



# Application of a Jacobian-Free Newton-Krylov Method to the Simulation of Hypersonic Flows

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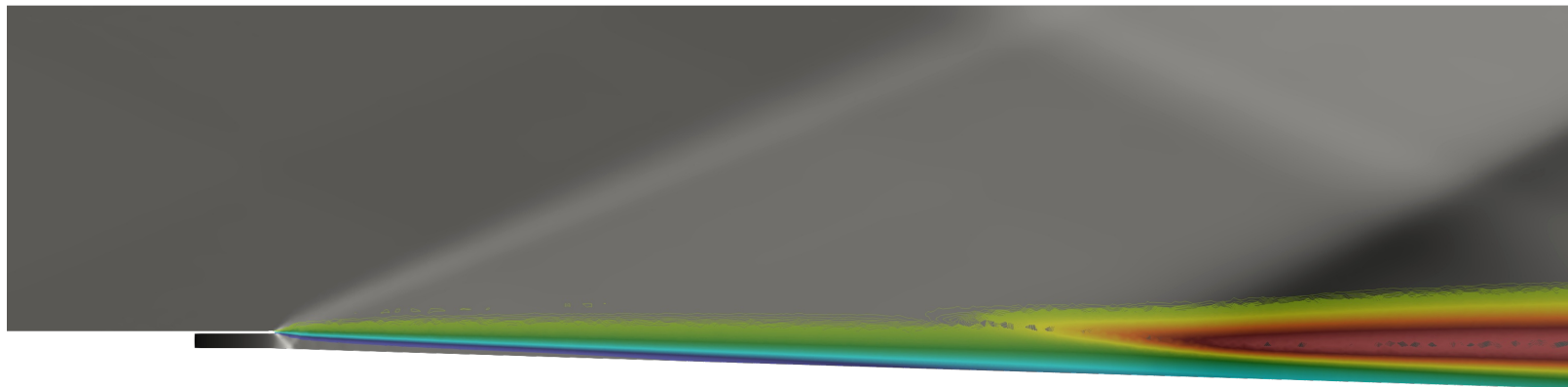
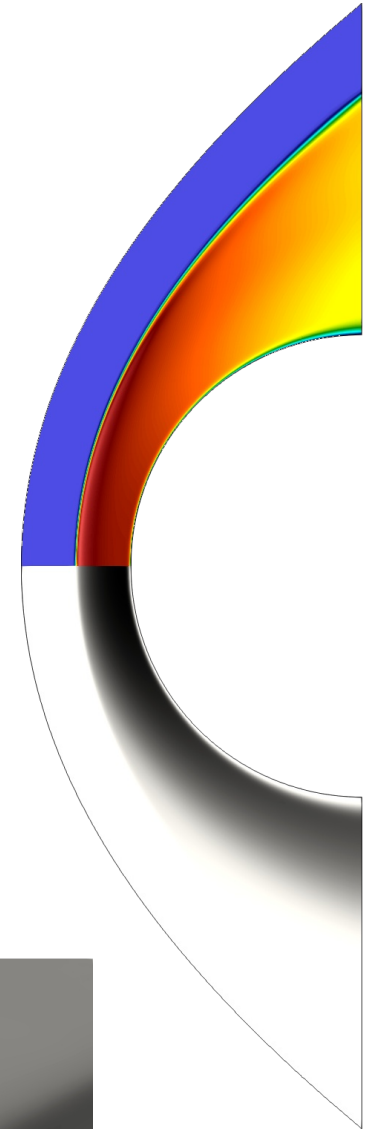
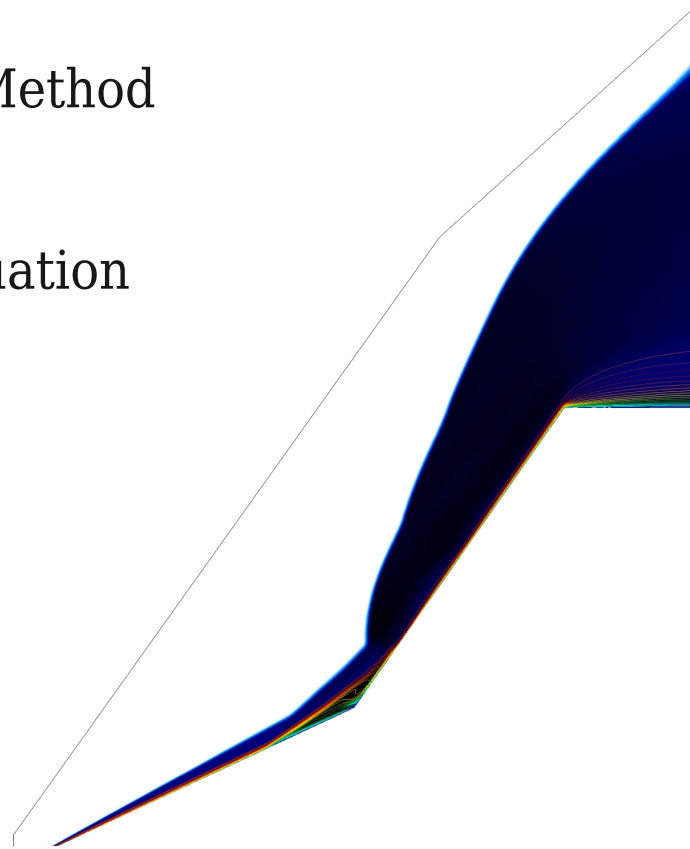
Context: Eilmer flow solver

Jacobian-free Newton-Krylov Method

- + Newton method
- + pseudo-transient continuation
- + Krylov method: GMRES

Point-implicit relaxation

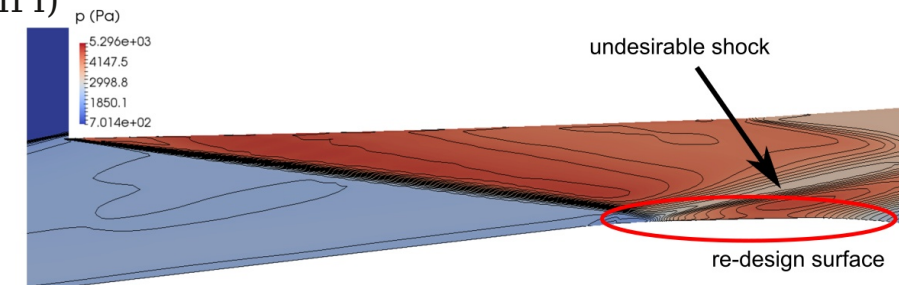
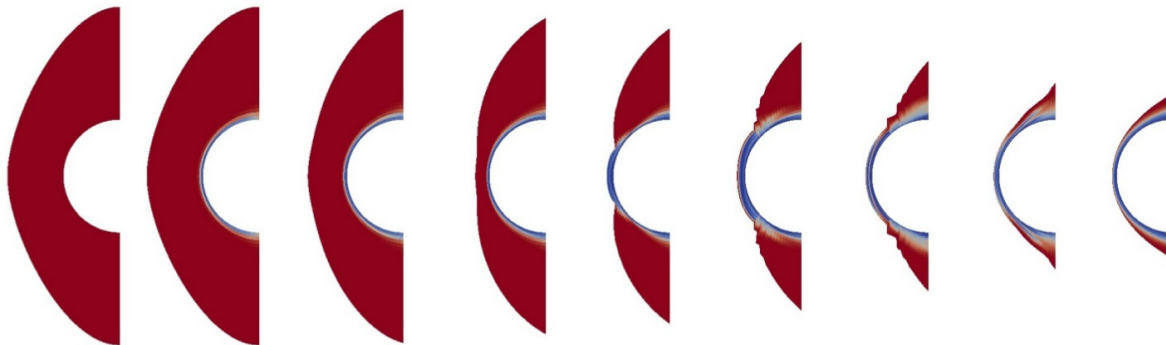
Performance comparisons



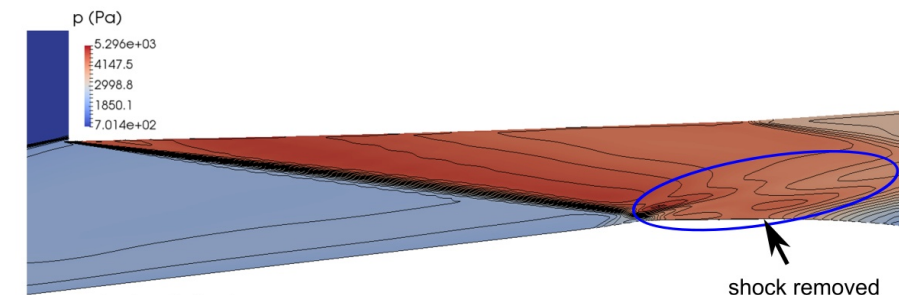
# Eilmer: what it does



- + 2D/3D compressible flow simulation
- + Gas models include ideal, thermally perfect, multi-temperature and state-specific
- + Finite-rate chemistry
- + Inviscid, laminar, turbulent flows
- + Solid domains with conjugate heat transfer
- + User-controlled moving grid capability
- + Shock-fitting method for blunt body shock layers
- + A rotating frame of reference for turbomachine modelling
- + Transient, time-accurate updates with Runge-Kutta family integrators
- + Steady-state accelerator using Newton-Krylov approach
- + User-defined customisations available for boundary conditions, source terms, and pre- and post-processing
- + Parallel computation using shared memory or distributed memory (MPI)
- + Multiple-block structured and unstructured grids
- + Native grid generation and 3rd-party import capability
- + Unstructured-mesh partitioning via Metis
- + Adjoint solver for efficient sensitivities evaluation



a) original design



b) optimized design

solves the compressible Navier-Stokes equations with multi-species multi-temperature extensions

$$\frac{\partial}{\partial t} \int_V \mathbf{U} dV = - \oint_S (\mathbf{F}_i - \mathbf{F}_v) \cdot \hat{n} dA + \int_V \mathbf{Q} dV$$

$$\mathbf{U} = [\rho v_x, \rho v_y, \rho v_z, \rho E, \dots, \rho s, \dots, \rho e_v]^T$$

using finite volume discretization

$$\frac{\partial \mathbf{U}}{\partial t} = -\frac{1}{V} \sum_f^{\text{faces}} (\mathbf{F}_i - \mathbf{F}_v)_f \cdot \hat{n}_f A_f + \mathbf{Q} = \mathbf{R}(\mathbf{U})$$

## Residual evaluation:

1. Reconstruct the flow on both sides of each face
2. Compute the inviscid fluxes  $\mathbf{F}_i$
3. Compute the gradients of the flow at each face
4. Compute the viscous fluxes  $\mathbf{F}_v$
5. Compute the source term  $\mathbf{Q}$  in each cell
6. Compute the residual  $\mathbf{R} = \partial \mathbf{U} / \partial t$

## The promise of JFNK...

*handle any selection of options  
for  $\mathbf{R}(\mathbf{U})$  automatically*



## Newton method

$$\left(\frac{\partial \mathbf{R}}{\partial \mathbf{U}}\right)^n \Delta \mathbf{U}^n = -\mathbf{R}(\mathbf{U}^n), \quad \mathbf{U}^{n+1} = \mathbf{U}^n + \Delta \mathbf{U}^n, \quad n = 0, 1, \dots$$

## Krylov method

+ iterate to solve a linear system

$$\mathbf{Ax} = \mathbf{b}$$

## Jacobian-free

- + never form Jacobian explicitly
- + find algorithm that only uses Jacobian-vector products

to help get into the region of convergence, step loosely in time

$$[\mathbf{A}]^n \Delta \mathbf{U}^n = \left\{ \frac{1}{\Delta t_{\text{local}}} \mathbf{I} - \frac{\partial \mathbf{R}^n}{\partial \mathbf{U}} \right\} \Delta \mathbf{U}^n = \mathbf{R}^n.$$

and solve this system inexactly

$$\|\mathbf{R}^n - [\mathbf{A}]^n \Delta \mathbf{U}^n\| \leq \eta \|\mathbf{R}^n\|$$

as the residual drops, grow the CFL to recover Newton's method

$$CFL^n = CFL^{n-1} \left( \frac{\|\mathbf{R}(\mathbf{U}^{n-1})\|}{\|\mathbf{R}(\mathbf{U}^n)\|} \right)^a$$

to add further robustness, use a relaxation factor based on a physicality check

$$\mathbf{U}^{n+1} = \mathbf{U}^n + \omega^n \Delta \mathbf{U}^n \quad \text{with: } 0 < \omega^n \leq 1$$

adjust  $\omega^n$  so that:

- change in species mass is not too large
- primitive values are physically realizable

We use **GMRES**: Generalized Minimum RESidual iterative solver:

- $\mathbf{Jv}$  – only matrix-vector products appear
- strong solve – via global dot product
- registers of memory scale linearly with number of Krylov vectors

**Fréchet derivative** using complex number:

$$\mathbf{Jv} \approx \frac{\text{Im}[\mathbf{R}(\mathbf{U} + hvi)]}{h}.$$

## Point-implicit relaxation

$$[\mathbf{A}]^n \Delta \mathbf{U}^n = \left\{ \frac{1}{\Delta t_{\text{local}}} \mathbf{I} - \frac{\partial \mathbf{R}^n}{\partial \mathbf{U}} \right\} \Delta \mathbf{U}^n = \mathbf{R}^n.$$

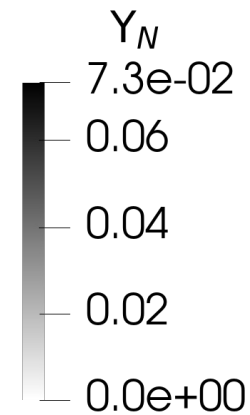
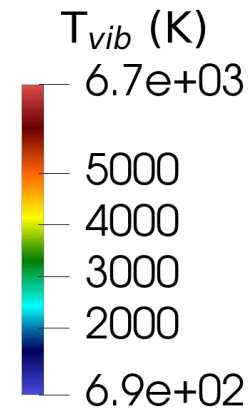
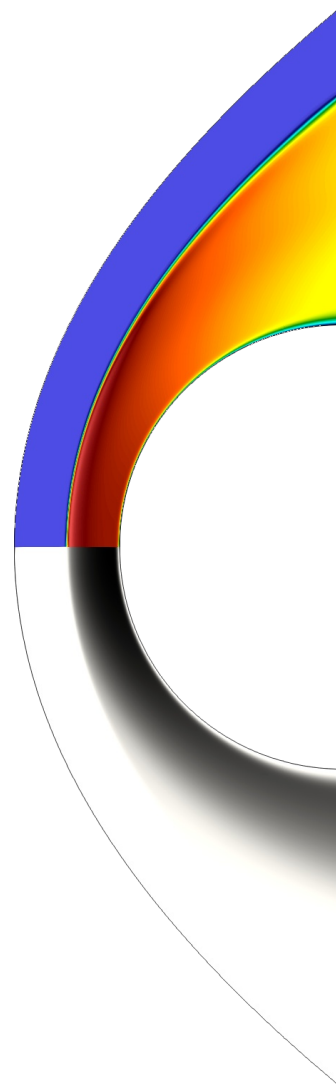
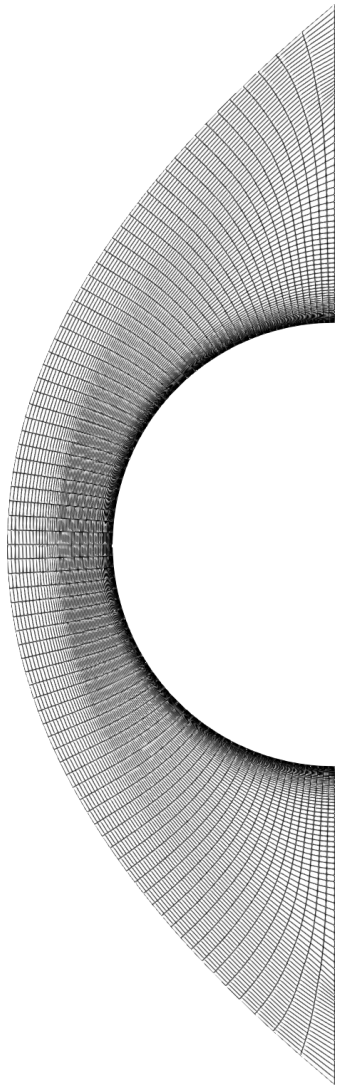
A defect correction type update:

- Jacobian per cell; local effects only
- first-order spatial reconstruction

Other notes:

- local Jacobian formed using complex-step perturbations
- direct solve to give update

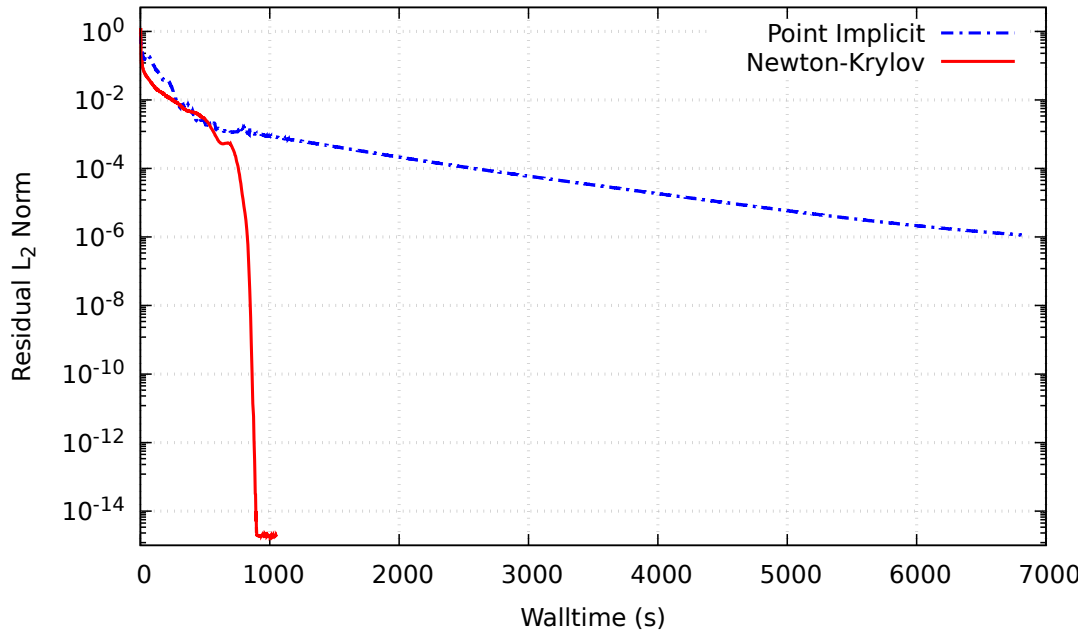
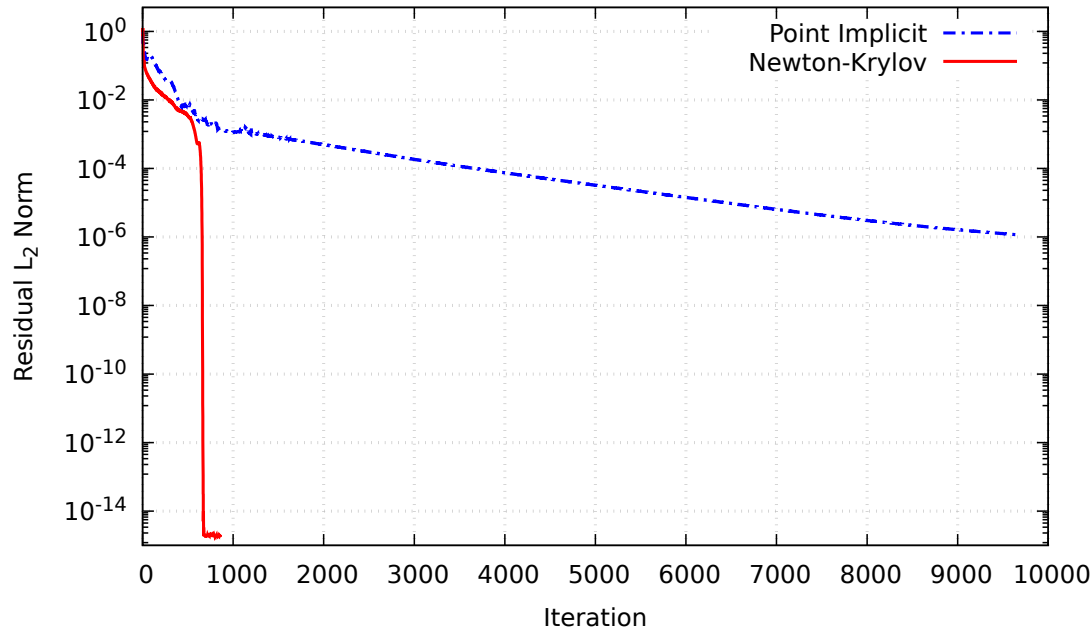
# High-enthalpy cylinder flow: description



- air flow over  $R = 45$  mm cylinder
- free-stream enthalpy: 13.5 MJ/kg
- Park 2-T model
- Fickian diffusion



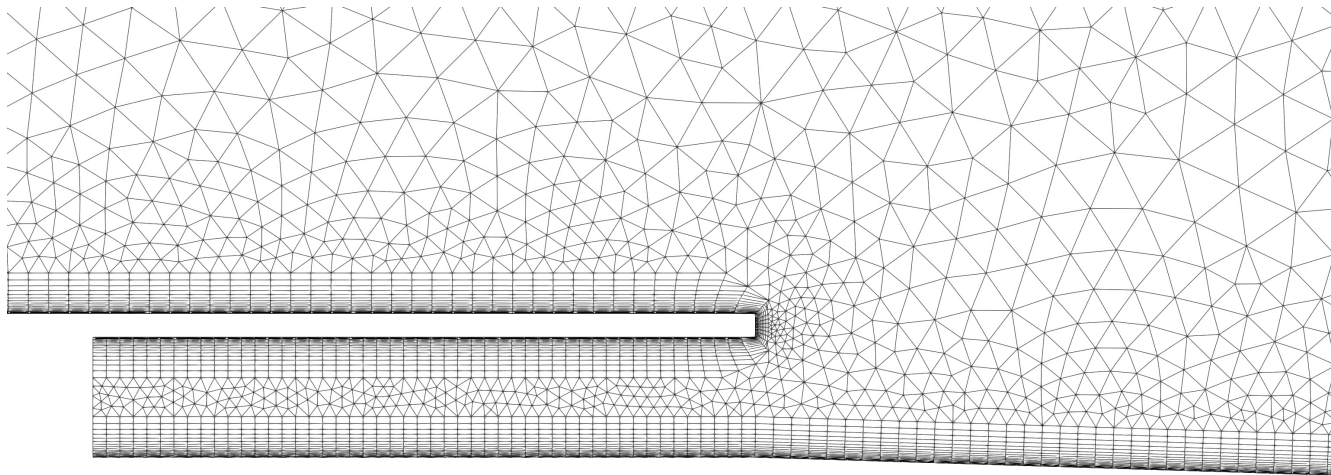
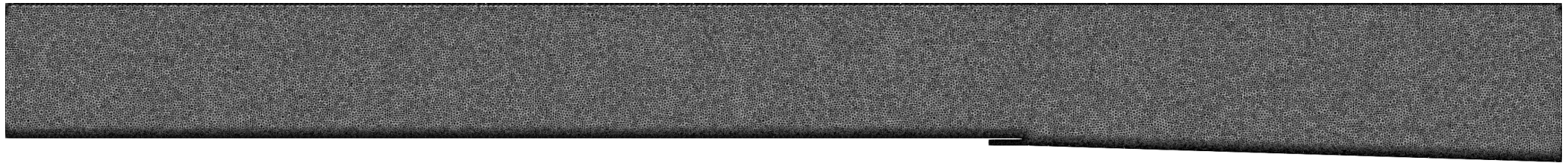
# High-enthalpy cylinder flow: results



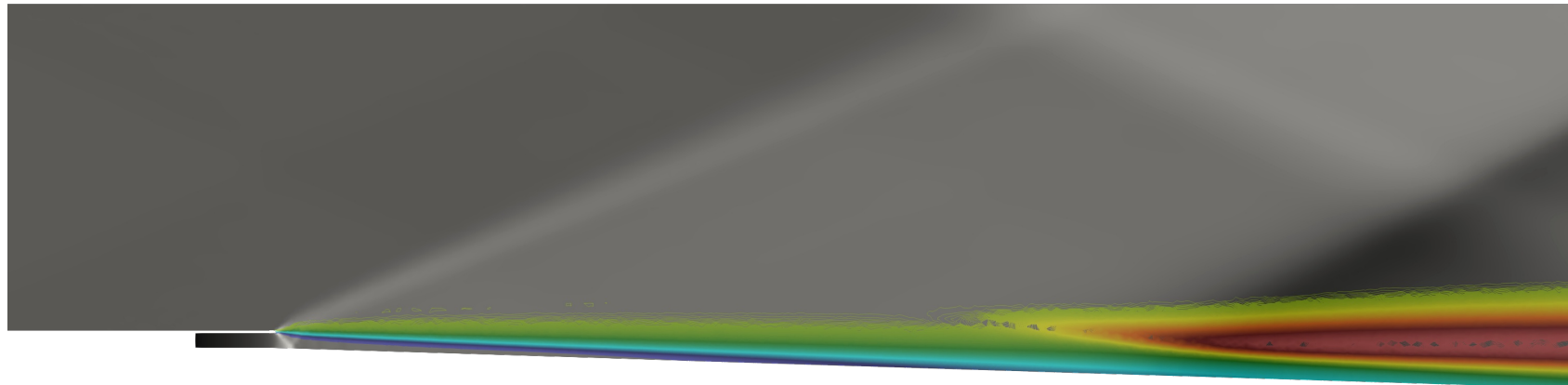
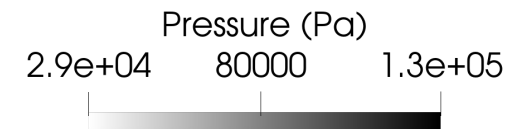
# Supersonic combustor: description



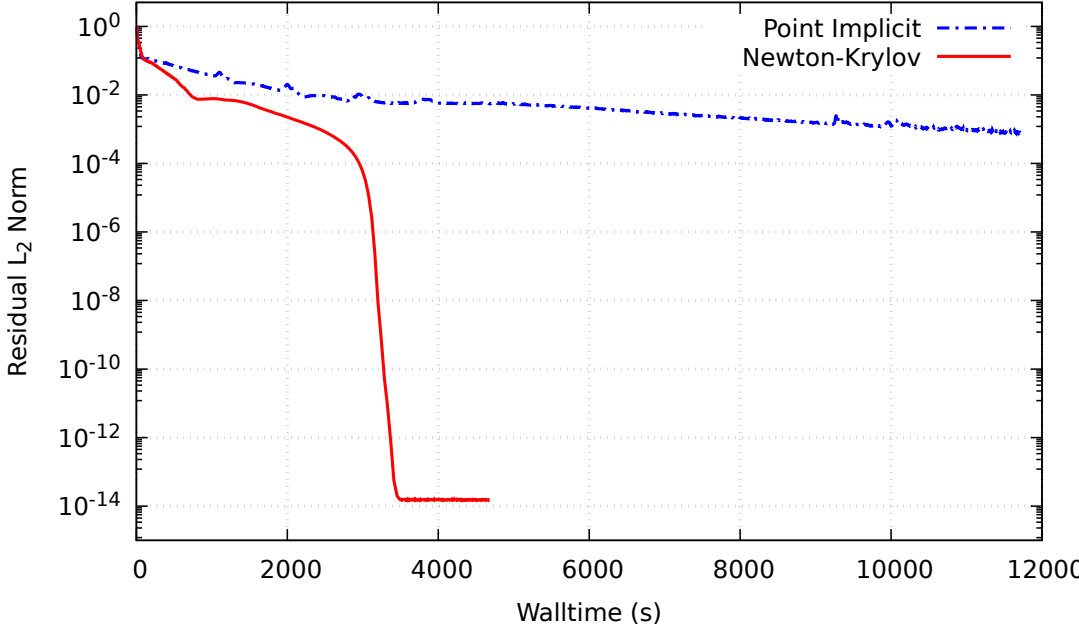
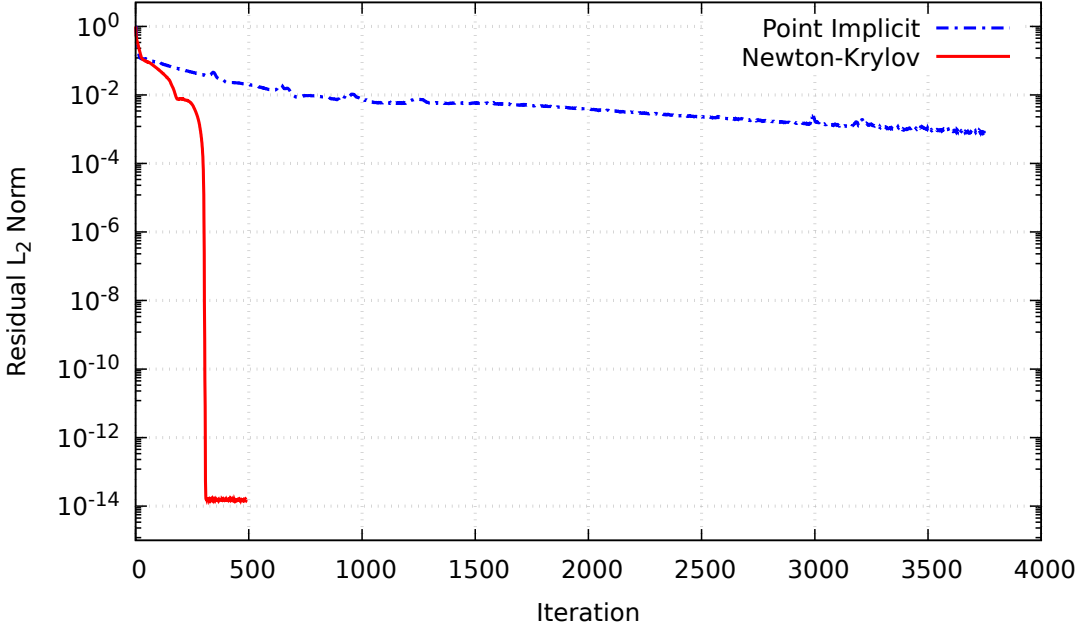
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- main stream: vitiated air
- injected stream: hydrogen
- mixture of thermally perfect gas
- Evans-Schexnayder  $7 \times 8$  H<sub>2</sub>-air combustion



# Supersonic combustor: results

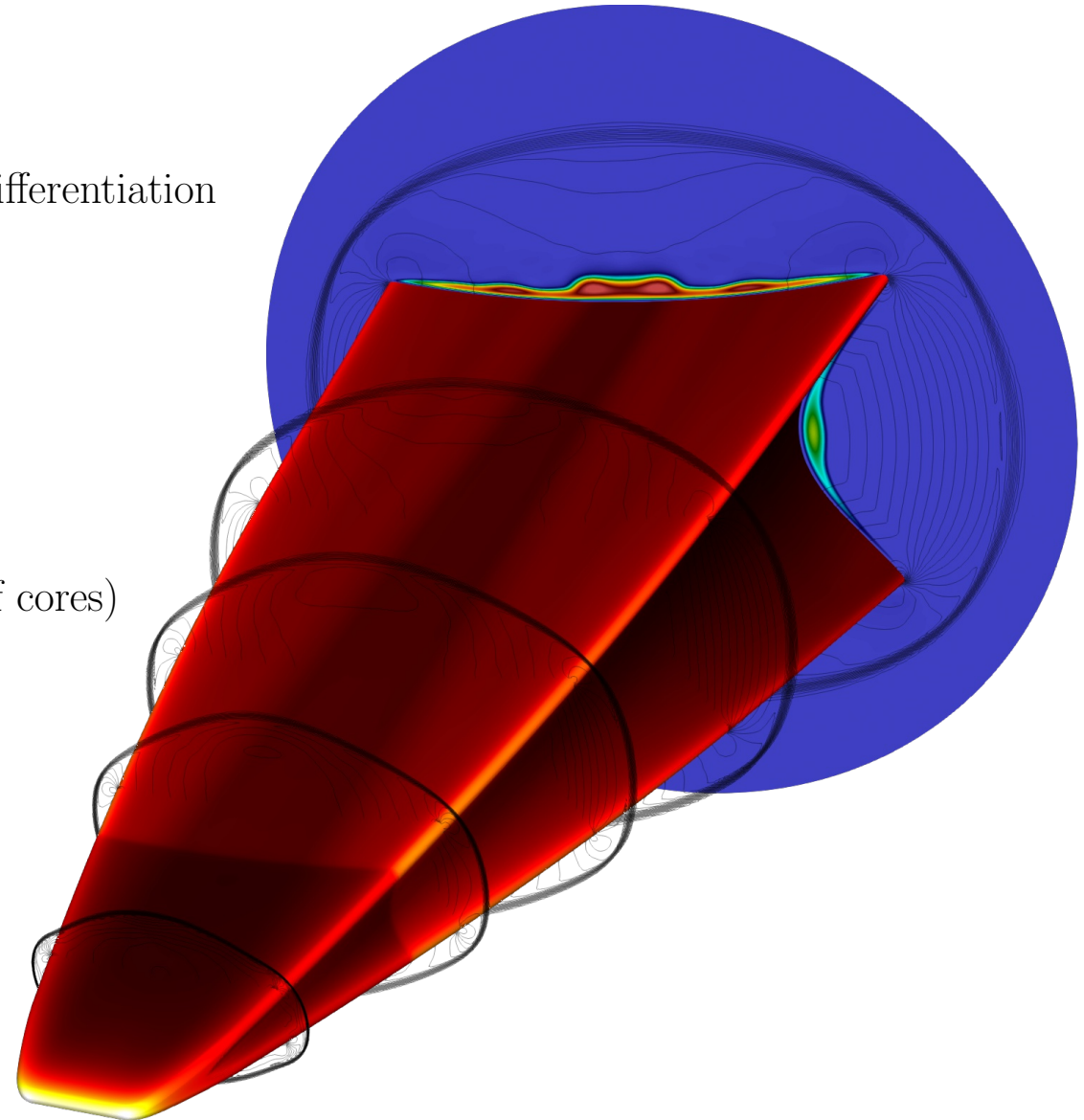


## Summary

- JFNK provides deep convergence for multi-species multi-temperature hypersonic flows
- Key enablers are:
  - GMRES
  - Fréchet derivative with complex-number differentiation
- outperforms a point-implicit relaxation

## Outlook

- method works well in 3D, but
- needs performance optimization /  
algorithm enhancements at large scale (1000s of cores)



# Backup 1: effect of preconditioner selection

