

# Direct Numerical Simulation of Supersonic Reacting Mixing Layers

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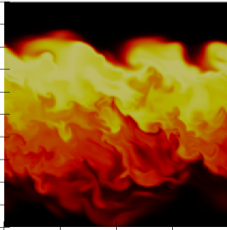
# About Me

- ▶ Postdoctoral Research Fellow @ The Centre for Hypersonics, The University of Queensland, Australia
- ▶ Finished PhD in 2019 with Prof. Vince Wheatley

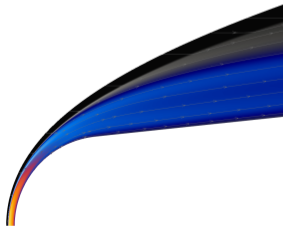
## Things I do:

- ▶ The Gasdynamic Toolkit ([github.com/gdtk-uq/gdtk](https://github.com/gdtk-uq/gdtk))
- ▶ equilibrium-c: Calculator for eq chemistry ([github.com/uqngibbo/equilibrium-c](https://github.com/uqngibbo/equilibrium-c))
- ▶ Simulations:

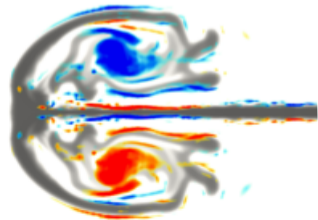
Supersonic Combustion



High Temperature Flows

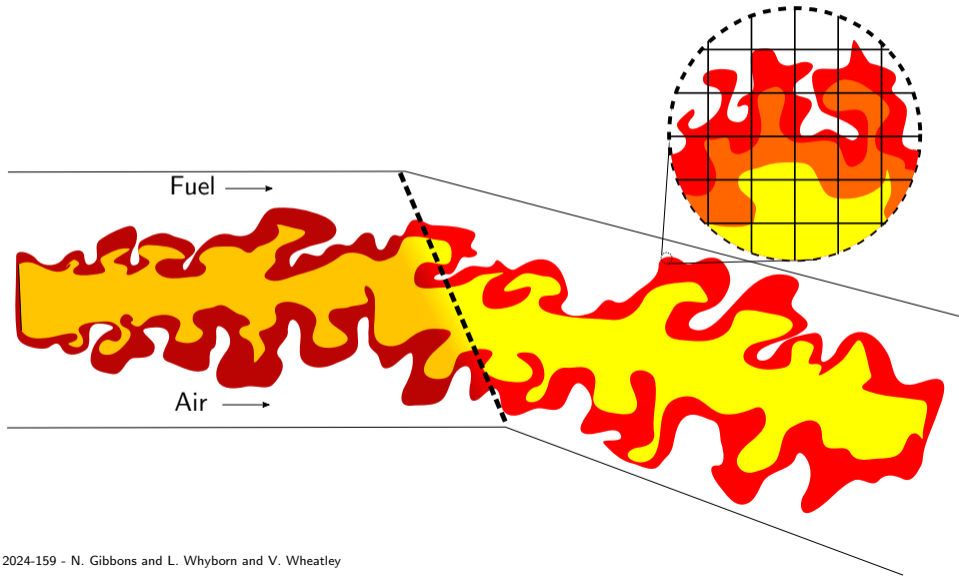


Compressible Turbulence



# Today's Talk: Combustion Models for Compressible Flow

Models are needed to approximate turbulence on (typically) too-coarse CFD grids:



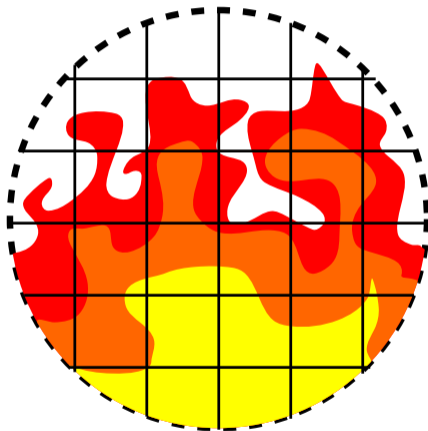
# Today's Talk: Combustion Models for Compressible Flow

$\dot{\omega}$  are the reaction rates:

$$\dot{\omega} = M \sum_r (\nu_{rs}^- - \nu_{rs}^+) \left( k_r^+ \Pi_n [X_n]^{\nu_{rn}^+} - k_r^- \Pi_n [X_n]^{\nu_{rn}^-} \right)$$

Integrate them over the PDF of the species and temperature:

$$\bar{\omega} = \int P(Y'_s, T') \dot{\omega}(Y'_s, T') dY'_s dT'$$

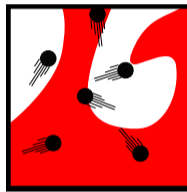


# Today's Talk: Combustion Models for Compressible Flow

$$\bar{\omega} = \int P(Y'_s, T') \dot{\omega}(Y'_s, T') dY'_s dT'$$

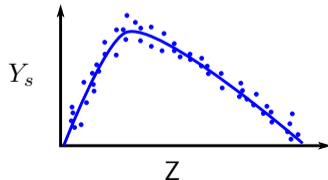
## Multiple Mapping Closure:

- Lagrangian Monte-Carlo method
- Sparse stochastic particles
- Cleary and Klimenko, 2009



## Conditional Moment Closure:

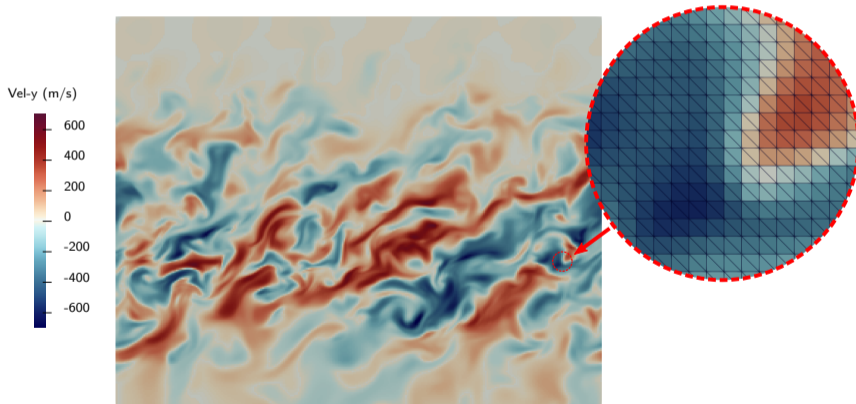
- Use correlations of  $Z$  and  $Y_s$
- Model mixture fraction ( $Z$ ) only
- Klimenko and Bilger, 1999



# Methodology: Direct Numerical Simulations

It is possible to resolve turbulence at low enough Reynolds numbers:

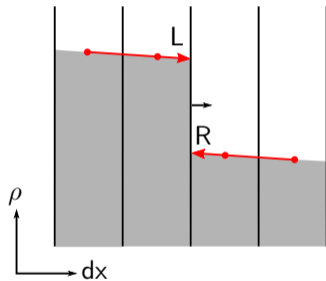
- ▶ In this work: time developing supersonic mixing layer from Gibbons, 2019
- ▶ Simulations using Eilmer, part of UQ's open-source GDTk
- ▶ Needs specialised numerics and high parallel performance



# Methodology: Numerical Method

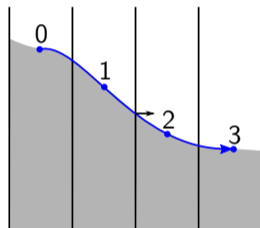
- Inviscid fluxes are computed using two very different kinds of numerical method:

AUSMDV: Wada and Liou, 1994



$$F^c = \frac{1}{2}(\rho u)_f \begin{bmatrix} 1 \\ u \\ H \end{bmatrix}_{L/R} + p_f$$

SPB-ASF: Fisher et al., 2012



$$\mathbf{F}_{div}^c = \frac{1}{12} [-\rho_0 u_0 + 7\rho_1 u_1 + 7\rho_2 u_2 - \rho_3 u_3]$$

$$\mathbf{F}_{prod}^c = \frac{1}{12} [-\rho_0 u_2 - \rho_2 u_0 + 8\rho_1 u_2 + 8\rho_2 u_1 - \rho_1 u_3 - \rho_3 u_1]$$

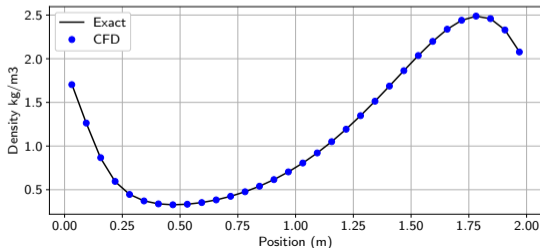
$$F^c = \alpha F_{div}^c + (1 - \alpha) F_{prod}^c$$

# Results: Steepening Wave Problem

- Analytic compressible flow solution from Landau and Lifshitz (1987)

$$u(x) = u_0(x) \sin \left( \pi \left( x - t \left( c_0 + \frac{1}{2} (\gamma + 1) u(x) \right) \right) \right)$$

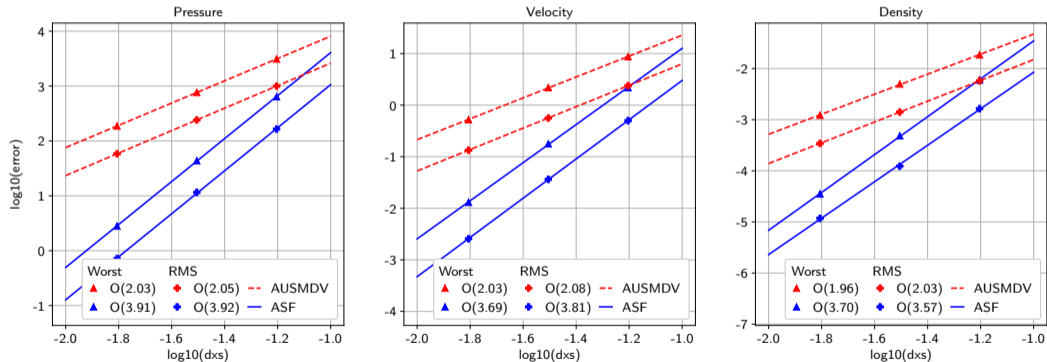
$$p(x) = p_0 \left( \frac{1 + (\gamma - 1)u(x)}{2c_0} \right)^{\frac{2\gamma}{\gamma - 1}} \quad \rho(x) = \rho_0 \left( \frac{1 + (\gamma - 1)u(x)}{2c_0} \right)^{\frac{2}{\gamma - 1}} \quad T(x) = \frac{p(x)}{R\rho(x)}$$





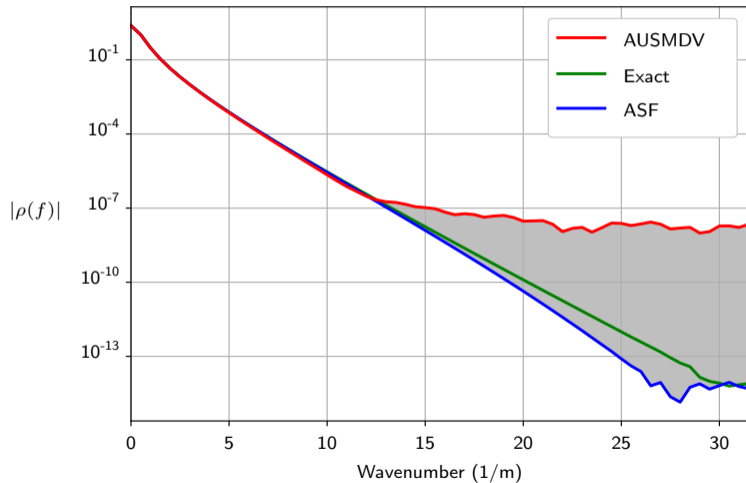
# Results: Steepening Wave Problem

- Error should decrease with  $dx$ , slope in log-log space gives the order:



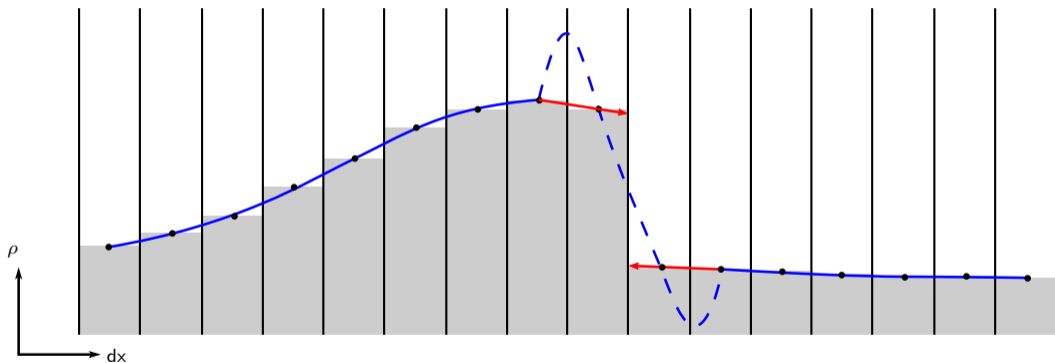
# Results: Steepening Wave Problem

- ▶ Since the solution is periodic, we can analysis error by wavenumber:



# Methodology: Numerical Method

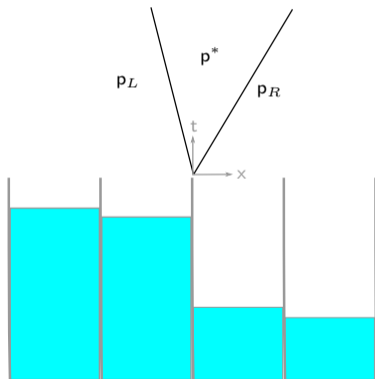
Hybridise the two approaches by detecting discontinuities:



# Methodology: Discontinuity Detection

How do we actually detect discontinuities?

- ▶ Shockwave sensor uses the HLLC "hybrid" wavespeeds: Toro, Spruce, and Speares, 1994



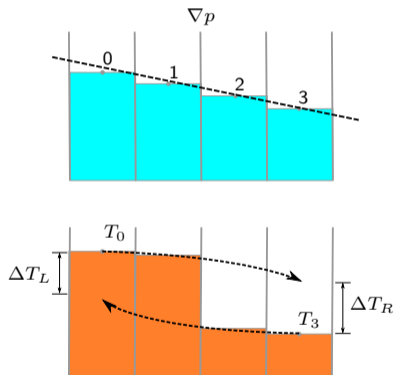
$$p^* = \frac{p_L + p_R}{2} - \frac{(u_R - u_L)}{2} \frac{(\rho_L + \rho_R)}{2} \frac{(a_L + a_R)}{2}$$

$$q_{L/R} = \begin{cases} 1 & p^*/p_{L/R} \leq 1 \\ \sqrt{1 + \frac{\gamma+1}{2\gamma} \left( \frac{p^*}{p_{L/R}} - 1 \right)} & \text{otherwise} \end{cases}$$

$$S_{shock} = \min \left( \frac{q-1}{\mathcal{M}}, 1.0 \right) \quad : \quad q = \max(q_R, q_L)$$

# Methodology: Discontinuity Detection

- Thermal/interface discontinuity detection by isentropic extrapolation:



$$p_R/p_L = \frac{p_0 + p_1 + p_2 + p_3}{4} \pm \frac{3}{2} \frac{-3p_0 - p_1 + p_2 + 3p_3}{10}$$

$$T_R = T_0 \left( \frac{p_R}{p_0} \right)^{(\gamma-1)/\gamma} \quad T_L = T_3 \left( \frac{p_L}{p_3} \right)^{(\gamma-1)/\gamma}$$

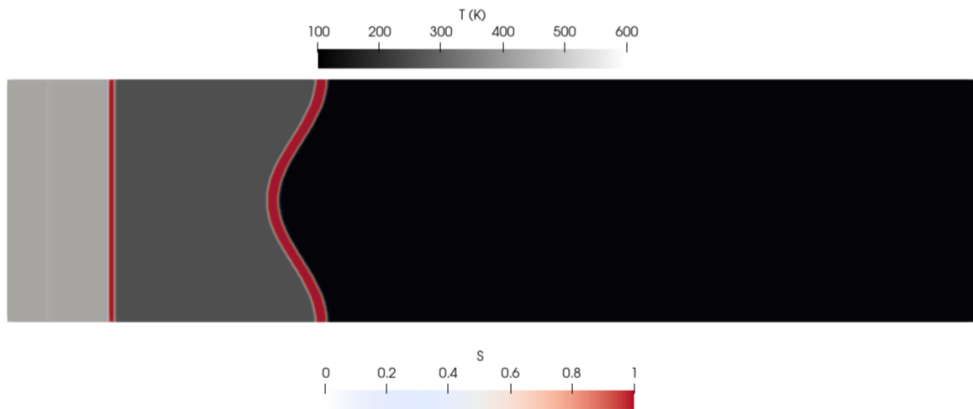
$$\Delta T = \frac{|T_L - T_0|}{T_0} + \frac{|T_R - T_3|}{T_3}$$

$$S_{contact}^T = \frac{1}{2} \tanh(6\Delta T - 2) + \frac{1}{2}$$

# Methodology: Discontinuity Detection

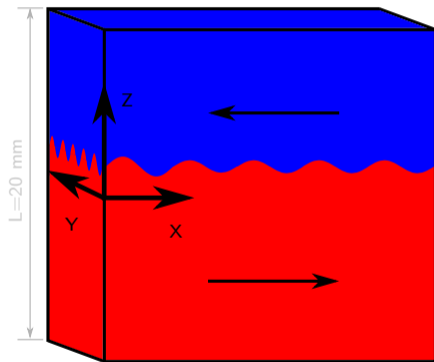
The final value of the shock detector is then the maximum of all three sensors:

$$S = \max(S_{shock}, S_{contact}^p, S_{contact}^T) \quad (1)$$



# Flow Description: Supersonic Mixing Layer

- ▶ Hydrogen conditions taken from Gibbons (2019)
- ▶ Hydrocarbon velocities reduced to match  $M_c = 0.76$



	Hydrogen:	Air:	Hydrocarbon:
p	101,000 (Pa)	p	101,000 (Pa)
T	1,400 (K)	T	1,400 (K)
u	-1,168.89 (m/s)	u	-500 (m/s)
$Y_{N_2}$	0.767	$Y_{N_2}$	0.767
$Y_{O_2}$	0.233	$Y_{O_2}$	0.233
Fuel:			
p	101,000 (Pa)	p	101,000 (Pa)
T	1,500 (K)	T	1,500 (K)
u	1,665.89 (m/s)	u	634.3 (m/s)
$Y_{H_2}$	1.0	$Y_{C_2H_4}$	1.0

Figure 1: Supersonic Mixing Layer Initial Conditions. (Interface perturbations are exaggerated.)

# Methodology: Eilmer

Eilmer is our high-speed flow research simulation code:

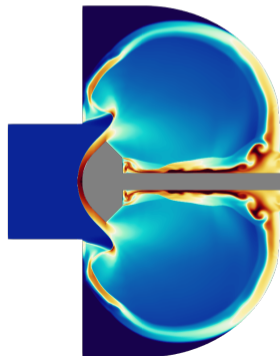
- ▶ Developed at UQ by Rowan Gollan, Peter Jacobs, Kyle Damm, and me!
- ▶ Used for studies of re-entry flows, combustion, compressible flow and more
- ▶ Part of the Gasdynamic Toolkit (GDTk)

Features:

- ▶ Free and open-source
- ▶ Parallel scaling to thousands of cores
- ▶ Build structured/unstructured grids or read them in
- ▶ Extensively validated against hypersonic experiments
- ▶ Very capable turbulence, chemical and thermal nonequilibrium models

Website: [gdtk.uqcloud.net](http://gdtk.uqcloud.net)

Paper: [doi.org/10.1016/j.cpc.2022.108551](https://doi.org/10.1016/j.cpc.2022.108551)





# Numerical Details and Initial Condition

Slide of technical details for posterity:

- ▶ This talk will be on [gdtk.uqcloud.net/docs/pub-n-pres/presentations](http://gdtk.uqcloud.net/docs/pub-n-pres/presentations)

Initial Condition		
$L$	20 (mm)	Domain Size
$A$	1/100 L	Perturbation Amplitude
$k$	6	Perturbation Wave Number
$D$	1/6 L	Vertical Offset
$\zeta$	3/100 L	Smearing Factor

$$\psi = f\psi_{air} + (1 - f)\psi_{fuel}$$

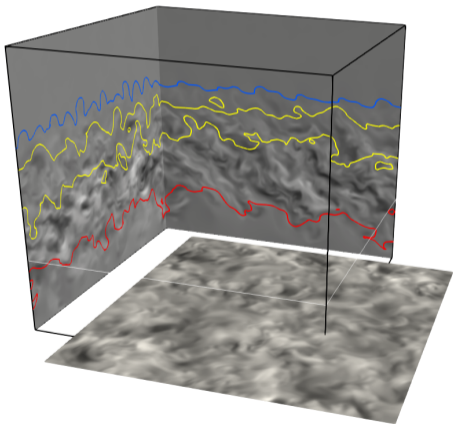
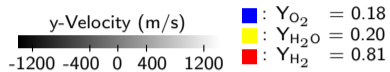
$$f = \frac{1}{2} \tanh\left(\frac{6z'}{\zeta}\right) + \frac{1}{2}$$

$$z' = z - A\left(\sin\left(\frac{2\pi kx}{L}\right) + \sin\left(\frac{2\pi ky}{L}\right)\right) + D$$

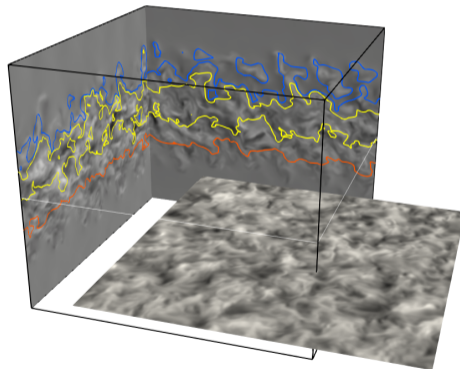
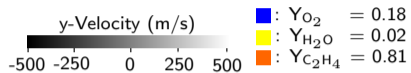
Solver Settings	
Eilmer Rev-id:	71d0040e
Fluid Time-Adv:	RK3 Explicit @ CFL=0.5
Chem Time-Adv:	RK45 Adaptive
Fluxes:	AUSMDV/SBP-ASF
n Smooth:	4
$\mathcal{M}$ :	0.1
Cell Count:	299 <sup>3</sup>
Hydrogen Reactions:	Jachimowski, 1992
Ethylene Reactions:	Baurle and Eklund, 2002
Max Time:	100 $\mu$ s
RKF errTol	1e - 5

# Results: Flow overview @ 40 $\mu$ s

## Hydrogen

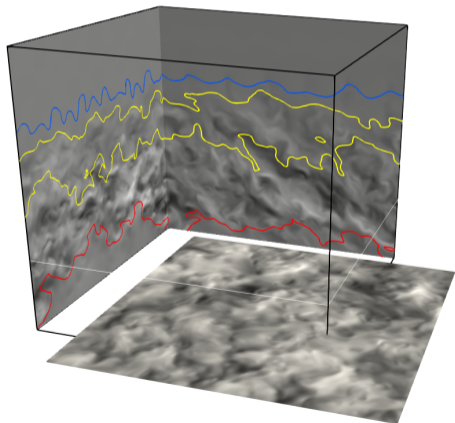
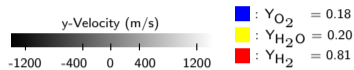


## Hydrocarbon

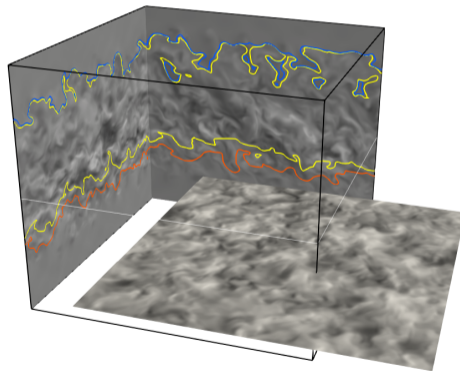
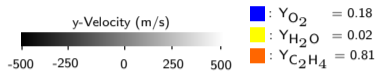


# Results: Flow overview @ $60 \mu s$

## Hydrogen

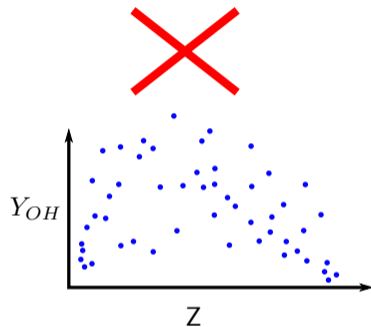
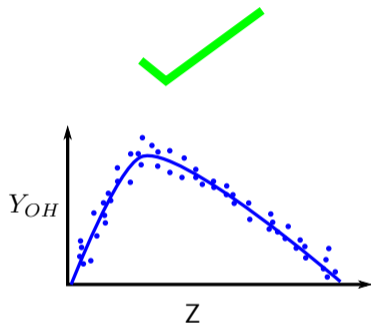


## Hydrocarbon



# Results: Conditional Statistics

Our goal is to develop extend Conditional Moment Closure for highly compressible flow:



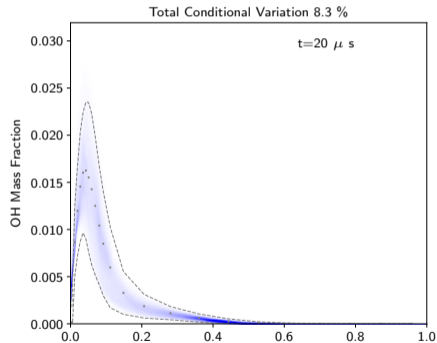
- The mixture fraction  $Z$  is the mass fraction of gas from the fuel stream:

$$Z = \sum_s Y_s \left( a_s^H \frac{M_H}{M_s} + a_s^C \frac{M_C}{M_s} \right) \quad (2)$$

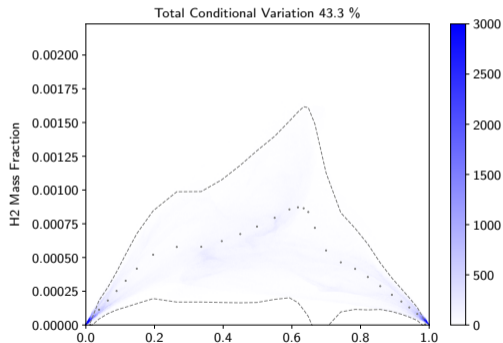
# Results: Conditional Statistics

- ▶ Intermediate species OH and H<sub>2</sub> follow the Z curve at late times:

## Hydrogen



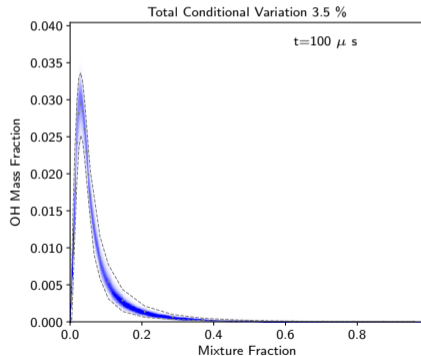
## Hydrocarbon



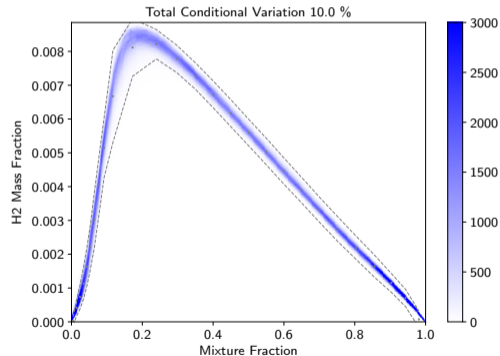
# Results: Conditional Statistics

- ▶ Intermediate species OH and H<sub>2</sub> follow the Z curve at late times:

## Hydrogen



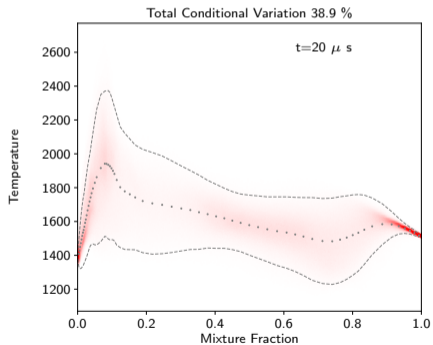
## Hydrocarbon



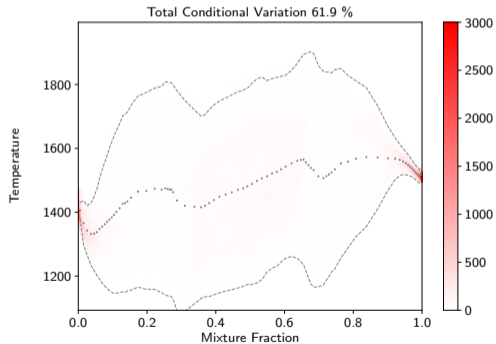
# Results: Conditional Statistics

- Temperature is pretty bad initially:

## Hydrogen



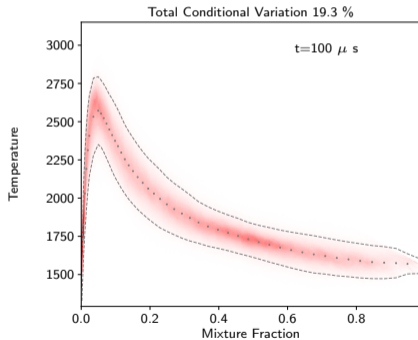
## Hydrocarbon



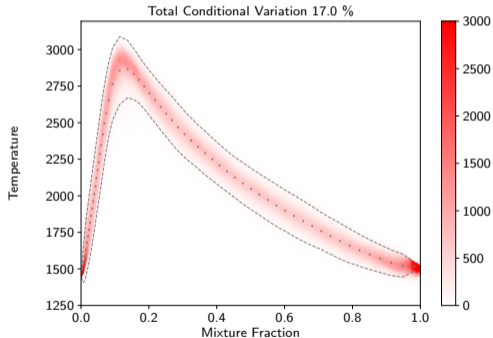
# Results: Conditional Statistics

- ▶ Even at late times it has a fair bit of variation:

## Hydrogen



## Hydrocarbon





# Conclusions and What's Next?

- ▶ Numerical method is holding water for reacting DNS calculations
- ▶ Have plans for a larger simulation with shocks in it
- ▶ Can then do statistical analysis of the whole flowfield for CMC

# References I

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