#### **Supporting information for**

# **Ag-Thiolate Interactions to Enable an Ultrasensitive and Stretchable MXene Strain Sensor with High Temporospatial Resolution**

Yang Liu<sup>#,\*1</sup>, Zijun Xu<sup>#,1</sup>, Xinyi Ji<sup>#,2</sup>, Xin Xu<sup>1</sup>, Fei Chen<sup>1</sup>, Xiaosen Pan<sup>1</sup>, Zhiqiang Fu<sup>1</sup>, Yunzhi Chen<sup>1</sup>, Zhengjian Zhang<sup>1</sup>, Hongbin Liu<sup>1</sup>, Bowen Cheng\*,<sup>1</sup>, Jiajie Liang\*<sup>2,3,4</sup>

<sup>1</sup> State Key Laboratory of Biobased Fiber Manufacturing Technology, Tianjin Key Laboratory of Pulp and Paper, Tianjin University of Science and Technology, Tianjin 300457, China

<sup>2</sup> School of Materials Science and Engineering, National Institute for Advanced Materials, Nankai University, Tianjin 300350, China.

<sup>3</sup> Key Laboratory of Functional Polymer Materials of Ministry of Education, College of Chemistry, Nankai University, Tianjin 300350, China.

<sup>4</sup> School of Materials Science and Engineering & Smart Sensing Interdisciplinary Science Center, Nankai University, Tianjin 300350, China.

Address correspondence to:  $\text{liuyangtust}(\text{a})\text{tust.edu}$ .cn (Y. Liu), bowen15@tiangong.edu.cn (B. Cheng), liang0909@nankai.edu.cn (J. Liang) # These authors contributed equally to this work.

### **This PDF file includes:**

Supplementary Note 1 and 2 Supplementary Fig. 1 to 25 Supplementary Table 1 Supplementary Movie 1 Supplementary References

## **Supplementary Note 1:**

Figure S5 plots the relative change in resistance of the S-M/A1 strain sensor with various thicknesses (T) of 2.4, 1.4, and 0.7 µm as a function of applied strain. Obviously, the stretchability of the S-M/A1 strain sensor increases with the device thickness decreases from thickness of 2.4 to 1.4 µm. The highest GF for the rigid S-M/A1 strain sensor with device thickness of 2.4 μm was calculated to be 445000 in working strain range of 9-11%. Although the maximum GF drops to 71400 as the device thickness declines to 1.4 from 2.4 μm, the working strain range shows a significant increase from 11% to 45%. This stretchability increase can be attributed to the fact that reducing thickness in the film can render the brittle thin film flexible<sup>1</sup>. With the thickness further decreased to 0.7  $\mu$ m from 1.4  $\mu$ m, the stretchability of the S-M/A<sub>1</sub> strain sensor decreased and the GF values increased. This phenomenon was mainly attributed to easier destruction of electrical junctions between adjacent sensing islands under stretching when the sensing film had a very small thickness<sup>2</sup>.

#### **Supplementary Note 2:**

We conducted tensile and crack distribution analysis on the model using a standard module of ABAQUS software. The simulation process included the following four steps: (1) Material definition. We utilized the Johnson-Cook damage model and referenced stress-strain curves from previous reports for MXene<sup>3</sup> and AgNW<sup>4</sup>. The fracture condition was set based on the tensile properties of MXene and AgNW. The density, elastic modulus, and tensile strength used in the simulation process for MXene (and S-MXene) was 4.4 g/cm<sup>3</sup>, 80 GPa, and 0.67 GPa<sup>3,5</sup>, and 10.5 g/cm<sup>3</sup>, 86 GPa, and  $2 \text{ GPa}^{4,6}$ , respectively. (2) Contact settings. We then specified frictionless and adhesive contact between AgNW and MXene (or S-MXene). The calculation of Ag-S bonding points was based on the MPTES molecule weight and S-MXene mass, with the adhesion strength defined as  $17.74$  kcal·mol<sup>-1</sup>. (3) Mesh partitioning. Tetrahedral free mesh partitioning with C3D10 elements for MXene (or S-MXene) and AgNW models was employed. (4) Boundary conditions. We fixed the constraints at one end and the load tensile strain of 10% at the other end.

## **Supplementary figures and tables**



**Supplementary Fig. 1.** S-M/A<sub>1</sub> sensor array in the unstretched state and under 60% strain.



**Supplementary Fig. 2.** XPS spectra of a, b) S-MXene and c) MXene films in the O 1*s* and Si 2*p* region.



**Supplementary Fig. 3.** Relative resistance changes of MXene and S-MXene after storage in the aging chamber with a temperature of 80 °C and relative humidity (RH) of 85% for 30 days. Compared with the MXene film, the S-MXene film exhibited much improved oxidation resistance.



**Supplementary Fig. 4.** S-M/A sensing films with different thicknesses (T).



**Supplementary Fig. 5.** (a) Relative resistance variation as a function of large strain and its details for S-M/A1 sensors with different thickness. (b) The calculated GF for the S-M/A1 sensors with different thickness.



**Supplementary Fig. 6.** TEM images and corresponding EDS element maps of (a) and (b) AgNW and (c)-(h) S-MXene.



**Supplementary Fig. 7.** SEM images of original S-M/A film under 0% strain and corresponding elemental distribution.



**Supplementary Fig. 8.** Calculation of the bending strain when bending the device to different strains,  $\varepsilon = T/2R$ , where *T* is the combined thickness of the sensing film and substrate, and *R* is the bending radius.



**Supplementary Fig. 9.** Relative resistance variation as a function of tiny strain (0– 0.05%) for (a)  $S-M/A_1$ , (b)  $S-M/A_2$ , and (c)  $S-M/A_5$  sensors.



**Supplementary Fig. 10.** The other 4 repeated results of relative resistance variation as a function of tiny strain (0–0.05%) for the S-M/ $A<sub>0.5</sub>$  sensor.



**Supplementary Fig. 11.** The other 4 repeated results of the transient sensing response and recovery time to an applied strain of 0.05% for the S-M/A0.5 sensor.



**Supplementary Fig. 12.** Relative resistance variation as a function of large strain for (a)  $S-M/A<sub>1</sub>$ , (b)  $S-M/A<sub>2</sub>$ , and (c)  $S-M/A<sub>5</sub>$  sensors.



**Supplementary Fig. 13.** Relative resistance variation as a function of large strain for (a)  $M/A_2$  and (b)  $M/A_5$  sensors.



**Supplementary Fig. 14.** (a) Relative resistance variation as a function of large strain for S-M/A<sub>0.5</sub>, S-M/A<sub>1</sub>, S-M/A<sub>2</sub>, and S-M/A<sub>5</sub> sensors under one stretch-release cycle. Detailed relative resistance changes versus strain curves at 1st, 10th, and 100th stretchrelease cycle for (b)  $S-M/A_{0.5}$ , (c)  $S-M/A_1$ , (d)  $S-M/A_2$ , and (e)  $S-M/A_5$  sensors.



**Supplementary Fig. 15.** (a) Relative resistance changes of the S-M/A<sub>0.5</sub> sensor over 4000 stretch-release cycles in the strain range of 0–0.05%. (b) Detailed resistance changes recorded between 3900 and 3910 stretch-release cycles.



**Supplementary Fig. 16.** Relative resistance changes of S-M/A5 sensor (a) over 8000 stretch-release cycles in the strain range of 0–70% under RH of 50% and (b) over 7000 stretch-release cycles in the strain range of 0–70% under RH of 85%.



**Supplementary Fig. 17.** (a) and (b) Magnifed SEM images of S-M/A film under 60% strain. EDS element maps of (c) S and (d) Ti from (a). Uniform distribution of AgNWs can be clearly seen in the S-M/A film.



**Supplementary Fig. 18.** (a) and (b) SEM images of M/A film under 60% strain. EDS element maps of (c) O and (d) Ti from (b). Uniform distribution of AgNWs can be clearly seen in the M/A film.



**Supplementary Fig. 19.** Schematic diagram of the proposed working principle of the tunneling effect for the crack-based S-M/A strain sensor.



**Supplementary Fig. 20.** SEM images of S-M/A sensing film (a) under 100% strain and (b) after 5000 stretch-release cycles at 60% strain.



**Supplementary Fig. 21.** Photograph of a 100-channel S-M/A0.5 strain sensor array with a device density of 100 sensors per square centimeter.



**Supplementary Fig. 22.** Photograph showing the monitoring of an artery pulse waveform of a volunteer using our multichannel pulse sensing system.



**Supplementary Fig. 23.** (a) Photograph of a 36-channel S-M/A<sub>1</sub> strain sensor array detecting a small object with complex shape, and (b) and (c) the corresponding intensity distribution of the normalized resistance change on the sensing array. (d) Photograph of a pipette tip poking on a 36-channel S-M/A1 strain sensor array, and (e) and (f) the corresponding intensity distribution of the normalized resistance change on the sensing array.

**Hydrolysis reaction:**

$$
\begin{array}{ccc}\n & \mathsf{OCH}_3 \\
\mathsf{R} - \mathsf{S}i - \mathsf{OCH}_3 + 3\mathsf{H}_2\mathsf{O} & \longrightarrow & 3\mathsf{n} & \mathsf{R} - \mathsf{S}i - \mathsf{OH} + 3\mathsf{CH}_3\mathsf{OH} \\
 & \mathsf{OCH}_3 & & \mathsf{OH} \\
\end{array}
$$

**Self-polymerization reaction:**



**Surface modification reaction:**



**Supplementary Fig. S24.** The hydrolysis, self-polymerization, surface modification reaction mechanism of MPTES.



**Supplementary Fig. S25.** TGA and DTG results for S-MXene and MXene. The content of MPTES grafted onto the S-MXene was about 3.6 wt%.



**Supplementary Table 1.**



**Supplementary Movie 1:** Real-time and dynamic display of the 3D pulse strength distribution measured by the 36-channel S-M/A1 strain sensor array.

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