

UC San Diego

UC San Diego Previously Published Works

Title

Soiling losses for solar photovoltaic systems in California

Permalink

<https://escholarship.org/uc/item/5kd297nm>

Journal

Solar Energy, 95

ISSN

0038092X

Authors

Mejia, Felipe A
Kleissl, Jan

Publication Date

2013-09-01

DOI

10.1016/j.solener.2013.06.028

Peer reviewed

Soiling Losses for Solar Photovoltaic Systems in California

Felipe A Mejia, Jan Kleissl

Keywords: Soiling, PV Performance

Center for Renewable Resources and Integration, Department of Mechanical and Aerospace Engineering, University of California, San Diego 9500 Gilman Dr., La Jolla, CA 92093, USA

Abstract

Soiling is the accumulation of dust on solar panels that causes a decrease in the solar photovoltaic (PV) system's efficiency. The changes in conversion efficiency of 186 residential and commercial PV sites were quantified during dry periods over the course of 2010 with respect to rain events observed at nearby weather stations and using satellite solar resource data. Soiling losses averaged 0.051% per day overall and 26% of the sites had losses greater than 0.1% per day. Sites with small tilt angles ($<5^\circ$) had larger soiling losses while differences by location were not statistically significant.

1. Introduction

With the rapid increase in the use of photovoltaic (PV) power in California, which has 47% of the installed PV capacity in the US, the optimal management and analysis of expected performance of PV sites becomes increasingly important. Soiling can have a large effect on efficiency during long droughts[1], which mainly occur during the summer season coincident with the largest solar resource. Dust from air pollution particles, sea salt, pollen, agricultural activity, construction and other anthropogenic and natural sources accumulates on the panels until it is removed either by rain or washing.

Research on soiling has primarily been conducted in the middle-east [2] due to the large aerosol loading in the air and the greater abundance of or plans for concentrating solar power plants that are much more affected by soiling. For a concentrating solar power desalination plant in Abu Dhabi, UAE soiling was found to be strongest during sandstorms in the summer season [3]. The transmittance of glass panels after 30 days of exposure in India decreased from 90% to 30% for horizontal and from 90% to 88% for vertical panels [4].

Another more recent study examined the effects of soiling for 250 sites monitored by PowerLight (now SunPower) [1]. Since several of these sites are in areas with frequent rain their study focused on sites in the southwestern United States where long droughts are more common. They also excluded sites with an R^2 value between soiling energy losses and time of less than 0.7 which left a total of 46 sites. Between rain events, soiling losses were found to aggregate linearly with time with an average daily soiling loss of 0.2%. While this paper provides a methodological foundation for analyzing soiling losses, the site selection criteria may have led to an overestimate of soiling losses.

36 The goals of this study are to quantify performance decrease due to soiling and to provide
 37 guidance on the necessity of cleaning solar panels in California. In Section 2 the PV power
 38 dataset and quality control are described and three different methods for identifying soiling
 39 losses on PV panels are introduced. Soiling results are presented, stratified by location and panel
 40 tilt, and discussed in Section 3. The conclusions are given in Section 4.

41 2. Data

42 2.1. California Solar Initiative Sites

43 Under the Performance Based Incentive (PBI) program of the California Solar Initiative
 44 (CSI) rebate payouts are based on AC energy output metering in 15 minute intervals [5]. The AC
 45 power produced from 194 San Diego Gas and Electric (SDG&E), 385 Southern California
 46 Edison (SCE), and 403 Pacific Gas and Electric (PGE) sites were obtained for the year of 2010.
 47 These data were then quality controlled one-by-one to eliminate sites that had more than 70 %
 48 missing data, large noise, or inverter clipping of power. In this way, 305 sites with high quality
 49 data were identified. The CSI database also includes the azimuth and tilt angle of the solar
 50 panels.

51 2.2 Solar Conversion Efficiency

52 The 15 minute data from the CSI database was aggregated over a day to obtain more
 53 robust efficiency estimates. The estimated solar irradiation from SolarAnywhere (SAW) was
 54 used to model the solar resource for each CSI site. SAW uses satellite images to derive global
 55 horizontal (GHI) and direct normal irradiation (DNI) every 30 minutes at 1 km resolution.
 56 SAW's solar irradiation shows a typical mean bias error of 3% and no persistent error trends
 57 across the year [6]. Using the daily energy produced from the CSI site (P_{CSI}) and the daily
 58 incident solar energy modeled from SAW (P_{SAW}), the daily (relative) DC solar conversion
 59 efficiency (η_r) for the solar panels was calculated, controlling for the effects of temperature
 60 η_T and inverter η_{AC} efficiency as follows:

$$\eta = \frac{P_{CSI}}{P_{SAW}} (1)$$

$$P_{SAW} = \frac{GI_{SAW}}{1000 \text{ W m}^2} P_{rated} \eta_{AC} \eta_T (2),$$

61 where GI_{SAW} is SolarAnywhere global irradiation at the plane-of-array transposed using the Page
 62 model [7] and P_{rated} is the rated DC power output of the site. PV cell temperature and
 63 temperature efficiency correction were modeled as in [8] and $\eta_T = 1 - \alpha(T_{cell} - 25^\circ\text{C})$ with
 64 $\alpha = 0.5 \text{ \% K}^{-1}$, respectively. Inverter efficiency was modeled using a 3rd order polynomial
 65 versus power factor as in [9]. To be able to intercompare soiling effects between sites, η was
 66 then normalized by its average for the year to obtain a relative performance η_r .

67 2.3 Rain Data

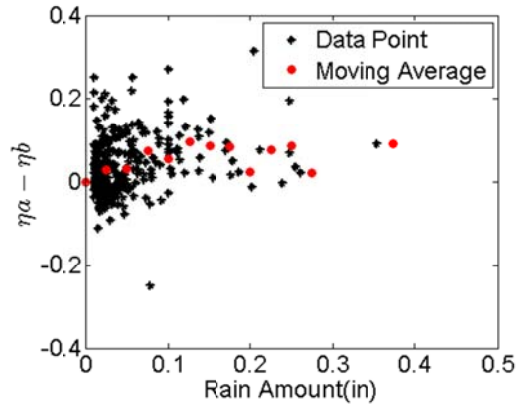
68 Data from the California Irrigation Management Information Systems (CIMIS) were used
69 to estimate the amount of rain at each CSI site. Hourly data from 134 CIMIS stations were
70 obtained and quality controlled by examining the difference in daily rain versus the site distance
71 for each station pair (not shown) leading to exclusion of one CIMIS station. Daily rain data were
72 linearly interpolated from the 133 remaining CIMIS stations to the CSI sites. 90 CSI sites were
73 outside the interpolation region and were excluded. Within the interpolation region all CSI sites
74 were within 50 km from a CIMIS site indicating that the rain data was generally representative of
75 the CSI sites.

76 A final quality control was conducted by visually inspecting plots of interpolated rain and
77 η_r for each site over the course of the year. At 36 sites η_r exhibited a pronounced parabolic
78 shape suggesting that the tilt angle in the CSI database was incorrect and these sites were
79 removed from this study. This left 186 sites, 76 sites from PGE, 75 from SCE, and 35 sites from
80 SDG&E. 14 sites were found to have a pronounced decrease in η_r during the summer,
81 suggesting soiling, but η_r rapidly increased without a concurring rain event. These sites were
82 assumed to have a washing system for the PV panel and 0.1 in rain events were manually added
83 to the data.

84 2.4 Rain Events

85 Two main factors control how much soiling exists on a PV panel: the accumulation of
86 dust which is a function of location and duration of exposure, and the removal of dust through
87 rain. PV panels are naturally cleaned by rain, but the effectiveness of cleaning varies with the
88 amount of rain. This was analyzed by averaging η_r for the week before a rain event (η_b) and for
89 the week after a rain event (η_a). The difference ($\eta_a - \eta_b$) was then assumed to be the increase in
90 efficiency that is caused by a rain event. However, no correlation between rain amount and
91 change in efficiency was observed consistent with [1], probably because the majority of soiling
92 durations are only 10s of days and during such a short time soiling losses are smaller than other
93 sources of variations in efficiency. Consequently, only rain events after droughts of at least 31
94 days (similar to [1] who applied a 20-50 day “grace period”) were considered for this part of the
95 analysis (Fig. 1). Then, $\eta_a - \eta_b$ increased with rain amount from 0 to 0.1 in of rain and
96 stabilized at larger rain amounts. This suggests a proportionality relationship for small rain
97 amounts and a threshold of 0.1 in of rain beyond which the cleaning effectiveness does not
98 increase.

99 Consequently, a rain event was defined as a day when more than 0.1 in of rain are
100 observed and is assumed to restore the panel’s efficiency to that of a clean panel. Rain storms
101 with multiple consecutive rain event days were combined into one multi-day rain event.

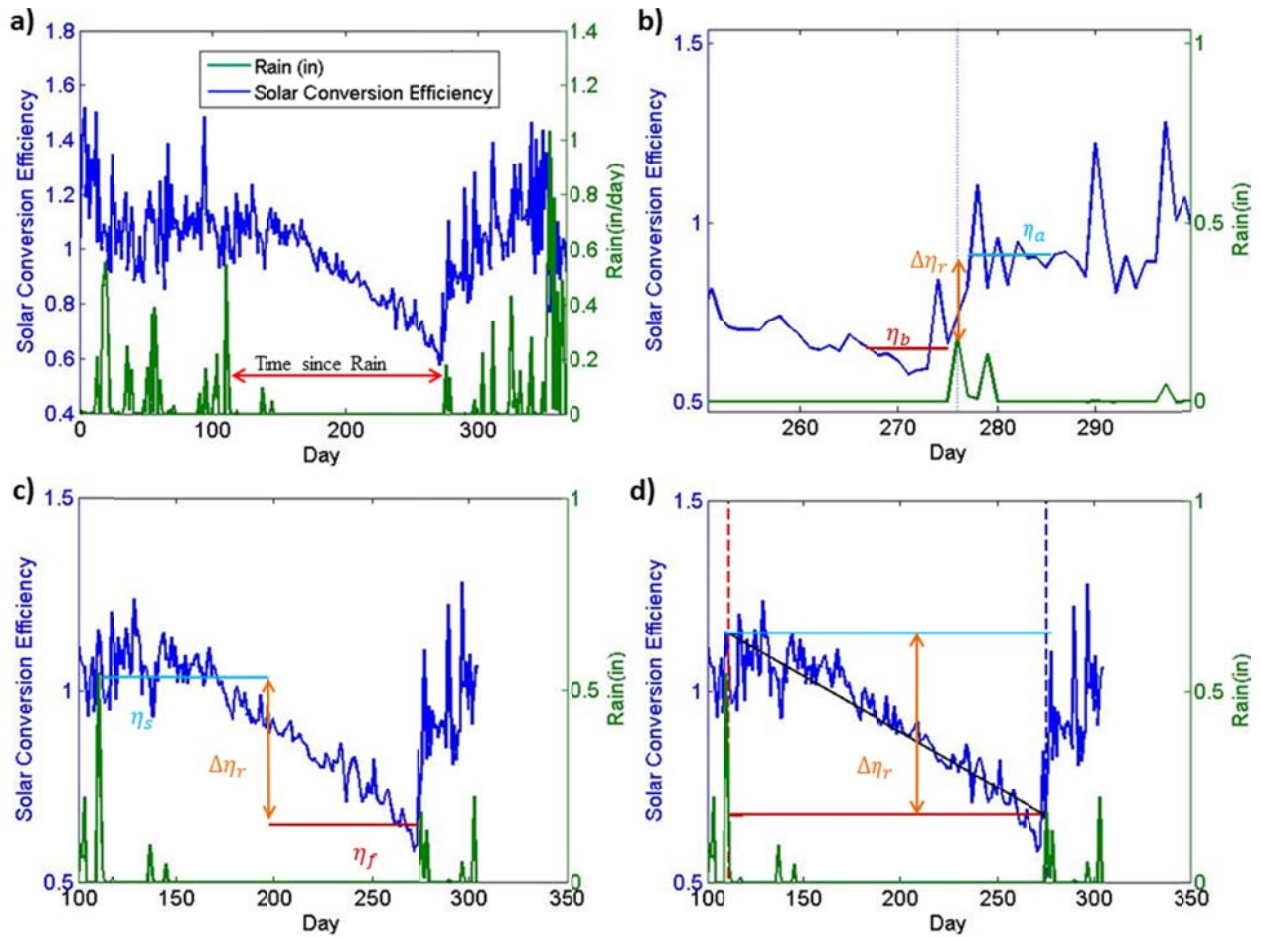


102

103 Fig. 1 Change in panel efficiency during a rain event after droughts longer than 31 days versus
 104 amount of rain for all CSI sites during 2010. The moving average is computed over bins of 0.02
 105 in of rain.

106 **2.5 Quantifying losses due to soiling**

107 As demonstrated in Fig. 2a, large soiling impacts were observed at some sites. These
 108 soiling effects were particularly strong during the long summer droughts. At the site in Fig. 2a,
 109 there is a steady decrease in the efficiency of the PV plant after the last rainfall before summer
 110 (day 110). The rain events in the fall restore the PV plant to the efficiency observed at the
 111 beginning of the year. Note that the large day-to-day variability in solar conversion efficiency is
 112 caused by random errors in the satellite solar resource model that average out when longer
 113 periods are considered.



114

115 Fig. 2a) Timeseries of daily solar conversion efficiency η_r and daily rainfall for a 554 kW_{dc} PV
 116 plant in Hanford Kings, CA in 2010. Soiling losses are quantified through three different
 117 methods: b) Zoom in to before and after the first rain event following the summer drought. The
 118 weekly average solar conversion efficiency before (η_b in red) and after (η_a in blue) the rain
 119 event (vertical dashed line) are used to compute the soiling effect $\Delta\eta_r$. c) The weekly average
 120 solar conversion efficiency for the first week of the drought (η_s in blue) and the last week of the
 121 drought (η_f in red) are used to compute $\Delta\eta_r$. d) Linear regression of efficiency versus number of
 122 days since last rain in black. For consistency with the other methods $\Delta\eta_r$ is expressed as the first
 123 (blue) minus the last (red) value of the drought period and these data are used in Fig. 3.

124 Three different methods were used to identify the soiling losses. Method 1, which was
 125 used in analyzing the effects of rain amount (Section 2.4), uses the averages of the weeks before
 126 and after the rain event (Fig. 2b). Assuming that the panels are completely clean after the rain
 127 event, the amount of soiling that existed prior to the rain event causes an efficiency decrease
 128 of $\eta_b - \eta_a$ (the difference is now reversed since it refers to soiling losses and not recovered
 129 performance). The day(s) of the rain event are not included in the weekly averaging, rather the
 130 averaging occurs over the week before and the week after the rain event. The seven day
 131 averaging is used to reduce noise (e.g. from random errors in the satellite solar resource estimate
 132 in Eq. 1) and avoid occasional days of missing data right before or after the rain from impacting
 133 the analysis. Also days that had an efficiency above 1.5 or below 0.5 were excluded since large

134 excursions are typically a result of an error in the solar resource model. The daily soiling losses
135 for the drought period are calculated as $\eta_b - \eta_a$ divided by the days since the previous rainfall.
136 The calculations for method 1 are demonstrated in Fig. 2b, where $\eta_b - \eta_a = -0.28$ and the
137 soiling losses for the preceding 165 day drought period were $-0.0017/\text{day}$.

138 The second method - similar to the first method - uses weekly averaging, but the
139 efficiencies averaged over the week after the previous rain event η_s and the week before the next
140 rain event η_f are compared. Days that had efficiency above 1.5 or below 0.5 were also excluded
141 from the average. Again the daily soiling losses for the drought period are calculated as $\eta_f - \eta_s$
142 divided by the days since the previous rainfall. This method can be observed in Fig. 2c, where
143 $\eta_f - \eta_s = -0.41$ and the soiling losses for that drought period were found to be $-0.0025/\text{day}$.

144 The final method calculates soiling losses by applying a linear regression fit to the entire
145 data during the drought period. The slope of the best fit line is then assumed to be the daily
146 soiling for that drought. For quality control, droughts when more than 20% of the efficiency data
147 were above 1.5 or below 0.5 were excluded. Also efficiency data greater than 1.5 or less than 0.5
148 were not used in the fit. This method can be observed in Fig. 2d, where the soiling losses for that
149 drought period were found to be $-0.0029/\text{day}$.

150 Each of these methods has particular benefits and assumptions. The method of choice in
151 this analysis is method 3, which was previously shown to quantify soiling [1]. Method 3 only
152 includes the assumption that the efficiency changes are caused by soiling and not by other factors
153 such as panel degradation and seasonal errors in the SAW resource model. In general, these other
154 factors are small or should average out over many sites and rain events. Method 3 also uses the
155 largest amount of data points. Method 2 uses similar assumptions but is limited because it uses a
156 smaller amount of data. Finally method 1 assumes that the panel is equally clean at the start of
157 the drought period and after the next rain event such that differences in efficiency are only
158 related to soiling during that drought period. For long droughts, method 1 has the advantage that
159 the data used for soiling calculations fall within a continuous 2 week period such that panel
160 degradation and seasonal errors in the SAW resource model become minimal. Overall little
161 difference in the overall soiling losses was observed for the different methods (see Fig. 4 later)
162 indicating that the results are robust.

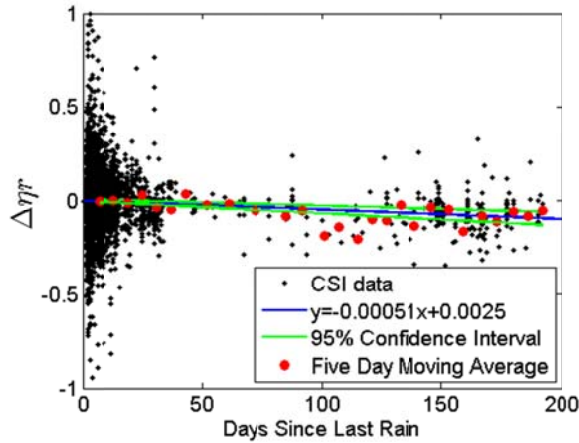
163 **3. Results and Discussion**

164 **3.1 Average soiling losses**

165 Fig. 3 demonstrates the soiling losses as change in relative solar conversion efficiency
166 versus time between rain events as calculated from method 3 (Fig. 2d) for all rain events at every
167 site. The slope of the linear regression gives the average daily soiling losses as 0.00051 per day
168 in relative solar conversion efficiency. In other words, if a site had an average efficiency of 15%
169 its efficiency would decrease to 13.89% after a 145 day drought, which is the average of the
170 longest drought period for each site.

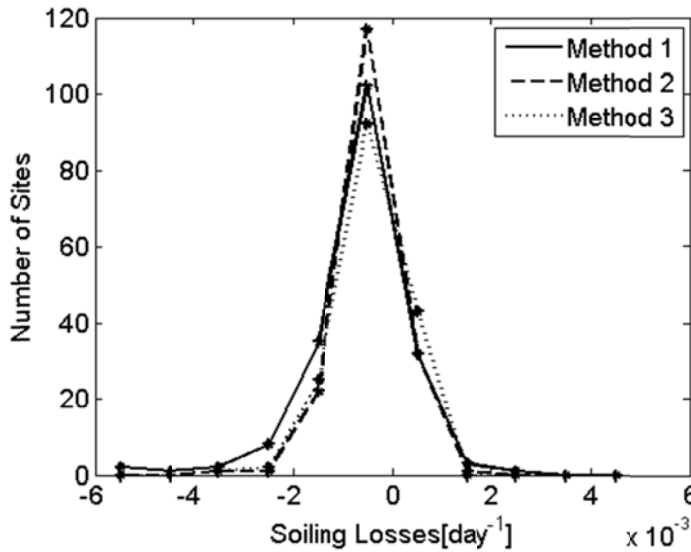
171 To calculate the losses for each site, a linear regression is fit to the scatter plot of the soiling
172 losses and drought period for each site. Fig. 4 shows the distribution of soiling losses for the 186

173 sites for each of the three methods. Some sites have a positive soiling losses (or soiling gains)
 174 which indicates that essentially no soiling occurred and that small errors in the solar resource
 175 model caused a positive slope in Fig. 2d. There is also a possibility that a few sites had
 176 automated washing systems (or meticulous owners/operators) which kept the panels
 177 continuously clean, but overall these scenarios are unlikely. Since the soiling losses are
 178 consistent between the three methods, the linear regression method (method 3) is used for the
 179 remainder of the paper.



180

181 Fig. 3 Change in efficiency during a drought period (method 3) versus time since last rain event
 182 at all CSI sites. 12 outliers smaller than -1 are not shown. Red circles show the average for each
 183 day. A linear regression fit with 95% confidence interval is applied to the data.



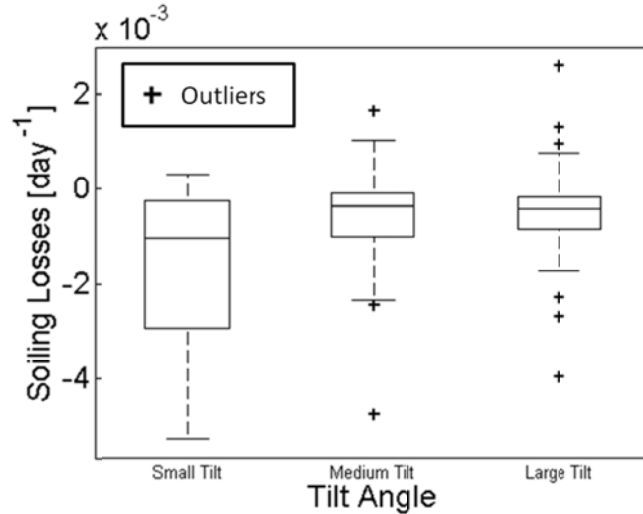
184

185 Fig. 4 Histogram of the soiling losses at all CSI sites as computed from the three different
 186 methods (Section 2.5).

187 **3.2 Tilt angle and Geographical Location**

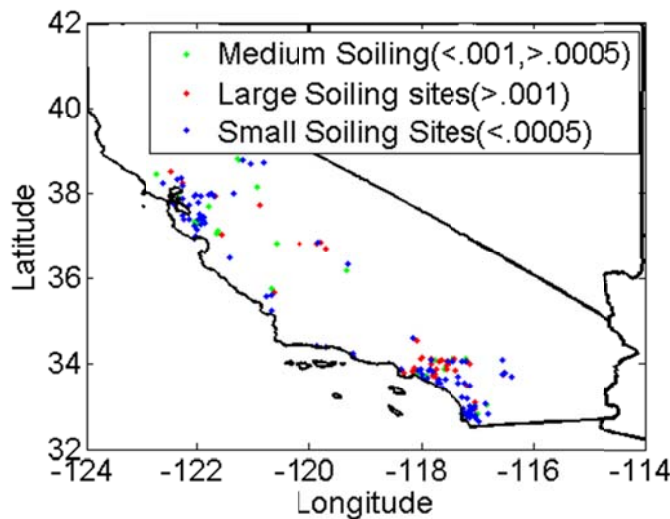
188 48 CSI sites were identified to have losses greater than 0.001. To identify why these sites
189 had larger losses the tilt angle and the location of the sites were investigated.

190 Fig. 5 shows the mean soiling losses for tilt angles from 0-5, 6-19, and greater than 20
191 degrees. The average soiling losses for sites with a tilt angle smaller than 5° is five times that of
192 the rest of the sites as shown in Table 1.



193
194 Fig. 5 Box-Whisker plot of the distribution of soiling loss (method 3) for different tilt angles.
195 The bin from 0 to 5° contains 12 sites, 102 sites have tilts from 6° to 19° and 88 sites have tilts
196 equal to or greater than 20°.

197 A map (Fig. 6) and table (Table 2) of soiling losses by site was used to identify clustering
198 of large soiling sites to identify patterns due to e.g. air pollution or farming. Large soiling
199 appears to be more prevalent in the Los Angeles Basin and the Central Valley area, but the
200 differences are not statistically significant at the 5% level.



201
202 Fig. 6 Map of CSI sites and their soiling losses per day.

203 4. Conclusion

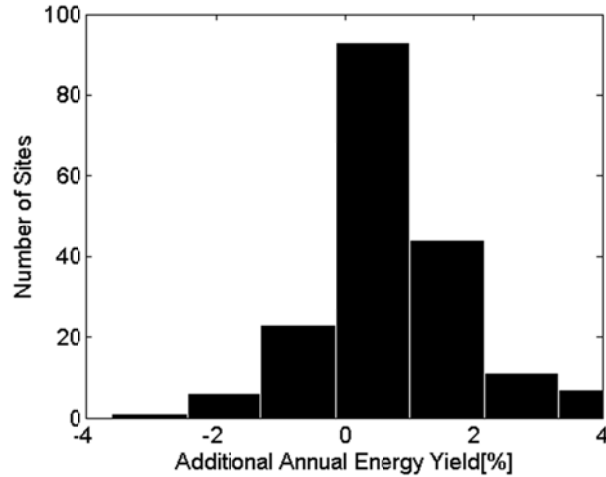
204 One year of power output from 186 PV sites demonstrated how soiling decreases the
205 efficiency of solar PV plants. The accumulated soiling effects were found to depend primarily on
206 the time since the previous rainfall (Fig. 3) and supported previous findings that soiling can be
207 modeled as a linear degradation [1]. On average losses were 0.00051 per day in relative solar
208 conversion efficiency. Over an average 145 day summer drought this results in a 7.4% loss in
209 efficiency. For a 15% efficient PV panel soiling losses over a 145 day drought would decrease
210 the efficiency to 13.9%. For reference, this is more than an order of magnitude larger than losses
211 due to cell degradation (typically 0.5% efficiency loss per year or 0.19% in 145 days) [10].

212 Using a similar method and in a similar geographical region [1] had found four times
213 larger soiling losses of 0.002 per day. We hypothesize that the elimination of sites with R^2 values
214 less than 0.7 in [1] as well as the limited amount of sites examined caused their soiling losses to
215 be biased high. Sites with small soiling losses tend to have smaller R^2 since random errors in the
216 solar resource estimates dominate over the correlation between soiling and time since last rain
217 event.

218 The distribution of soiling by site is skewed with a few sites showing very large soiling
219 losses. Of the 186 sites, 48 were found to have soiling losses greater than 0.001 per day. One
220 factor for these large soiling losses was the tilt angle: sites with a tilt angle less than 5 degrees
221 had on average 5 times the soiling losses than the other sites. This finding supports that more
222 soiling accumulates on a horizontal panel as previously found for glass plates in [4]. The large
223 variability of the data for larger tilts and inconsistent regional trends suggests that soiling is very
224 site specific. For example some sites could have high winds that are able to clean low tilt panels
225 while high tilt panels are better cleaned by gravity. Sites in the Los Angeles basin and the Central
226 Valley Area were found to have larger soiling losses but the differences were not statistically
227 significant to conclusively determine the location as a cause.

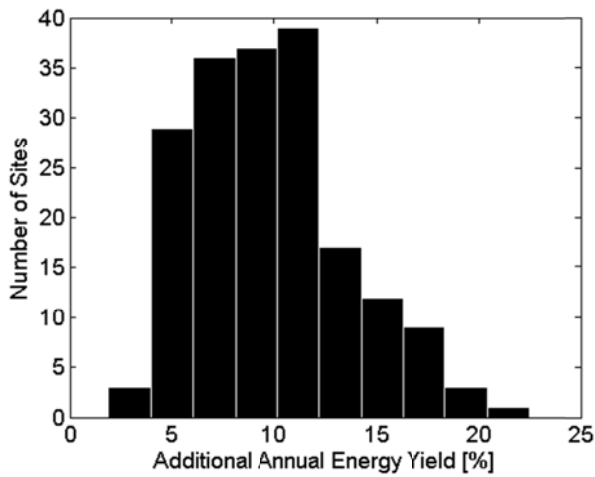
228 How much additional solar energy could be harvested through panel washing? Manual
229 washing is expensive and typically only scheduled during the summer drought. We estimate
230 impacts of one annual washing based on the average soiling losses for each site (Fig. 4) and the
231 one half the length of the summer drought for each site. On average, the sites would have yielded
232 0.81% more annual energy if they had been washed halfway through the summer drought period
233 while some sites would have realized solar energy production increases of up to 4% (Fig. 7).

234 If an automated cleaning system was installed to clean the sites regularly, larger energy
235 gains would be possible, on average 9.8% of annual energy. This estimate is calculated by
236 assuming that the annual maximum of the 30 day moving average efficiency equals the energy
237 output for a completely clean panel. The extra yield (Fig. 8) is then calculated as the integral
238 between the efficiency of this clean panel and the actual observed efficiency.



239

240 Fig 7. Histogram of the additional annual yield possible for each site by cleaning the panel once
 241 per year halfway through the summer drought period.



242

243 Fig 8. Histogram of the percent additional yield if the panel was always clean.

244 The California Solar Initiative database is unique in that production data from a large set
 245 of stations is publicly available and soiling losses could be determined without confidential
 246 information. While soiling effects in California were found to be relatively small and rarely
 247 warrant the additional expense of panel cleaning, sites in direct proximity to anthropogenic air
 248 pollution or natural events such as dust storms may experience more significant soiling.

249 **Acknowledgements**

250 This work was supported by the California Solar Initiative RD&D program. We are
 251 grateful to Stephan Barsun, Itron for helpful comments and provision of literature.
 252 SolarAnywhere data for all of California was provided by Clean Power Research
 253 (Thomas Hoff and Skip Dise).
 254

255 **References**

256 1. Kimber A, Mitchell L, Nogradi S, Wenger H. The Effect of Soiling on Large Grid-Connected
 257 Photovoltaic Systems in California and the Southwest Region of the United States. *IEEE 4th*
 258 *World Conference* 2006.

259 2. Monto M, Rohit P. Impact of Dust on Solar Photovoltaic (PV) Performance: Research Status,
 260 Challenges and Recommendations. 2010; **14** : 3124-3131. DOI: **10.1016/j.rser.2010.07.065**

261 3. El-Nashar A. Effect of dust deposition on the performance of a solar desalination plant operating
 262 in an arid desert area. *Solar Energy* 2003; **75** : 421-431. DOI: **10.1016/j.solener.2003.08.032**

263 4. Garg H. Effect of Dirt on Transparent Covers in Flat-plate Solar Energy Collectors. *Solar*
 264 *Energy* 1974; **15** : 299-302. DOI: **10.1016/0038-092X(74)90019-X**

265 5. California Public Utilities Commission California Solar Initiative Program Handbook. Accessed
 266 Sep. 2011 at: http://www.gosolarcalifornia.org/documents/CSI_HANDBOOK.PDF

267 6. Jamaly M, Bosch JL, Kleissl J. Validation of SolarAnywhere Enhanced Resolution Irradiation
 268 Using Power Output of Distributed PV Systems in California. *Report to the California Solar*
 269 *Initiative RD&D Program*.

270 7. Page J. The role of solar radiation climatology in design of photovoltaic systems. In: Markvart T.
 271 and Castaner L. *Practical handbook of photovoltaics: fundamentals and applications*. Elsevier:
 272 Oxford, 2003;5-66.

273 8. Jones A, Underwood C. A thermal model for photovoltaic systems. *Solar Energy* 2001; **70** : 349-
 274 359. DOI: **10.1016/S0038-092X(00)00149-3**

275 9. Luoma J, Kleissl J, Murray K. Optimal inverter sizing considering cloud enhancement. *Solar*
 276 *Energy* 2012; **86** : 421-429. DOI: **10.1016/j.solener.2011.10.012**

277 10. Itron, Inc., *CPUC California Solar Initiative 2010 Impact Evaluation*, 2012 available at
 278 [http://www.cpuc.ca.gov/NR/rdonlyres/E2E189A8-5494-45A1-ACF2-
 279 5F48D36A9CA7/0/CSI_2010_Impact_Eval_RevisedFinal.pdf](http://www.cpuc.ca.gov/NR/rdonlyres/E2E189A8-5494-45A1-ACF2-5F48D36A9CA7/0/CSI_2010_Impact_Eval_RevisedFinal.pdf)

280 **Tables**

281 Table 1. Soiling losses stratified by tilt angle.

	Number of Sites	Mean Soiling Losses [10 ⁻⁴ day ⁻¹]	Fraction of sites with soiling > 0.1/day [%]
Tilt < 5°	12	-18.0	50
5° < Tilt < 19°	90	-5.2	24.4
Tilt > 20°	84	-5.3	23.8

282

283 Table 2. Soiling losses stratified by geographical region.

	Number of Sites	Mean Soiling Losses [10 ⁻⁴ day ⁻¹]	Fraction of sites with soiling > 0.1%/day [%]
San Francisco Bay	47	-4.8	12.8
Central Valley	29	-5.8	24.1
SCE	75	-8.3	41.3
SDG&E	35	-2.7	11.4

284