.1	From iterative solution, option 1
Eff Trun Bias	Milliradians	F7.5	From iterative solution, option 1

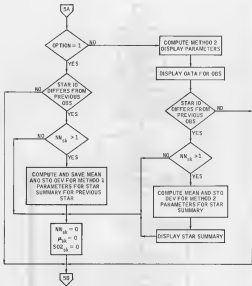
Change 1, August 13, 1970

TABLE I.- VARIABLES NEEDED FOR OUTPUT- Concluded

Variable name	Units	Format	Remarks
SIGH	Kilometers	F7.4	From iterative solution covariance, option 1
SIGHT	Milliradians	F7.5	From iterative solution covariance, option 1
RHD	None	F7.5	From iterative solution covariance, option 1
Row 2 of final solution			
ACT HT	Kilometers	F5.1	From iterative solution, option 2
ACT Trun Bias	Milliradians	F7.5	From iterative solution, option 2
SIGH	Kilometers	F7.4	From iterative solution covariance, option 2
SIGHT	Milliradians	F7.5	From iterative solution covariance, option 2
RHD	None	F7.5	From iterative solution covariance, option 2

DATE	DESCRIPTION	AMOUNT	BALANCE
01/01/2018	OPENING BALANCE	1000.00	1000.00
01/15/2018	SALES	500.00	1500.00
01/20/2018	PAYROLL	(200.00)	1300.00
01/25/2018	RENT	(100.00)	1200.00
02/01/2018	SALES	750.00	1950.00
02/05/2018	PAYROLL	(300.00)	1650.00
02/10/2018	RENT	(150.00)	1500.00
02/15/2018	SALES	600.00	2100.00
02/20/2018	PAYROLL	(250.00)	1850.00
02/25/2018	RENT	(120.00)	1730.00
03/01/2018	SALES	800.00	2530.00
03/05/2018	PAYROLL	(350.00)	2180.00
03/10/2018	RENT	(180.00)	2000.00
03/15/2018	SALES	900.00	2900.00
03/20/2018	PAYROLL	(400.00)	2500.00
03/25/2018	RENT	(200.00)	2300.00
04/01/2018	SALES	1000.00	3300.00
04/05/2018	PAYROLL	(450.00)	2850.00
04/10/2018	RENT	(220.00)	2630.00
04/15/2018	SALES	1100.00	3730.00
04/20/2018	PAYROLL	(500.00)	3230.00
04/25/2018	RENT	(240.00)	2990.00
05/01/2018	SALES	1200.00	4190.00
05/05/2018	PAYROLL	(550.00)	3640.00
05/10/2018	RENT	(260.00)	3380.00
05/15/2018	SALES	1300.00	4680.00
05/20/2018	PAYROLL	(600.00)	4080.00
05/25/2018	RENT	(280.00)	3800.00
06/01/2018	SALES	1400.00	5200.00
06/05/2018	PAYROLL	(650.00)	4550.00
06/10/2018	RENT	(300.00)	4250.00
06/15/2018	SALES	1500.00	5750.00
06/20/2018	PAYROLL	(700.00)	5050.00
06/25/2018	RENT	(320.00)	4730.00
07/01/2018	SALES	1600.00	6330.00
07/05/2018	PAYROLL	(750.00)	5580.00
07/10/2018	RENT	(340.00)	5240.00
07/15/2018	SALES	1700.00	6940.00
07/20/2018	PAYROLL	(800.00)	6140.00
07/25/2018	RENT	(360.00)	5780.00
08/01/2018	SALES	1800.00	7580.00
08/05/2018	PAYROLL	(850.00)	6730.00
08/10/2018	RENT	(380.00)	6350.00
08/15/2018	SALES	1900.00	8250.00
08/20/2018	PAYROLL	(900.00)	7350.00
08/25/2018	RENT	(400.00)	6950.00
09/01/2018	SALES	2000.00	8950.00
09/05/2018	PAYROLL	(950.00)	8000.00
09/10/2018	RENT	(420.00)	7580.00
09/15/2018	SALES	2100.00	9680.00
09/20/2018	PAYROLL	(1000.00)	8680.00
09/25/2018	RENT	(440.00)	8240.00
10/01/2018	SALES	2200.00	10440.00
10/05/2018	PAYROLL	(1050.00)	9390.00
10/10/2018	RENT	(460.00)	8930.00
10/15/2018	SALES	2300.00	11230.00
10/20/2018	PAYROLL	(1100.00)	10130.00
10/25/2018	RENT	(480.00)	9650.00
11/01/2018	SALES	2400.00	12050.00
11/05/2018	PAYROLL	(1150.00)	10900.00
11/10/2018	RENT	(500.00)	10400.00
11/15/2018	SALES	2500.00	12900.00
11/20/2018	PAYROLL	(1200.00)	11700.00
11/25/2018	RENT	(520.00)	11180.00
12/01/2018	SALES	2600.00	13780.00
12/05/2018	PAYROLL	(1250.00)	12530.00
12/10/2018	RENT	(540.00)	11990.00
12/15/2018	SALES	2700.00	14760.00
12/20/2018	PAYROLL	(1300.00)	13460.00
12/25/2018	RENT	(560.00)	12900.00
01/01/2019	CLOSING BALANCE		12900.00





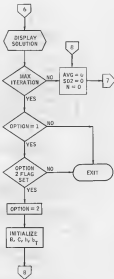
Page 5A of 6

Flow chart 1. - Continued.



Page 5B of 6

Flow chart 1.- Continued.



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Flow chart 1. - Concluded.