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4 Supplementary Materials for
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6 **Plastic waste discharge to the global ocean constrained by seawater observations**

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33 **Supplementary Discussion**

34 Inclusion of seawater observations

35 Supplementary Table 8 lists the observed surface ocean plastic abundance data used in this
36 study. Isobe et al. compiled a multilevel dataset that includes almost all available ocean plastic
37 abundance data so far¹. The Isobe database includes a total of 9959 data points obtained by
38 Neuston net, WP2 net, Manta net, Bango net, and Plankton net. The identification method
39 includes visual identification, FTIR (Fourier transform infrared spectrophotometer), and Raman
40 spectroscopy. There is a large discrepancy among data obtained with a different method^{2,3}. The
41 risk of clogging and uncertainty in sample volumes also depends on the mesh size of the net and
42 the flow conditions³. Visual inspection is known to lead to an overestimation of the particle
43 count because 20-70% of the particles identified visually as plastics might be of other chemical
44 compositions, e.g., coal ash, especially for the particle smaller than 500 μm ^{4,5}. However, visual
45 identification misses the transparent and small microplastics thus underestimating the plastic
46 concentrations². The data obtained by different methodologies are thus generally not comparable
47 with each other. More importantly, different methodologies are used in different studies covering
48 different ocean basins. A mixture of data obtained by different methodologies may distort the
49 real spatial pattern of surface ocean plastic abundance and reduce the reliability of the
50 comparison between simulations and observations. There is a trade-off between “more data” and
51 “ghost spatial pattern” arising from different measurement methodologies. Therefore, we use
52 only the dataset obtained by Neuston net and the visual identification method due to its large
53 sampling number and spatial coverage. The number of such data is 7431 (Supplementary Table
54 8), accounting for 75% of the Isobe database. The data in different ocean basins are also
55 comparable due to similar methodology.

56 All the data used in this study are reported as numerical concentrations (N), which are transferred
57 to mass concentrations (M) following Cozar et al.⁶:

$$58 \quad \log M(g \cdot km^{-2}) = 1.21 \times \log N(items \cdot km^{-2}) - 3.99 \quad (1)$$

59 and are compared with modeled mass concentrations of plastics in the surface ocean. Such a
60 transfer does not change the number of independent measurements used in this study. The
61 conversion bears uncertainty but the uncertainty is reduced due to the large sampling number⁷.
62 The item-mass conversion factors of all observed concentrations range from 1.3×10^{-5} to 2.4×10^3
63 g per item, with a mean value of 31 g per item. However, mass concentrations (or total mass) are
64 more comparable with plastic emission inventories that are also in a mass unit. Moreover, the
65 modeled number concentrations are prone to larger uncertainties due to the fragmentation
66 process, which is mass-conservative but could greatly change the number concentrations⁶.

67 **Supplementary Methods**

68 Other sources of plastics to the ocean than MPW

69 There are other potential sources contributing to the ocean plastics beyond riverine discharge,
70 coastal erosions, and marine sources that are considered in this study. One potential source is
71 atmospheric transport and deposition. The total deposition of plastics to ocean surfaces from land
72 sources is 13 kilo Mt yr^{-1} , much smaller than the three sources mentioned in the main text.
73 Moreover, there is a suggested net transport of 9 kilo Mt yr^{-1} plastics from ocean to land, i.e. the
74 loss of sea surface ocean plastics to the atmosphere (via mechanical processes similar to sea salt

75 emissions) surpasses that is deposited to the ocean⁸. Another source is direct wastewater to ocean
 76 by coastal population (other wastewater enters the ocean via rivers, hence being considered in
 77 this study), which is estimated about 0.44 kilo Mt yr⁻¹, even smaller than what we already
 78 considered⁹. Other plastic sources than mismanaged plastic waste include unintentional plastic
 79 emissions, such as fibers from textiles, tire wear particles, and lost resin pellets. We assume that
 80 they have been included in the riverine inventories of plastic waste discharge, as these
 81 inventories were built upon riverine measurements that cover all plastic types. Natural disasters
 82 are also potential significant sources. For example, the Fukushima earthquake and tsunami in
 83 March, 2011 released ~20 million Mt of debris to the ocean¹⁰. However, the emission of plastic
 84 waste in such events is poorly quantified at global scale, and its contribution to the ocean plastics
 85 is rather small given its unusual and episodic nature.

86 Stokes drift

87 We take the estimated Stokes drift velocity from the GlobCurrent and apply it to all the plastic
 88 tracers in our model¹¹. The data are available between 1990 and 2015, with a time resolution of 3
 89 hours. We calculate a 26-year average of the Stokes drift velocity for each month. In this way, 12
 90 months of Stokes drift velocity is achieved and cycled in the model for the whole simulation
 91 period. The strongest Stokes drift is simulated in the Southern Ocean and the high-latitude ocean
 92 in the northern hemisphere where plastic concentrations are relatively low (Supplementary Fig.
 93 6), consistent with previous results¹². The modeled plastic accumulation in the subtropical gyres
 94 is moved westward slightly by Stokes drift, while plastics in the Southern Ocean are moved
 95 eastward.

96 Sinking and rising

97 The sinking/rising rate of plastics depends on its density. Plastic particles in our model are
 98 treated as spheres. At steady state, the forces acting on plastic particles are balanced:

$$99 \quad \mathbf{F}_D + \mathbf{F}_g + \mathbf{F}_b = 0 \quad (2)$$

100 where \mathbf{F}_D is vertical dragging force, \mathbf{F}_g is gravity, and \mathbf{F}_b is buoyancy. These forces are calculated
 101 as:

$$102 \quad \mathbf{F}_g = V_p \rho_p \mathbf{g} \quad (3)$$

$$103 \quad \mathbf{F}_b = -V_s \rho_s \mathbf{g} \quad (4)$$

$$104 \quad \mathbf{F}_D = -\frac{1}{2} C_D (\text{Re}_s) A_p \rho_s \frac{(\mathbf{w} - \mathbf{w}_s)^3}{|\mathbf{w} - \mathbf{w}_s|} \quad (5)$$

105 where V_p is the volume of the particle, while V_s is the volume of the particle that is submerged in
 106 seawater ($V_p = V_s$ in this case, but $V_p > V_s$ for floating particles with zero sinking/rising velocity
 107 relative to the seawater, e.g., unbiofouled PP and PE). C_D is the coefficient of dragging, which is
 108 a function of the Reynolds number (Re) of a certain motion of a fluid. A_p is the horizontal
 109 sectional area of a particle, ρ_s is the density of seawater, ρ_p is the mean density of a particle, \mathbf{w}
 110 is the vertical velocity of the particle, \mathbf{w}_s is the vertical velocity of seawater, and \mathbf{g} is the gravity
 111 acceleration.

112 Based on Supplementary Equation (2)–(5), we get $(\mathbf{w} - \mathbf{w}_s)^2$:

$$113 \quad (\mathbf{w} - \mathbf{w}_s)^2 = \frac{4|\mathbf{g}|d(\rho_p - \rho_s)}{3C_D(\text{Re}_s)\rho_s} \quad (6)$$

114 where d is Stokes diameter of a particle, and C_D is calculated as¹³:

115
$$C_D(\text{Re}) = \begin{cases} 24 \text{Re}^{-1} & \text{Re} \leq 0.3 \\ 18.5 \text{Re}^{-0.6} & 0.3 < \text{Re} \leq 1000 \\ 0.44 & 1000 < \text{Re} \leq 20000 \end{cases} \quad (7)$$

116 Re_s is the Re of seawater and is calculated as:

117
$$\text{Re}_s = \frac{d \rho_s |\mathbf{w} - \mathbf{u}_s|}{\mu_s} \quad (8)$$

118 Based on Supplementary Equation (6) (7), we get $\mathbf{w} - \mathbf{w}_s$:

119
$$\mathbf{w} - \mathbf{w}_s = \begin{cases} \frac{d^2 g(\rho_p - \rho_s)}{18\mu} & \text{Re} \leq 0.3 \\ \frac{0.153 d^{1.143} [g(\rho_p - \rho_s)]^{0.714}}{\rho_s^{0.286} \mu^{0.429}} & 0.3 < \text{Re} \leq 1000 \\ 1.74 \left(\frac{dg(\rho_p - \rho_s)}{\rho_s} \right)^{\frac{1}{2}} & 1000 < \text{Re} < 200000 \end{cases} \quad (9)$$

120 Supplementary Equation (6) is a piecewise function. The three conditions of different Re are all
 121 possible in reality because of the variety of particles, but it is hard to know which range of
 122 Supplementary Equation (6) should be used in a certain situation, since Re should be calculated
 123 directly by sinking velocity \mathbf{w} , which is unknown here.

124 Notice that Supplementary Equation (7) can be represented by:

125
$$C_D = \frac{a}{\text{Re}^b} \begin{cases} a = 24, b = 1 & \text{Re} \leq 0.3 \\ a = 18.5, b = 0.6 & 0.3 < \text{Re} \leq 1000 \\ a = 0.4, b = 0 & 1000 < \text{Re} < 200000 \end{cases} \quad (10)$$

126 Combine Supplementary Equation (6) (8) (10) and eliminate $|\mathbf{w} - \mathbf{u}_s|$ and C_D :

127
$$\text{Re} = \left(\frac{4}{3a} \right)^{\frac{1}{2-b}} \left(d^3 \frac{\rho_s g(\rho_p - \rho_s)}{\mu^2} \right)^{\frac{1}{2-b}} \quad (11)$$

128 Define K :

129
$$K = d^3 \frac{\rho_s g(\rho_p - \rho_s)}{\mu^2} \quad (12)$$

130 Then:

131
$$\text{Re} = \begin{cases} 0.0556K & \text{Re} \leq 0.3 \\ 0.072K^{\frac{5}{7}} & 0.3 < \text{Re} \leq 1000 \\ 1.74K^{\frac{1}{2}} & 1000 < \text{Re} < 200000 \end{cases} \quad (13)$$

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$$\mathbf{w} - \mathbf{w}_s = \begin{cases} \frac{d^2 g(\rho_p - \rho_s)}{18\mu} & K \leq 5.4 \\ \frac{0.153 d^{1.143} [g(\rho_p - \rho_s)]^{0.714}}{\rho_s^{0.286} \mu^{0.429}} & 5.4 < K \leq 24 \\ 1.74 \left(\frac{dg(\rho_p - \rho_s)}{\rho_s} \right)^{\frac{1}{2}} & K > 24 \end{cases} \quad (14)$$

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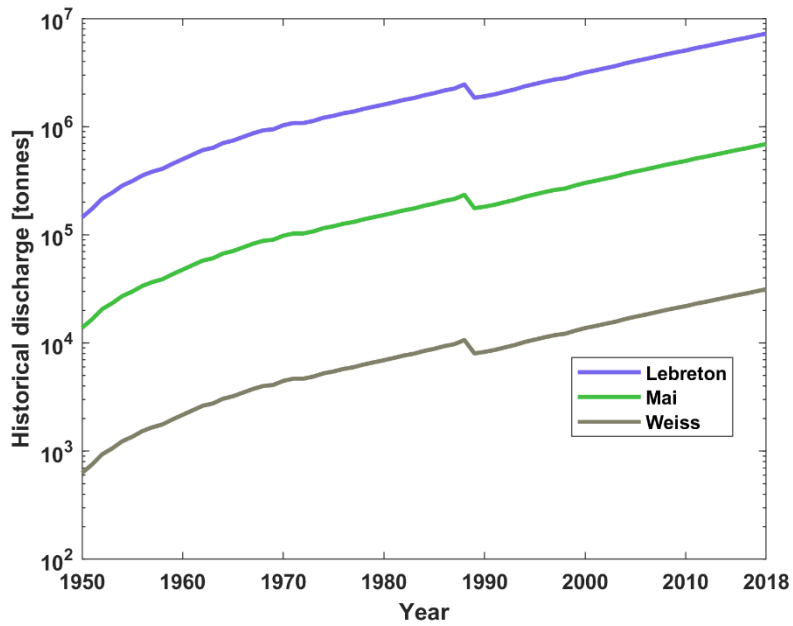
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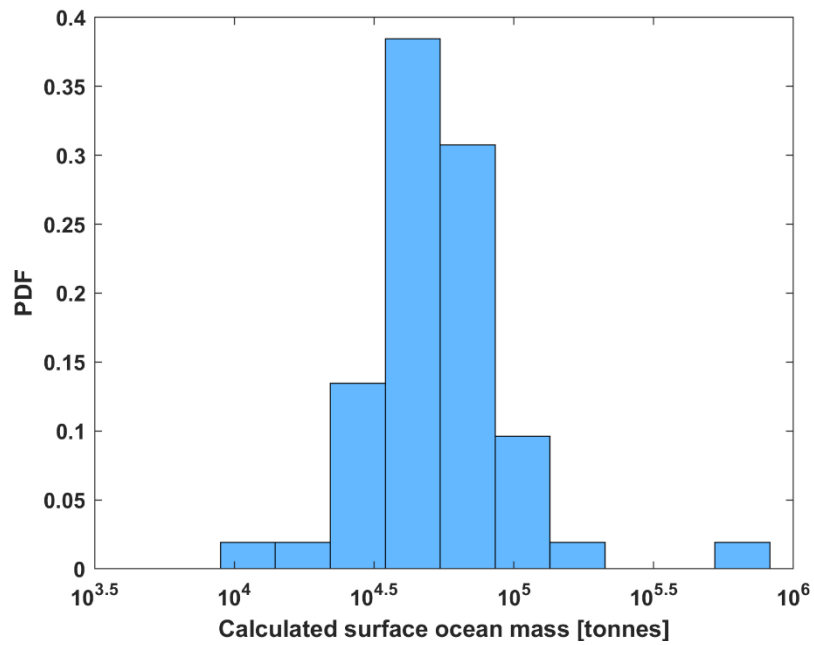
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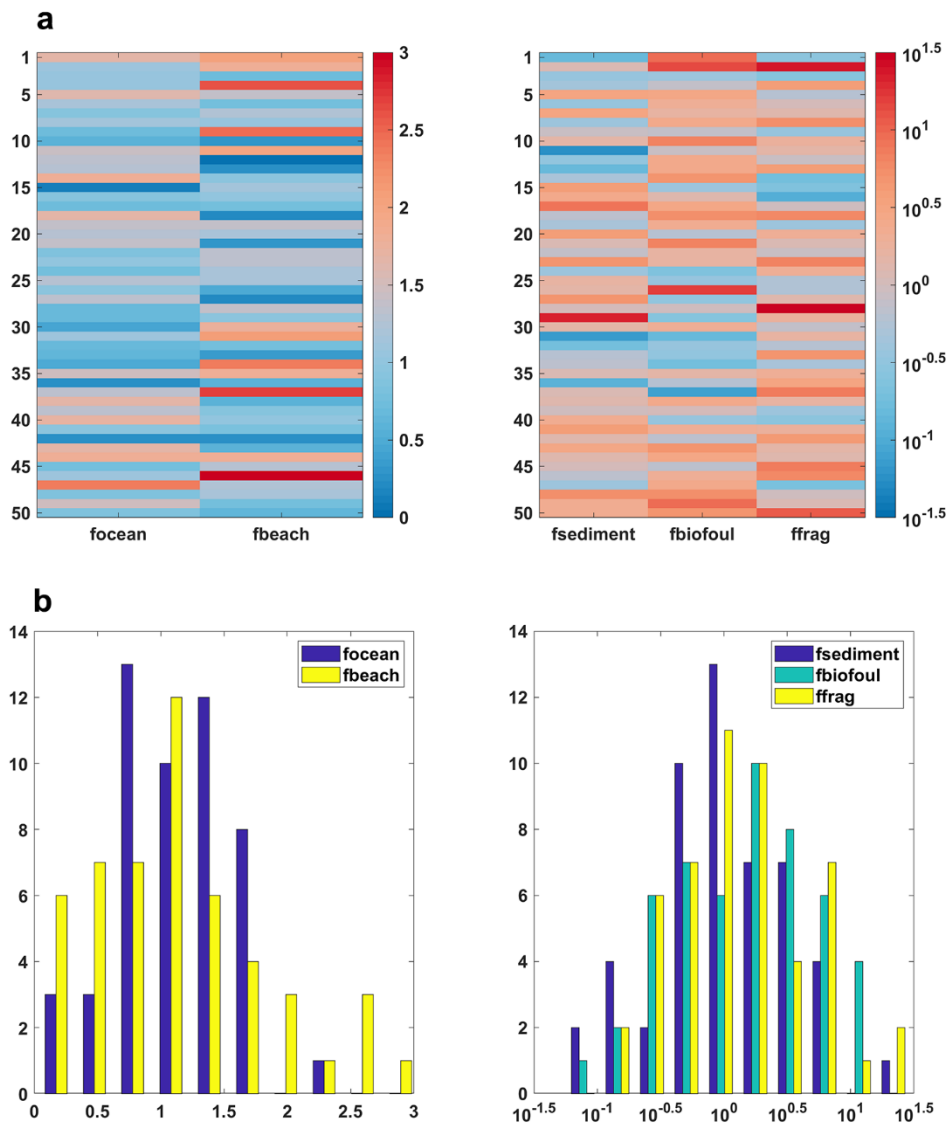
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 142 **Supplementary Fig. 1: The historical trends of global total plastic emissions during 1950-**
 143 **2018 for the High (Lebreton), Middle (Mai), and Low (Weiss) scenarios.** The abrupt decrease
 144 in the 1980s is associated with the MARPOL Convention that bans the dumping of waste from
 145 ships.

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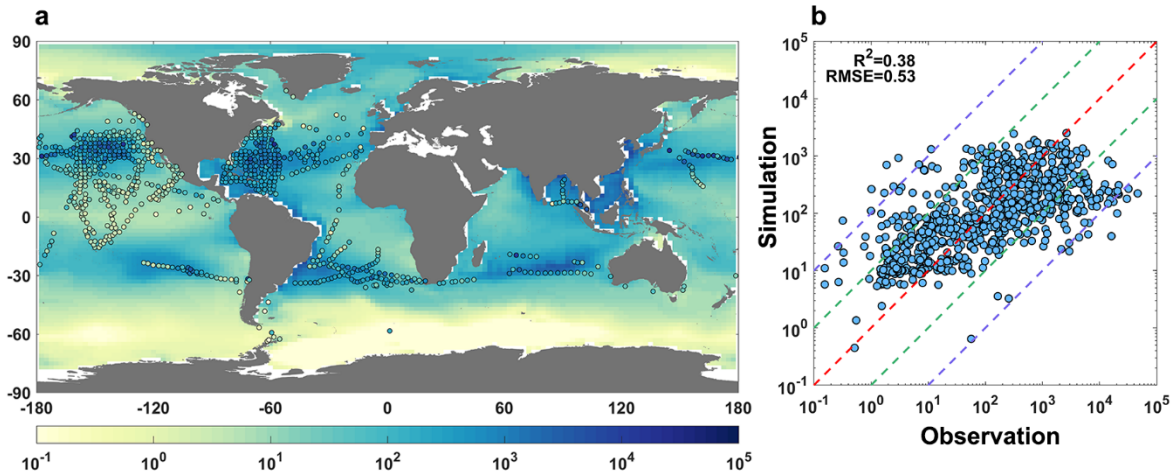
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 152 **Supplementary Fig. 2: Probability distribution function of the calculated surface ocean**
 153 **plastic mass.** The results are from the ensemble members ($N = 52$) driven by the Middle
 154 emission scenario.

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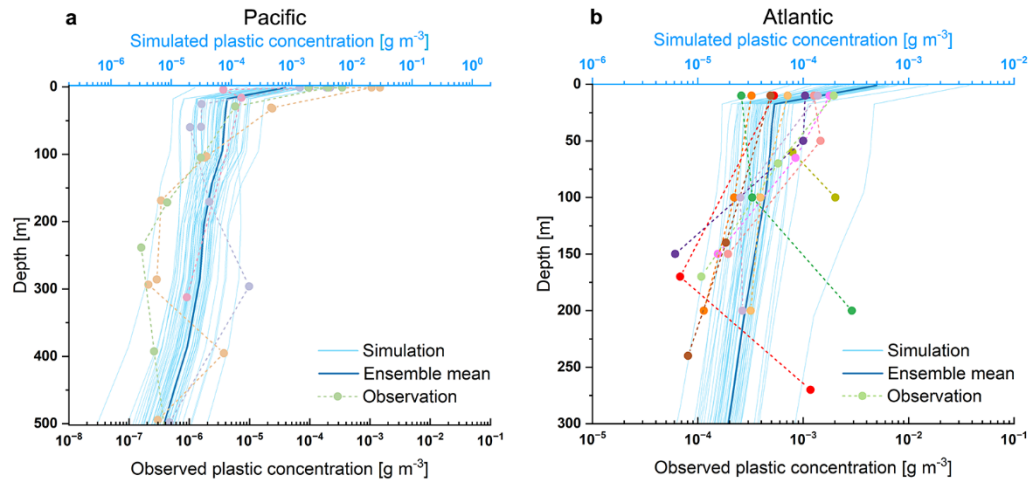


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 159 **Supplementary Fig. 3: Parameters of the model ensemble ($N = 50$).** **a** parameter values. **b**
 160 frequency distributions of the values. Parameters are represented as the ratio to the corresponding
 161 values in the test case simulation (Table 1), including *focean*: fraction of marine discharge to the
 162 total discharge; *fbeach*: beaching rate; *fsediment*: sedimentation rate; *fbiofoul*: biofouling rate;
 163 *ffrag*: fragmentation rate.

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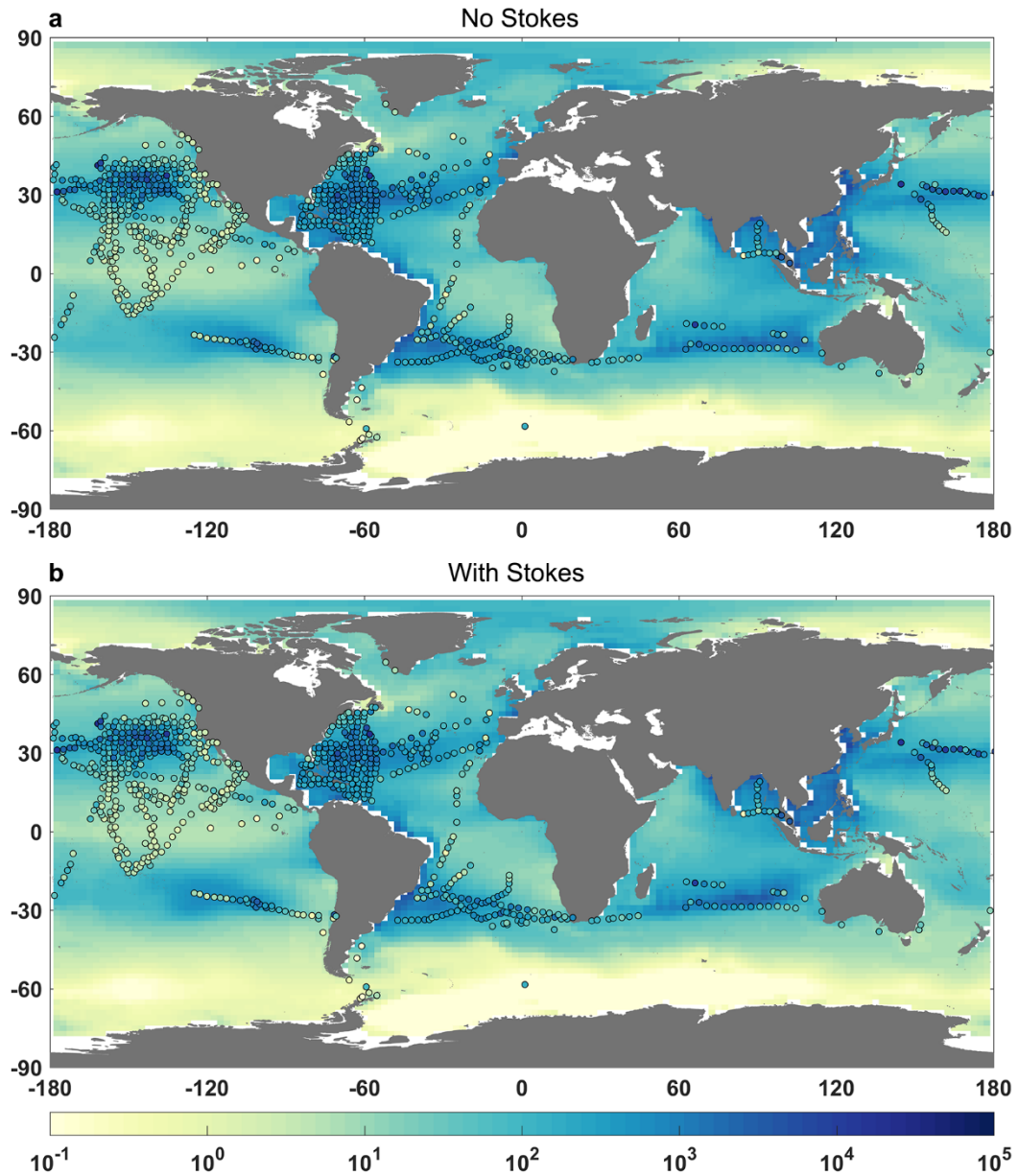


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 168 **Supplementary Fig. 4: Comparison between observed and modeled surface ocean plastic**
 169 **mass concentrations driven by the best-estimate emissions.** The background colors in panel **a**
 170 are the modeled results, while the circles are observations. The dashed lines in panel **b** are 100:1,
 171 10:1, 1:1, 1:10, and 1:100. All the concentrations, and the calculation of R^2 and RMSE are in a
 172 base 10 logarithmic scale with a unit of g km^{-2} . The best-estimate emission is close to the middle
 173 emission scenario and the simulated concentrations in panel **b** are just slightly higher than those
 174 in Fig. 2e.
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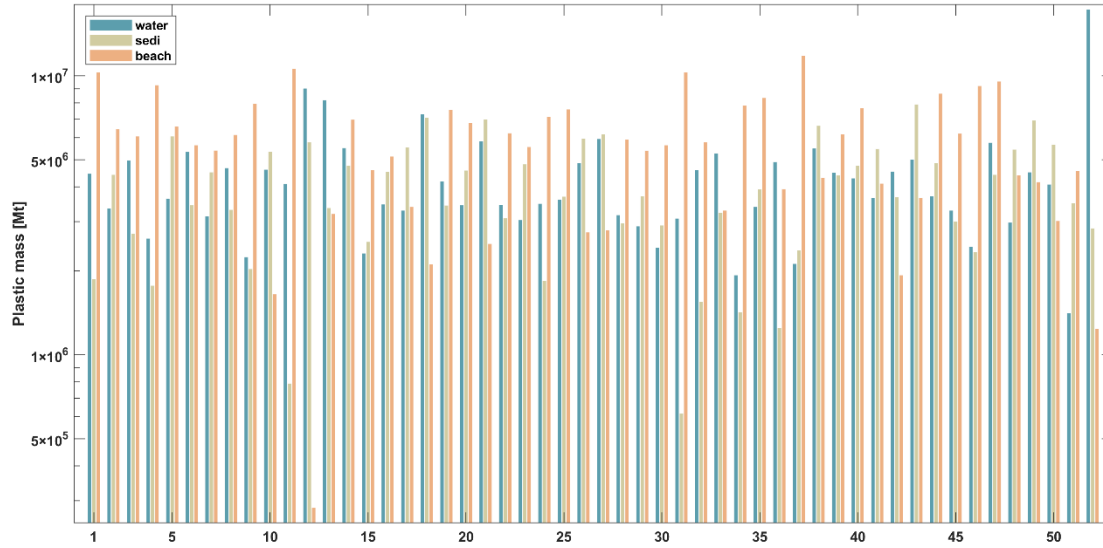
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 177 **Supplementary Fig. 5: Comparison between observed and modeled vertical profile of**
 178 **plastic mass. a Pacific. b Atlantic Ocean.** The dash lines indicate individual observed profiles
 179 with the filled-colored circles representing sampling depths. The light blue solid lines are the
 180 mean plastic mass concentrations over the sampling sites by the 52 member models under the
 181 middle emission scenario (other emission scenarios simulate higher or lower concentrations but
 182 with similar vertical trends), while the dark blue solid lines are the ensemble means. The
 183 observations are from Egger et al. (2020) and Pabortsave and Lampitt (2020) for the Pacific and
 184 Atlantic Ocean, respectively^{14,15}.

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 188 **Supplementary Fig. 6: The modeled spatial pattern of surface plastic abundance. a** Without
 189 Stokes drift. **b** With Stokes drift. Compared with panel **a**, Stokes drift slightly changes the spatial
 190 pattern in panel **b**.

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194 **Supplementary Fig. 7: Modeled amount of plastics in the water column, sediments, and**
 195 **beaches.** The 52 ensemble members are driven by the middle emission scenario. The parameters
 196 of the model members are listed in Supplementary Table 7.
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212 **Supplementary Table 1.** Mapping of emission inventory to the size bins of our model

Emission inventory	Model tracers
Microplastics	All assumed as the <0.0781-5 mm bin
Macroplastics	Equally distributed between 5-50 mm and > 50 mm bins

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216 **Supplementary Table 2.** Fraction of emissions from different continents

	Lebreton	Mai	Weiss
Asia	86.00%	69.00%	45.34%
Africa	7.80%	1.55%	11.31%
North America	0.95%	6.23%	14.78%
South America	4.80%	21.39%	17.31%
Europe	0.28%	1.71%	10.61%
Oceania	0.02%	0.16%	0.65%

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219 **Supplementary Table 3.** Consumption of different plastic types around the world in 2013, in the
220 unit of 10 thousand metric tons¹⁶.

Type	Global	Asia	North America	Western Europe	Middle East
PE	8157.8	3648.1	1557.9	1101.2	534.5
PP	5606.8	3070.9	720.1	737.4	375.2
PVC	3854.9	2192.4	514.4	402	215.9
Others	2387.3	1345.9	323.8	326.1	126

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Supplementary Table 4. Model parameterization of plastic particle settling.

Parameter	Unit	Description	Value or formula
F_D	kg m s^{-2}	Dragging force of seawater (vertical)	$F_D = -\frac{1}{2} C_D(\text{Re}_s) A_p \rho_s \frac{(\mathbf{w} - \mathbf{w}_s)}{ \mathbf{w} - \mathbf{w}_s }$
F_g	kg m s^{-2}	Gravity	$F_g = V_p \rho_p \mathbf{g}$
F_b	kg m s^{-2}	Buoyancy	$F_b = -V_s \rho_s \mathbf{g}$
C_D	unitless	Coefficient of dragging (function of Re)	$C_D = C_D(\text{Re})$
Re_s	unitless	Reynolds number of seawater	$\text{Re}_s = \frac{d \rho_s \mathbf{w} - \mathbf{w}_s }{\mu_s}$
A_p	m^2	Sectional area	$A_p = \frac{1}{4} \pi d^2$
d	m	Stokes diameter (For strict sphere particle, stokes diameter is normal diameter. For other shapes of particles, stokes diameter is the diameter of the sphere particle which has the same sinking speed.)	Model input
V_p	m^3	Volume of microplastics particle	$V_p = \frac{1}{6} \pi d^3$
V_s	m^3	Volume of microplastics particle submerged in seawater (when sinking or rising)	$V_s = V_p$
ρ_p	kg m^{-3}	Mean density of particle	Model input
ρ_s	kg m^{-3}	Density of sea water	Model input
\mathbf{g}	m s^{-2}	Gravitational acceleration	9.8
μ_s	$\text{kg m}^{-1} \text{s}^{-1}$	Dynamic-viscosity coefficient of seawater	Model input
\mathbf{w}	m s^{-1}	Sinking or rising speed (Need also a technique to eliminate Re. Flux of particle and settling of particle also have parameterization)	$(\mathbf{w} - \mathbf{w}_s)^2 = \frac{4 \mathbf{g} d(\rho_p - \rho_s)}{3C_D(\text{Re}_s)\rho_s}$
\mathbf{w}_s	m s^{-1}	Velocity of seawater	Model input

Supplementary Table 5. Model parameterization of plastic particle drifting.

Parameter	Unit	Description	Value or formula
\mathbf{F}_s	kg m s^{-2}	Dragging force by sea water (horizontal)	$\mathbf{F}_s = -\frac{1}{2} C_D (\text{Re}_s) A_s \rho_s \frac{(\mathbf{u} - \mathbf{u}_s)^3}{ \mathbf{u} - \mathbf{u}_s }$
\mathbf{F}_a	kg m s^{-2}	Dragging force by air (horizontal)	$\mathbf{F}_a = -\frac{1}{2} C_D (\text{Re}_a) A_a \rho_a \frac{(\mathbf{u} - \mathbf{u}_a)^3}{ \mathbf{u} - \mathbf{u}_a }$
\mathbf{F}_c	kg m s^{-2}	Coriolis force	$\mathbf{F}_c = V_p \rho_p f_C \mathbf{u}$
Re_a	unitless	Reynolds number of seawater	$\text{Re}_a = \frac{d \rho_a \mathbf{u} - \mathbf{u}_a }{\mu_a}$
V_s	m^3	Volume of microplastics particle submerged in sweater	$V_s = \frac{1}{6} \pi d^3 - \pi h^2 \left(\frac{d}{2} - \frac{h_a}{3} \right)$
h_a	m	height of the upper part (exposed to air)	By solving $\mathbf{F}_g + \mathbf{F}_b = 0$
A_a	m^2	Sectional area of particle exposed to air	$A_a = \frac{1}{4} r^2 (\alpha - \sin \alpha)$ $\alpha = 2 \arccos \left(1 - \frac{2h_a}{d} \right)$
A_s	m^2	Sectional area of particle exposed to seawater	$A_s = \frac{1}{4} \pi d^2 - A_a$
ρ_a	kg m^{-3}	Density of air	Model input
f_C	rad s^{-1}	Coriolis parameter	$f_C = 2\Omega \sin \varphi$
Ω	rad s^{-1}	Angular speed of the earth	7.3×10^{-5}
φ	degree	Latitude	Model grid
\mathbf{u}	m s^{-1}	Drifting speed (using gradient descent and fourth-order Adams method to calculate)	$m \frac{d\mathbf{u}}{dt} = \mathbf{F}_s + \mathbf{F}_a + \mathbf{F}_c$

Supplementary Table 6. Model parameterization of plastic particle biofouling and defouling¹⁷.

Parameter	Unit	Description	Value or formula
V_{bf}	m^3	Volume of biofilm	$\frac{dV_{bf}}{dt} = V_a \theta_p \frac{dA}{dt} + V_a A \frac{d\theta_p}{dt}$
V_a	m^3	Individual algae volume	2.0×10^{-16}
A	$\# m^{-2}$	the biomass of attached algae	$\frac{dA}{dt} = \frac{\beta_a A_a}{\theta_p} - m_a A$
θ_p	m^2	surface area of plastic particle	Model input
β_a	$m^3 s^{-1}$	Encounter kernel rate	$\beta_a = \beta_{brownian} + \beta_{shear}$
A_a	$\# m^{-3}$	Ambient algae concentration	Model input
m_a	s^{-1}	Mortality rate	4.5×10^{-6}
$\beta_{brownian}$	$m^3 s^{-1}$	Brownian motion frequencies	$\beta_{brownian} = 4\pi(D_p + D_a)(r_p + r_a)$
β_{shear}	$m^3 s^{-1}$	Advective shear collision frequencies	$\beta_{shear} = 1.3\gamma(r_p + r_a)^3$
D_p	$m^2 s^{-1}$	Diffusivity of plastics	$D_p = \frac{k(T + 273.16)}{6\pi\mu_{sw}r_p}$
D_a	$m^2 s^{-1}$	Diffusivity of individual algae cells	$D_a = \frac{k(T + 273.16)}{6\pi\mu_{sw}r_a}$
r_p	m	radius of plastics	Model input
r_a	m	radius of algae cells	Model input
k	$kg m^{-1} s^{-1}$	Boltzmann constant	1.3806×10^{-23}
T	$^{\circ}C$	Seawater temperature	Model input
ρ_{bf}	$kg m^{-3}$	Algae density	1388
γ	s^{-1}	Shear rate	1.9676
μ_{sw}	$kg m^{-1} s^{-1}$	Dynamic water viscosity	1.174×10^{-3}
τ_{trans}	s^{-1}	Fraction of transformation between biofouled and unbiofouled plastics	$\tau_{trans} = \delta \frac{\frac{dV_{bf}}{dt}}{\Delta V}$
ΔV	m^3	Deviation of volume between the two plastics	Calculate in the model
$V_{PE_{neutral}}$	m^3	Volume of a neutral PE particle	$\frac{4}{3}\pi r_{PE_{neutral}}^3$
$V_{PE_{floating}}$	m^3	Volume of a floating PE particle	$\frac{4}{3}\pi r_{PE_{floating}}^3$

231 **Supplementary Table 7.** Parameters of ensemble model members used in this study (ratios to
 232 those of the test scenario).

No.	focean^a	fbeach^b	fsediment^c	fbiofoul^d	ffrag^e
1	1.65	2.06	0.15	9.37	0.29
2	1.11	1.82	1.18	14.06	23.78
3	1.07	0.73	0.38	0.41	0.27
4	1.04	2.58	0.44	0.72	3.83
5	1.61	1.36	3.26	2.72	0.64
6	1.21	0.78	0.35	2.08	1.08
7	0.91	1.22	3.12	1.57	1.25
8	1.14	1.04	0.41	2.47	5.06
9	0.73	2.45	0.82	0.76	0.36
10	0.60	0.29	1.50	6.29	1.84
11	1.43	2.01	0.06	0.82	1.50
12	1.36	0.02	0.31	2.49	0.87
13	1.28	0.28	0.15	2.40	3.95
14	1.82	0.97	0.49	4.54	0.19
15	0.13	1.15	3.95	0.40	0.23
16	0.93	1.01	2.60	1.28	0.11
17	0.73	0.77	8.07	2.87	0.94
18	1.65	0.22	0.67	5.08	5.64
19	1.37	1.37	0.51	2.36	0.39
20	1.29	1.21	3.71	0.61	2.08
21	1.40	0.33	1.20	6.29	1.14
22	0.85	1.34	0.73	1.67	0.86
23	0.99	1.35	4.80	1.68	6.67
24	0.78	1.18	0.38	0.23	2.03
25	1.31	1.22	1.58	0.37	0.56
26	0.95	0.48	1.47	15.23	0.57
27	1.32	0.22	4.67	0.33	1.27
28	0.69	1.38	1.01	0.95	29.82
29	0.68	0.96	21.95	0.27	1.89
30	0.46	1.77	1.46	2.12	0.73
31	1.12	2.10	0.07	0.15	1.61
32	0.67	0.78	0.18	0.35	0.63
33	0.64	0.35	0.62	0.34	4.69
34	0.51	2.36	0.65	0.19	0.49
35	1.47	1.79	1.20	1.39	2.07
36	0.27	0.56	0.12	0.60	2.98
37	1.36	2.72	1.21	0.08	6.99
38	1.64	0.56	1.29	2.45	1.56
39	1.35	0.92	0.96	1.11	0.40
40	1.71	1.00	2.20	0.37	0.29
41	0.95	0.81	3.96	2.01	1.86
42	0.28	0.27	1.26	0.67	4.42
43	1.67	0.56	2.74	4.99	1.45

44	1.81	1.80	1.28	2.74	1.25
45	0.79	1.27	1.04	0.66	7.68
46	1.11	3.05	0.71	1.91	6.18
47	2.36	1.23	0.40	2.52	0.22
48	0.86	1.20	5.56	5.23	0.97
49	1.46	0.76	2.14	9.07	1.20
50	0.85	0.62	2.28	4.66	11.56
51	0.13	3.05	21.95	15.23	29.82
52	2.36	0.02	0.06	0.08	0.11
mean^f	1.11	1.18	2.37	2.87	3.62
stdev^g	0.50	0.77	4.28	3.70	6.53

233 ^afractions of the ocean emission to the total discharge. ^bbeaching rate. ^csedimentation rate.
234 ^dbiofouling rate. ^efragmentation rate. ^fthe mean of all the members. ^gthe standard deviation of the
235 members.
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238

239 **Supplementary Table 8.** summarizes the data sources and measurement procedures.

Area	Sampling method	Mesh size [mm]	Number of data	Without fiber (%)	Flowmeter	Identification method	Unit	Reference
Eastern N. Pacific	N ^a	0.335	2529	NR ^b	W/O ^c	V ^e	pieces/km ²	Law et al. 2014 ¹⁸
World's ocean	N	0.2	1943	100 ^f	W ^d	V	pieces/km ²	Cozar et al. 2014 ⁶
World's ocean	N	0.33	679	100 ^g	W/O	V	pieces/km ²	Eriksen et al. 2014 ¹⁹
Western N. Atlantic & Caribbean Sea ^h	N	0.335	2280	NR	W/O	V	pieces/km ²	Law et al. 2010 ²⁰

240 ^aNeuston net, ^bNot recorded, ^{c,d}Without or with a flowmeter, ^eVisual identification, ^fFibrous
 241 microplastics were discarded by this project, ^gThe “vast majority” of collected microplastics
 242 were fragments, ^hAlso includes macroplastics.

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