Scale-dependent fault roughness effects on earthquake dynamics and ground-motion

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Summary

The effects of **fault roughness** on earthquake rupture dynamics and the radiated seismic wavefield have received increasing attention in numerical models aiming to capture the full frequency range of observed ground motions.

We investigate the scale dependence of fault roughness effects in terms of rupture process zone width and minimum roughness wavelength on earthquake kinematics, dynamics, and ground motion. We study simple models of varying process zone width and faults incorporating band-limited roughness with varying length scales. We find that a larger rupture process zone leads to less coherent rupture fronts and higher variability of rupture speed. In addition, peak slip rate distributions are systematically modulated by the process zone width, highlighting its importance in modulating fault roughness dynamic effects. However, the spectral content of fault slip and rupture speed is consistently self-similar over all scales.

We then discuss the choice of the **smallest wavelength** of the bandlimited rough fault geometry and propose an efficient hybrid approach combining meshed fault roughness, roughness drag and traction heterogeneities.

1. Methods

- **High-resolution 3D** dynamic rupture modeling using **SeisSol**: Seismic wave propagation coupled with frictional fault failure and off-fault inelasticity, optimized for high-performance computing. https://github.com/SeisSol/SeisSol
- **Simple models**: homogeneous medium, flat free surface, all models based on the same strike-slip band-limited self-similar rough fault (50 \times 15 km, minimum (resp. maximum roughness wavelength $\lambda_{min} = 200$ m (resp. $\lambda_{max} = 50$ km), $\alpha = 10^{-2}$, Hurst index H=1).
- We use **linear slip weakening** friction because it is easier to control the rupture process zone width, e.g. using Day et al. (2005) breakdown-zone width estimate:

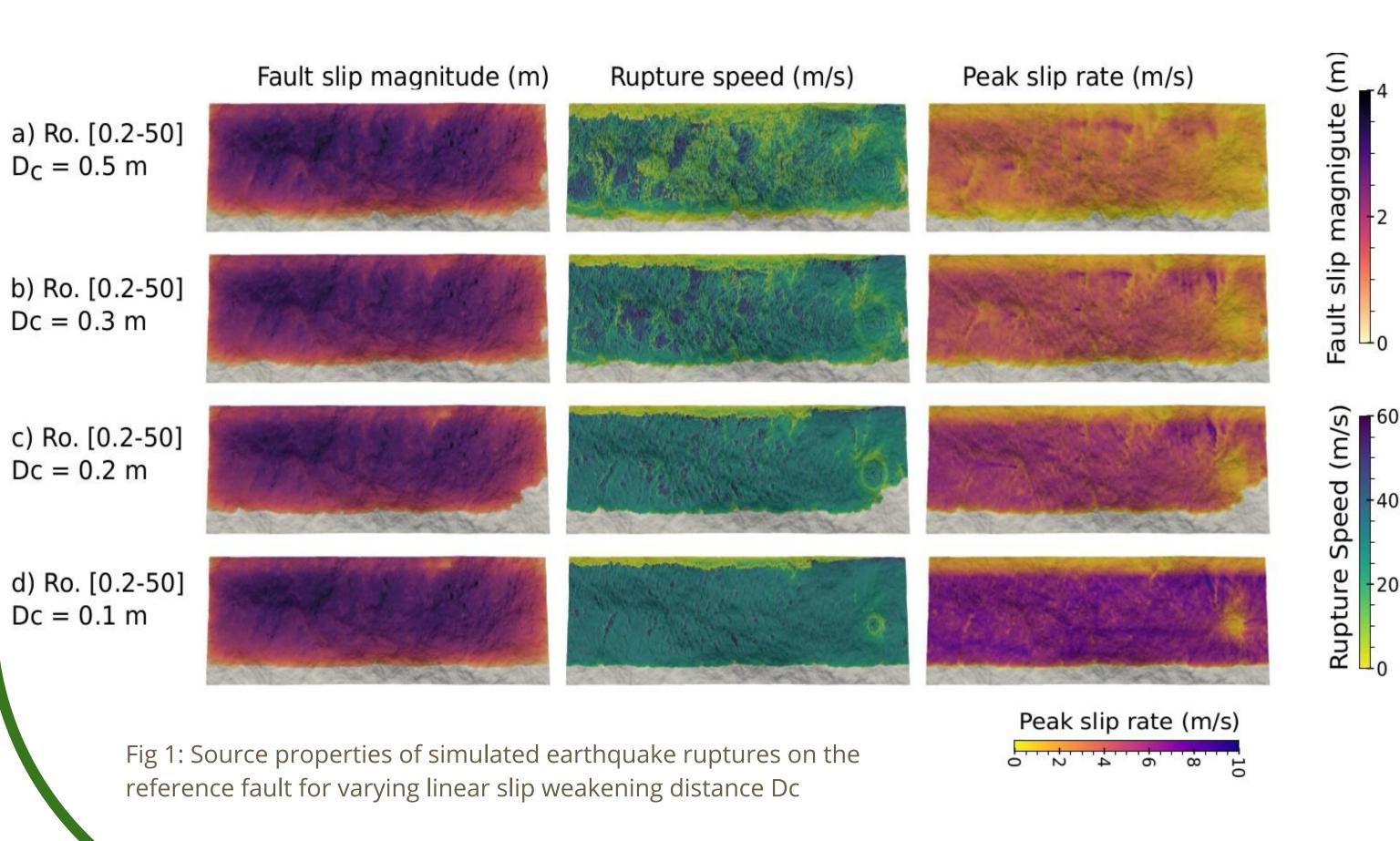
$$\Lambda_0^{III} = \frac{9\pi}{32} \mu \frac{D_c}{\tau_s - \tau_d}$$

With μ the shear modulus, D_c the slip weakening distance, $\tau_{\rm s}$ the fault shear strength and τ_d the fault frictional resistance

 Stress is Andersonian, the angle of maximum compressive stress to the fault is 50° Off-fault plasticity (Wollherr et al., 2018) is accounted for, to prevent unrealistic tresses near the fault kinks.

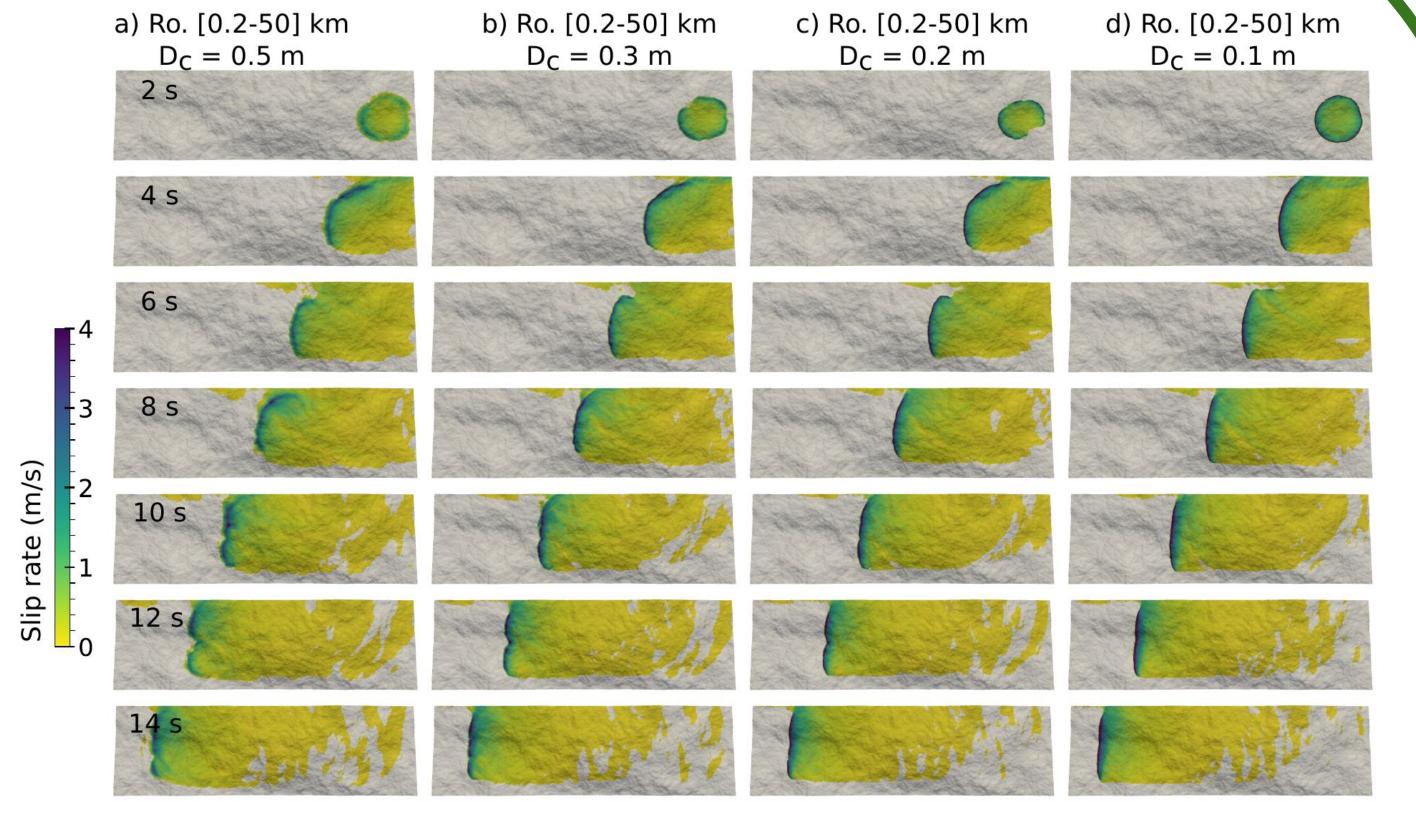
2. Rough fault rupture dynamics with varied process zone width

- We simulate rupture of varying process zone width by varying Dc. The same fault is used in all simulations.
- Rupture evolution is controlled by the energy balance between strain energy release and fracture energy (Madariaga & Olsen 2000): all models have the same stress drop, but the fault strength (parametrized by the prestress ratio R_n) is adapted to keep this balance unchanged.
- Our results suggest that the dynamic rupture process zone width is a key factor modulating the strength of roughness effects. A larger rupture process zone leads to less coherent rupture fronts and higher variability of rupture speed.
- We observe a systematic change in the spectral fall-off of peak slip rate associated with the process zone length (Fig 4b) highlighting its importance in modulating fault roughness dynamic effects.
- On the other hand, the spectral content of **other rupture characteristics** (fault slip, rupture speed) is consistently self-similar over all scales, suggesting that such critical behavior is not an intrinsic characteristic of fault roughness effects.



:) Ro. [0.6-50] + HetT [0.2-0.6] + 0.5 RD, Dc = 0.5 m

Peak slip rate (m/s)



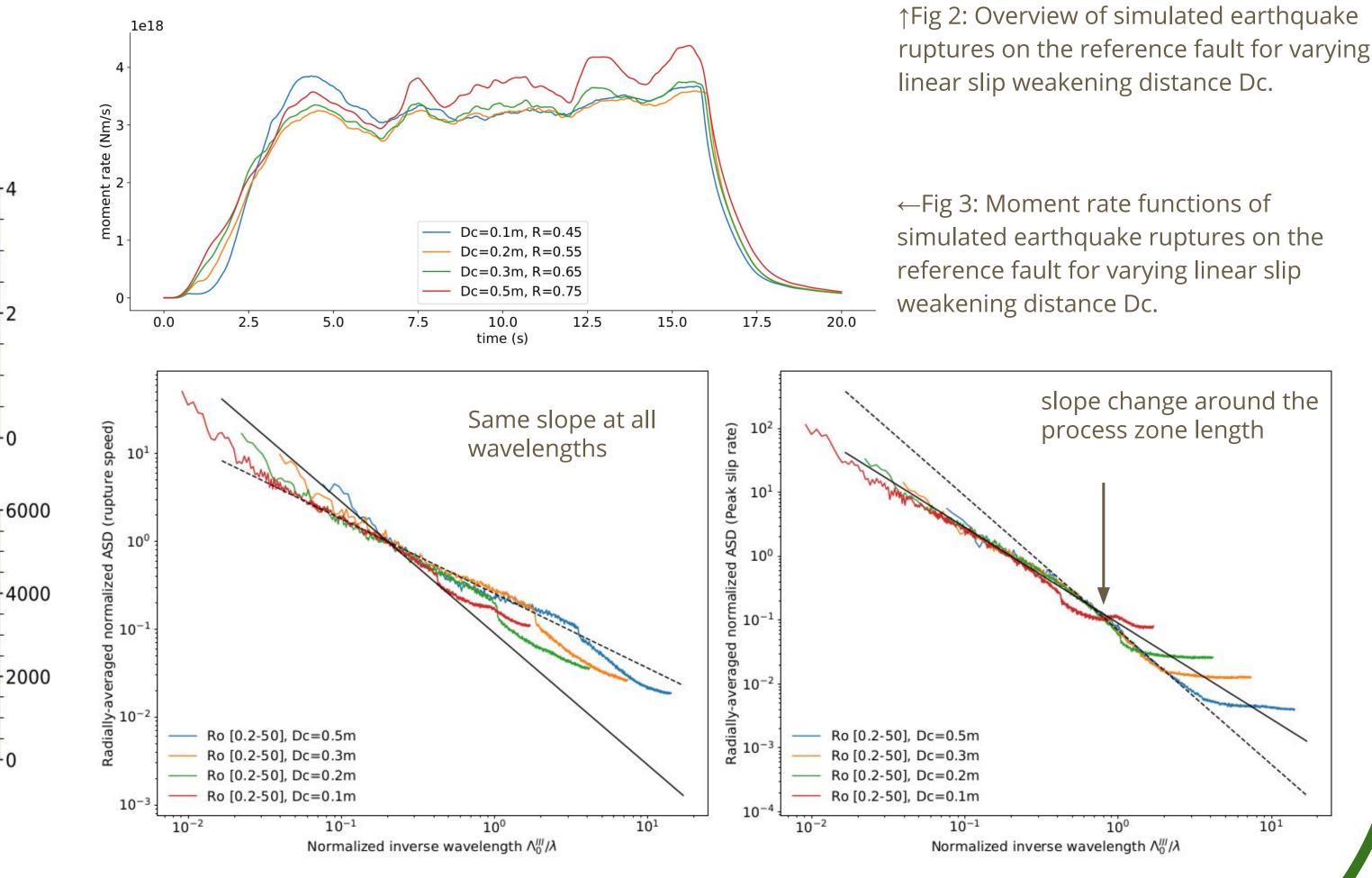


Fig 4: Normalized radially-averaged amplitude spectral density of the rupture speed (a) and the peak slip rate (b). The x axis is normalized by Day et al. (2005)'s estimate of the breakdown-zone with. All curves are normalized by their value at 0.2. The solid black lines illustrate the fall-off of a self-similar model (H=1). The dashed black lines illustrate the fall-off of a self-affine model featuring H=0.35 (a) (resp. H=1.6, (b)).

3. Heterogeneous tractions as a proxy for

a) Ro. [0.2-50] km

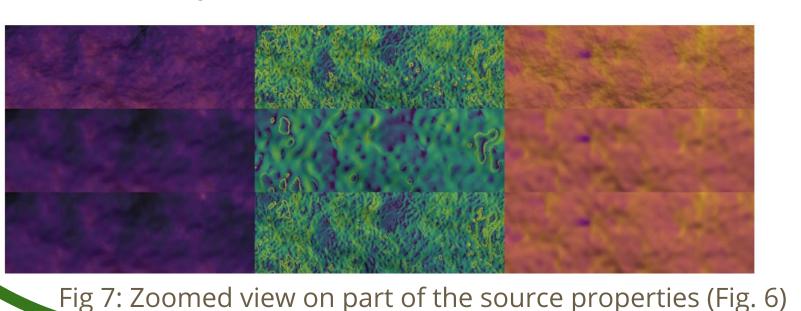
small-scale roughness

- The numerical cost of dynamic rupture models incorporating fault roughness effects may be greatly affected by the **choice of \lambdamin.**
- Based on our findings, we develop strategies to emulate the full dynamic behavior in a hybrid approach, combining small-scale traction and strength **heterogeneity** with **larger-scale** geometric complexity.
- Rupture on a fault derived from a reference fault by **low-pass filtering** its smallest-scale geometric features can resemble the rupture on the reference fault if **fault strength is scaled** accordingly.

$$\tau_{\rm drag} = 8\pi\alpha^2 G^* \Delta (1/\lambda_{\rm min} - 1/\lambda_{\rm max})$$

Roughness drag contribution of the filtered roughness bandwidth, with Δ the fault slip and α the amplitude to wavelength ratio (Fang and Dunham, 2013).

- Nevertheless, the fault slip, rupture velocity and peak slip rate of such model lack of small-scale heterogeneity, which may translate into less realistic synthetic ground motion.
- Proposed hybrid approach: roughness effectively meshed only to a given wavelength and smallest geometric features approximated by traction heterogeneities. performs better at capturing small-scale variations of fault slip and rupture velocity.



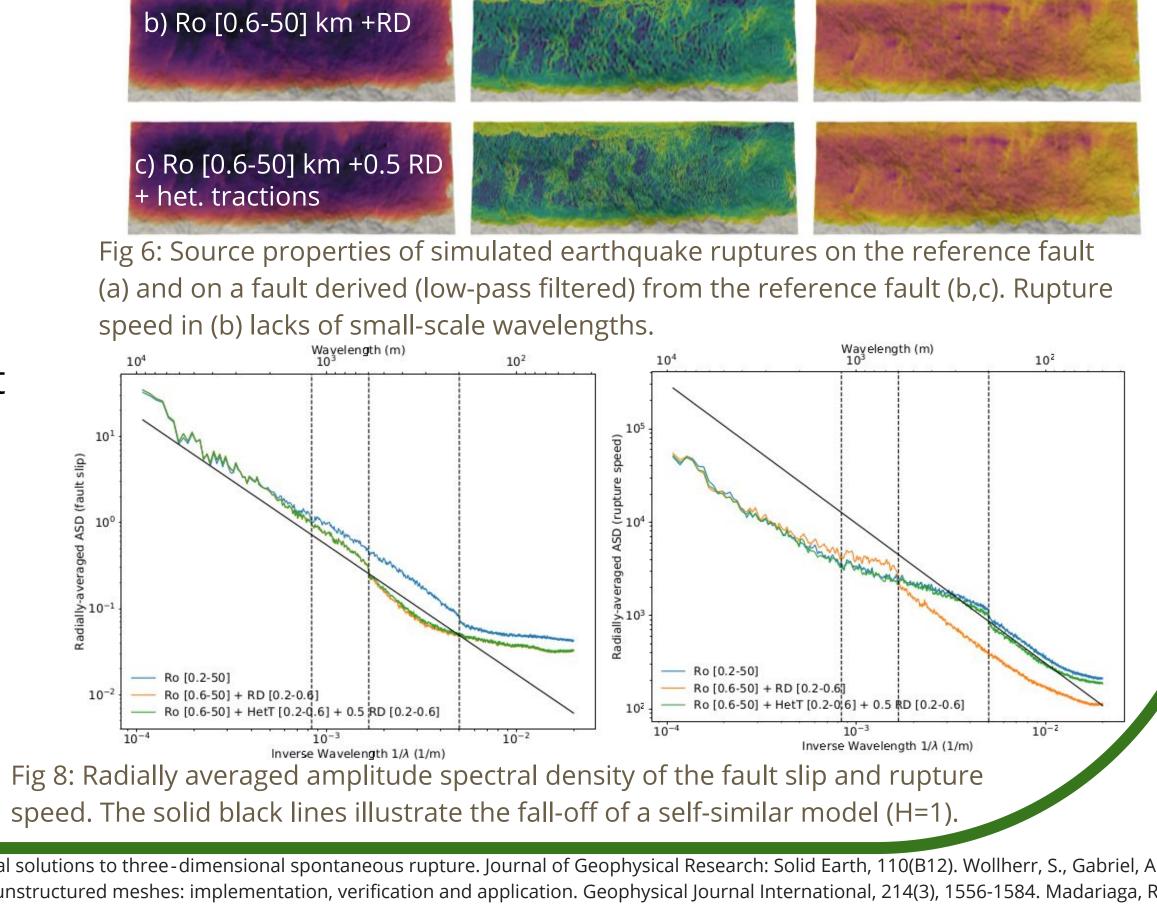


Fig 5: Overview of simulated earthquake ruptures on the reference fault (a) and on a

fault derived (low-pass filtered) from the reference fault (b,c). (b) scaled strength (c)

Rupture speed (m/s)

hybrid approach (traction heterogeneities and scaled strength).

Fault slip magnitude (m)

a) Ro [0.2-50] km,

Dc=0.5m

4. Fault roughness and ground-motion

) Ro. [0.6-50] + RD, D_C = 0.5 m

spectral acceleration computed at 9Hz.

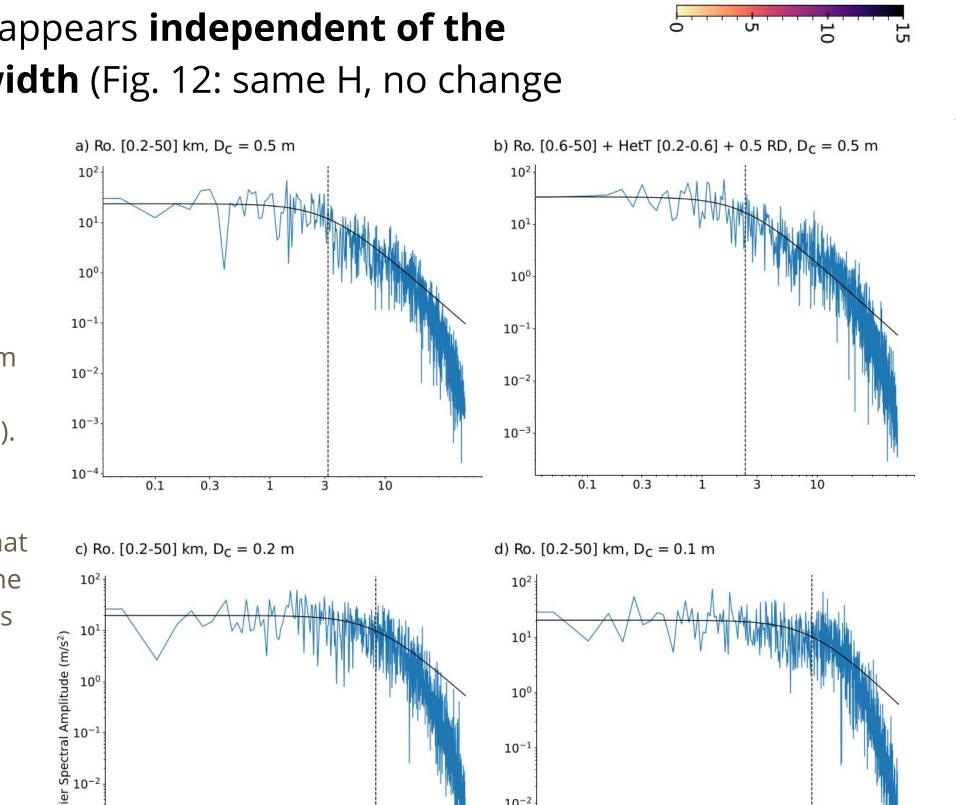
 $SA[0.111s] (m/s^2)$

 Surprisingly, ruptures on both low-pass filtered and reference fault yield high-frequency (up to 10Hz) ground motion with a **high degree of** statistical similarity (e.g. Fig. 10).

• The peak slip rate distribution has certainly a strong impact on the distribution of near-field ground motion. The fluctuations of the peak slip rate decay strongly for decreasing wavelengths below the process zone width (Fig. 4b). Models based on the derived fault, filtered of wavelengths smaller than the estimated process zone width, therefore capture most of the peak slip rate fluctuations, and then yield comparable ground motion.

 The simulated ground-motion presents a flat **spectrum** up to a **corner frequency** which increases with decreasing process zone width.

• The **spatial distribution** of the high frequencies ground-motion appears independent of the process zone width (Fig. 12: same H, no change of slope).



†Fig 9: Near-field synthetic ground motion distribution:

Fig 10: comparison of synthetic near-field ground motion data with 4 recent ground motion prediction equations (GMPE). Left: average spectral acceleration at 0.5, 1 and 2.5s vs fault distance. Right: intra-event standard deviation vs fault distance.

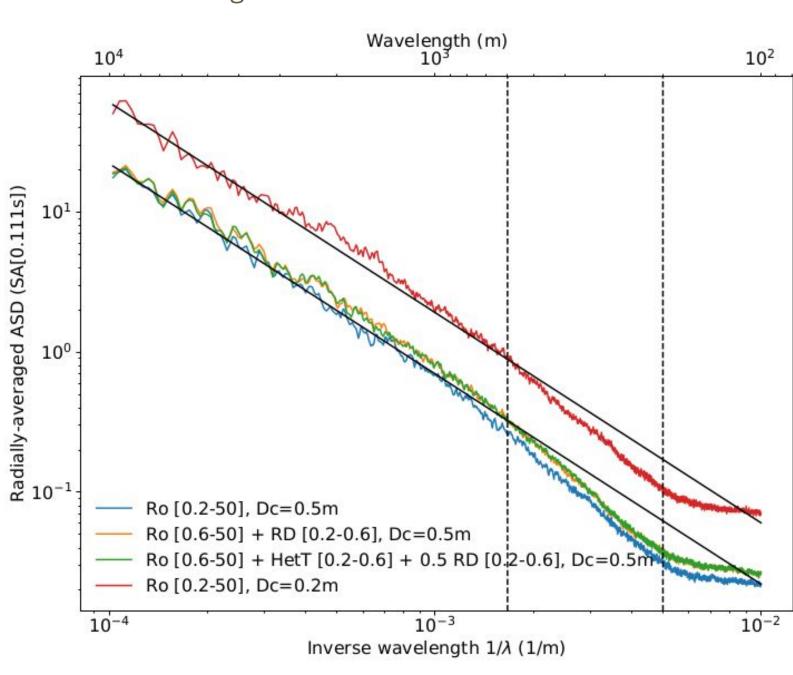
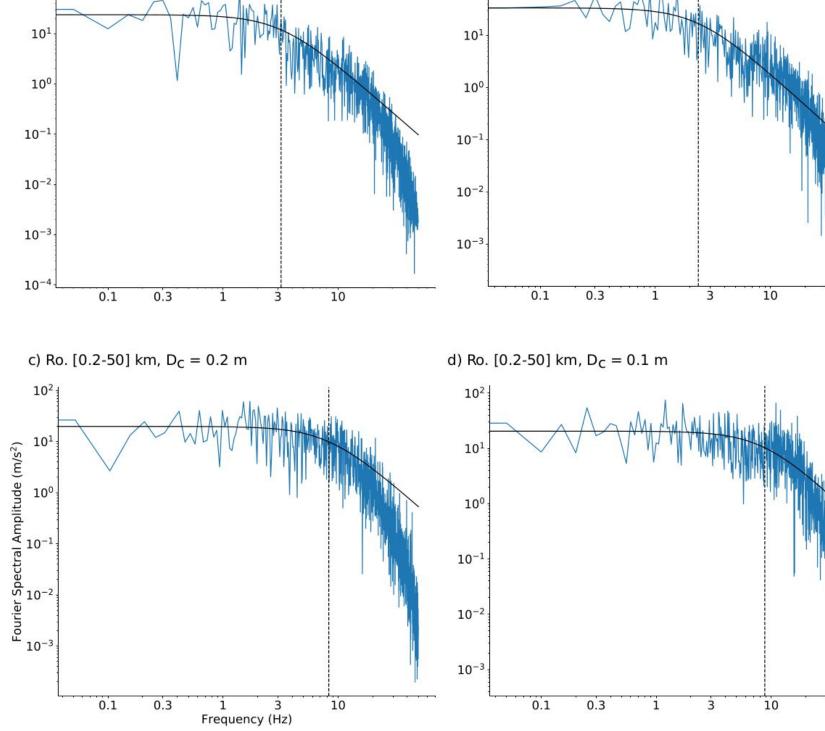


Fig 12: Radially-averaged amplitude spectral density of spectral acceleration at 9Hz SA[0.111s]. The black lines illustrate the fall-off of a self-similar model.

acceleration spectrum along a line of 100 receivers spaced every 0.5km between x=-25 km and x=25 km at y=0 km (roughly above the fault). The black line corresponds to a omega-square model that best fits the data, and the dashed vertical line to its corner frequency.

→Fig 11: Median



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