

**GLOBAL ROBUST  $H_\infty$  CONTROL FOR  
NON-MINIMUM-PHASE UNCERTAIN  
NONLINEAR SYSTEMS WITHOUT STRICT  
TRIANGULAR STRUCTURE<sup>1</sup>**

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Abstract: This paper deals with the robust  $H_\infty$  control problem for a class of multi-input non-minimum-phase nonlinear systems with parameter uncertainty. A system of this class is assumed to be in a special interlaced form, which includes a strict triangular form as a special case. By using an extension of backstepping, nonlinear static-state feedback controllers are designed such that the closed-loop system is input-to-state stable with respect to the disturbance input and has the prescribed  $L_2$ -gain from the disturbance input to the controlled output for all admissible parameter uncertainties. *Copyright©2005 IFAC*

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## 1. INTRODUCTION

$H_\infty$  control has become a powerful tool to solve the robust stabilization and disturbance attenuation problem and has been investigated heavily. There are some approaches which have been used to provide solutions to nonlinear  $H_\infty$  control problem. One is based on the dissipativity theory and differential games theory in (Basar and Bernhard, 1991; Ball and Helton, 1989). The other is based on the nonlinear version of classical bounded real lemma in (Isidori and Astolfi, 1992; Isidori, 1991; Van der Schaft, 2000). These results involve solving Hamilton-Jacobi-Isacs equations (HJIEs), whose nice feature is that they are par-

allel to the results of linear  $H_\infty$  control. However, for the aforementioned results, the lack of efficient numerical procedures for solving the HJIEs is a formidable difficulty. This motivates some attempts to look for methods which solve reduced-order HJIEs or need not to solve any HJIEs. By using "normal form" and backstepping technique, the  $H_\infty$  control problem has been investigated extensively. Results in (Isidori, 1996a; Marino, et al., 1994; Guo, et al., 2000) deal with minimum-phase systems and (Isidori, 1996b; Su, et al., 1999; Lin, et al., 1999) provide results for non-minimum-phase systems whose zero dynamics are divided into stable parts and unstable but stabilizable parts. Backstepping method has been extended to investigate the  $H_\infty$  control problem for systems with block-strict-triangular form (Xie and Su, 1997), subject to parameter uncertainty (Xie

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and Su, 1997; Su, et al., 1999) and with time-delay (Guo, et al., 2000).

Though backstepping play an important role in nonlinear  $H_\infty$  control problem, a significant restriction of the method is that it is only suitable to the systems with inherent strict triangular form.

In this paper, we will extend the backstepping technique to multi-input non-minimum-phase systems which are non-strict triangular form. Such a system, which includes the strict triangular form as a special case, consists of one autonomous subsystem (we call it zero dynamics of the system) and two single-input subsystems with special interconnections. We allow the existence of not only feedback but also feedforward interconnections among the subsystems. Also, our zero dynamics equation is allowed to contain the states of all subsystems, which is obviously much more general than those in papers mentioned above, where zero dynamics equation can only contain the states of the first subsystem. Such special interconnections in this paper make it possible to construct the robust  $H_\infty$  controllers using an extension of backstepping. The main design procedure is as follows. First, using backstepping technique, we design the robust  $H_\infty$  controller for the first subsystem. Then, by analyzing the resulting closed-loop subsystem through the interconnection to the next subsystem, another augmented subsystem is obtained, which is also in a strict triangular form. Finally, the second robust  $H_\infty$  controller can be designed by backstepping. The results of this paper can also be viewed as a generalization of the robust stabilization result in (Liu, et al., 1999), where no  $H_\infty$  control is considered.

## 2. PRELIMINARIES

This paper considers a nonlinear uncertain system with two inputs, which is described by

$$\begin{aligned} \dot{\eta} &= f_1(\eta, \xi_1, \theta) + p_0(\eta, \xi_1, \theta)w + f_2(\eta, \xi, u, \zeta_1, \theta)\zeta_1, \\ \dot{\xi}_1 &= \xi_2 + \mu_1(\eta, \xi_1, \theta) + p_1(\eta, \xi_1, \theta)w \\ &\quad + \varphi_1(\eta, \xi, u, \zeta_1, \theta)\zeta_1, \\ &\dots \\ \dot{\xi}_{m-1} &= \xi_m + \mu_{m-1}(\eta, \xi_1, \dots, \xi_{m-1}, \theta) \\ &\quad + p_{m-1}(\eta, \xi_1, \dots, \xi_{m-1}, \theta)w \\ &\quad + \varphi_{m-1}(\eta, \xi, u, \zeta_1, \theta)\zeta_1, \\ \dot{\xi}_m &= u + \mu_m(\eta, \xi_1, \dots, \xi_m, \theta) \\ &\quad + p_m(\eta, \xi_1, \dots, \xi_m, \theta)w \\ &\quad + \varphi_m(\eta, \xi, u, \zeta_1, \theta)\zeta_1, \\ \dot{\zeta}_1 &= \zeta_2 + \phi_1(\eta, \xi, u, \zeta_1, \theta) + q_1(\eta, \xi, u, \zeta_1, \theta)w, \\ &\dots \\ \dot{\zeta}_{n-1} &= \zeta_n + \phi_{n-1}(\eta, \xi, u, \zeta_1, \dots, \zeta_{n-1}, \theta) \\ &\quad + q_{n-1}(\eta, \xi, u, \zeta_1, \dots, \zeta_{n-1}, \theta)w, \\ \dot{\zeta}_n &= v + \phi_n(\eta, \xi, u, \zeta_1, \dots, \zeta_n, \theta) \\ &\quad + q_n(\eta, \xi, u, \zeta_1, \dots, \zeta_n, \theta)w, \\ y &= h(\eta, \xi_1, \theta) + d(\eta, \xi_1, \theta)w, \end{aligned}$$

where  $\eta \in R^l$ ,  $\xi = [\xi_1, \dots, \xi_m]^T \in R^m$ ,  $\zeta = [\zeta_1, \dots, \zeta_n]^T \in R^n$ ,  $u, v \in R$  are the control inputs,  $\theta$  is a uncertain parameter vector belonging to a known compact set  $\Omega$ ,  $w \in R^r$  is the disturbance input,  $y \in R^k$  is the controlled output. All vector fields are assumed to be smooth. We also assume  $f_1(0, 0, \theta) = 0$ ,  $\mu_i(0, \dots, 0, \theta) = 0$ ,  $\phi_i(0, \dots, 0, \theta) = 0$ ,  $i = 1, \dots, n$ , and  $h(0, 0, \theta) = 0$  for any  $\theta \in \Omega$ .

**Remark 1.** In single-input case, system (1) with  $\zeta_1 \equiv 0$  reduces to a strict triangular form, which has been studied extensively (see, for example, Isidori, 1996a; Isidori, 1996b; Su, et al., 1999). Obviously, system (1) is not in a strict feedback form and its zero dynamics ( $\eta$ -subsystem) contains not only the state of the first subsystem  $\xi$  but also the state of the second subsystem  $\zeta$ . Therefore, system (1) covers much broader class of nonlinear systems. At the same time, the results aforementioned are no longer suitable for system (1).

**Remark 2.** Here we study two inputs case only for the sake of simplicity. All results can be extended to multi-input case without any difficulty.

The following assumptions will be needed in the sequel.

**Assumption 1.** The  $\eta$ -subsystem of (1) with  $\zeta_1 \equiv 0$  can be decomposed into the following two cascade-connected subsystems:

$$\begin{aligned} \dot{\eta}_1 &= f_{01}(\eta_1, \eta_2, \xi_1, \theta) + p_{01}(\eta_1, \eta_2, \xi_1, \theta)w, \\ \dot{\eta}_2 &= f_{02}(\eta_2, \xi_1, \theta), \end{aligned} \quad (2)$$

where  $\eta_1 \in R^{m_1}$ ,  $\eta_2 \in R^{m_2}$ ,  $m_1 + m_2 = l$ ,  $\eta = [\eta_1^T, \eta_2^T]^T$ , and with  $f_{01}(0, 0, 0, \theta) = 0$  and  $f_{02}(0, 0, \theta) = 0$  for any  $\theta \in \Omega$ .

**Assumption 2.**

(a) For the  $\eta_1$ -subsystem, there exists a real-valued function  $W_1(\eta_1, \theta)$ , which is smooth in  $\eta_1$ , and positive definite and proper for any  $\theta \in \Omega$ , such that

$$\begin{aligned} \frac{\partial W_1}{\partial \eta_1} [f_{01}(\eta_1, \eta_2, \xi_1, \theta) + p_{01}(\eta_1, \eta_2, \xi_1, \theta)w] \\ \leq -\alpha_1 \|\eta_1\|^2 + \gamma_0^2 \|w\|^2 + k_1(\eta_2, \xi_1) \end{aligned} \quad (3)$$

for any  $\theta \in \Omega$ , some positive-definite function  $k_1(\eta_2, \xi_1)$  and some positive constants  $\alpha_1$  and  $\gamma_0$ .

(1) (b) For the  $\eta_2$ -subsystem, there exists a real-valued function  $\mu(\eta_2)$  with  $\mu(0) = 0$  and a real-valued function  $W_2(\eta_2, \theta)$ , which is smooth and positive definite in  $\eta_2$  for any  $\theta \in \Omega$ , such that

$$\frac{\partial W_2}{\partial \eta_2} f_{02}(\eta_2, \mu(\eta_2), \theta) \leq -\alpha_2 W_2(\eta_2, \theta), \quad (4)$$

$$\alpha_3 \|\eta_2\|^2 \leq W_2(\eta_2, \theta)$$

for any  $\theta \in \Omega$  and some positive constants  $\alpha_2$  and  $\alpha_3$ .

**Remark 3.** Here we adopt the standard conditions similar to that in (Su, et al., 1999; Isidori, 1996b). Assumption 1 and Assumption 2 mean that when  $\zeta \equiv 0$  the zero dynamics of (1) take two cascade-connected parts, one part is input-to-state stable, the other part may be unstable but stabilizable.

The following condition is crucial to the construction of a storage function of the system even in single-input strict triangular form, and is commonly applied in the literature (see, for example, Xie and Su, 1997; Su, et al. 1999).

**Assumption 3.**  $d(\eta, \xi_1, \theta)$  is uniformly bounded, i.e., there exists a positive real number  $\gamma_d$  such that for any  $\theta \in \Omega$ ,

$$\|d(\eta, \xi_1, \theta)\| \leq \gamma_d, \forall [\eta^T, \xi_1^T] \in R^{l+1}.$$

This paper deals with the following robust  $H_\infty$  control problem for system (1):

Given any scalar  $\gamma > \gamma_d$ , design feedback control laws  $u = u(\eta, \xi)$  with  $u(0, 0) = 0$  and  $v = v(\eta, \xi, \zeta)$  with  $v(0, 0, 0) = 0$  such that for any  $\theta \in \Omega$ :

(a) the resulting closed-loop system is input-to-state stable with respect to the disturbance input  $w$ .

(b) the  $L_2$ -gain from disturbance input  $w$  to controlled output  $y$  of the closed-loop is not larger than  $\gamma$  for any  $\theta \in \Omega$ , i.e., there exists a function  $\beta : R^l \times R^m \times R^n \times \Omega \rightarrow R$  with  $\beta(0, 0, 0, \theta) = 0$ ,  $\forall \theta \in \Omega$ , such that for any initial condition  $(\eta^0, \xi^0, \zeta^0)$  and all  $w \in L_2[0, \infty)$ , it holds that

$$\int_0^\infty y^T(\tau)y(\tau)d\tau \leq \gamma^2 \int_0^\infty w^T(\tau)w(\tau)d\tau + \beta(\eta^0, \xi^0, \zeta^0, \theta), \quad (5)$$

$\forall \theta \in \Omega.$

**Remark 4.** Since global asymptotic stability with zero input does not imply stability when they are subjected to some non-zero inputs, and the notion input-to-state stability (ISS) in (Sontag and Wang, 1995) describes stronger and desirable stability property of systems with bounded inputs. Here, the internal stability with zero initial value adopted in general  $H_\infty$  control problem (Isidori, 1996a; Isidori, 1996b; Guo, et al. 2000; Lin, et al. 1999) is replaced by ISS.

Before developing the main results, we review some results about robust  $H_\infty$  control for single-input strict triangular systems described as

$$\begin{aligned} \dot{\eta} &= f_1(\eta, \xi_1, \theta) + p_0(\eta, \xi_1, \theta)w, \\ \dot{\xi}_1 &= \xi_2 + \mu_1(\eta, \xi_1, \theta) + p_1(\eta, \xi_1, \theta)w, \\ &\vdots \\ \dot{\xi}_{m-1} &= \xi_m + \mu_{m-1}(\eta, \xi_1, \dots, \xi_{m-1}, \theta) \\ &\quad + p_{m-1}(\eta, \xi_1, \dots, \xi_{m-1}, \theta)w, \\ \dot{\xi}_m &= u + \mu_m(\eta, \xi_1, \dots, \xi_m, \theta) \\ &\quad + p_m(\eta, \xi_1, \dots, \xi_m, \theta)w, \\ y &= h(\eta, \xi_1, \theta) + d(\eta, \xi_1, \theta)w. \end{aligned} \quad (6)$$

**Lemma 1** (Su, 1999). The global robust  $H_\infty$  control problem for the uncertain nonlinear system (6) is solvable if Assumptions 1~3 are satisfied.

According to (Su, 1999), we can easily have the following fact.

**Proposition 1.** If the uncertain nonlinear system (6) satisfies Assumptions 1~3, then there exist functions  $\sigma_1(\eta, \xi_1), \dots, \sigma_m(\eta, \xi_1, \dots, \xi_m)$  with  $\sigma_j(0, \dots, 0) = 0, j = 1, \dots, m$ , and storage function  $S_m(\eta, \xi_1, \dots, \xi_m, \theta)$ , which is a positive definite Class  $K_\infty$  function, such that along the trajectory of (6) with  $u = \sigma_m(\eta, \xi_1, \dots, \xi_m)$ , we have

$$\begin{aligned} \dot{S}_m + \|y\|^2 - \varepsilon_m^2 \|w\|^2 \\ \leq -l_m(\|\eta\|^2 + (\xi_1 - \sigma_0)^2 + (\xi_2 - \sigma_1)^2 \\ + \dots + (\xi_m - \sigma_{m-1})^2) \end{aligned} \quad (7)$$

for some constants  $\varepsilon_m$  satisfying  $\gamma > \varepsilon_m > \gamma_d$  and  $l_m > 0$ , where  $\sigma_0(\eta) = \mu(\eta_2)$ .

We recall the following result when (6) becomes the form

$$\begin{aligned} \dot{x}_1 &= f_1(x_1, \theta) + q(x_1, x_2, \theta)x_2 + p_1(x_1, \theta)w, \\ \dot{x}_2 &= u + f_2(x_1, x_2, \theta) + p_2(x_1, x_2, \theta)w, \\ y &= h_0(x_1, \theta) + d_0(x_1, \theta)w. \end{aligned} \quad (8)$$

**Lemma 2** (Su, 1999). Suppose that for a given scalar  $\tau_1 > 0$ , there exists a storage function  $V_1(x_1, \theta)$  for system (8) with  $x_2 \equiv 0$  satisfying

$$\dot{V}_1(x_1, \theta) + \|y\|^2 - \tau_1^2 \|w\|^2 \leq -c_1 \|x_1\|^2, \quad (9)$$

$\forall \theta \in \Omega$

for some positive real number  $c_1$ . Then for any scalar  $\tau_2 > \tau_1$ , there exists a control law  $u = u(x_1, x_2)$ , such that storage function

$$V_2(x_1, x_2, \theta) = V_1(x_1, \theta) + \frac{1}{2}x_2^T x_2$$

for system (8) satisfies

$$\begin{aligned} \dot{V}_2(x_1, x_2, \theta) + \|y\|^2 - \tau_2^2 \|w\|^2 \\ \leq -c_2(\|x_1\|^2 + \|x_2\|^2), \forall \theta \in \Omega \end{aligned} \quad (10)$$

for some positive real number  $c_2$ .

From (Su, 1999), we know that the control law  $u = u(x_1, x_2)$  in Lemma 2 satisfies  $u(0, 0) = 0$ .

### 3. MAIN RESULT

In this section, we extend the backstepping technique to solve the robust  $H_\infty$  control problem for system (1). The main theorem is as follows.

**Theorem 1.** Assume Assumptions 1~3 are satisfied. Then the global robust  $H_\infty$  control problem for system (1) is solvable.

**Proof.** We divide the proof into three steps.

**Step 1.** Consider the  $(\eta, \xi)$ -subsystem, i.e., system (6). Proposition 1 gives (7).

**Step 2.** Make the global change of coordinates

$$\begin{aligned} \eta &= \eta, \\ \bar{\xi}_i &= \xi_i - \sigma_{i-1}, i = 1, \dots, m, \\ \zeta_i &= \zeta_i, i = 1, \dots, n, \end{aligned} \quad (11)$$

and impose the feedback  $u = \sigma_m$ , where  $\sigma_i, i = 0, 1, \dots, m$ , are shown in Proposition 1. Then, system (1) can be expressed as

$$\begin{aligned} \dot{z} &= F_1(z, \theta) + F_2(z, \zeta_1, \theta)\zeta_1 + P(z, \theta)w, \\ \dot{\zeta}_1 &= \zeta_2 + \phi_1(\eta, \xi, \sigma_m, \zeta_1, \theta) \\ &\quad + q_1(\eta, \xi, \sigma_m, \zeta_1, \theta)w, \\ &\vdots \\ \dot{\zeta}_{n-1} &= \zeta_n + \phi_{n-1}(\eta, \xi, \sigma_m, \zeta_1, \dots, \zeta_{n-1}, \theta) \\ &\quad + q_{n-1}(\eta, \xi, \sigma_m, \zeta_1, \dots, \zeta_{n-1}, \theta)w, \\ &\vdots \\ \dot{\zeta}_n &= v + \phi_n(\eta, \xi, \sigma_m, \zeta_1, \dots, \zeta_n, \theta) \\ &\quad + q_n(\eta, \xi, \sigma_m, \zeta_1, \dots, \zeta_n, \theta)w, \end{aligned} \quad (12)$$

$$y = h(\eta, \xi_1, \theta) + d(\eta, \xi_1, \theta)w,$$

$$\text{where, } z = [\eta^T, \bar{\xi}_1, \dots, \bar{\xi}_m]^T,$$

$$F_1(z, \theta) =$$

$$\begin{pmatrix} f_1 \\ \xi_2 + \mu_1 - \frac{\partial \sigma_0}{\partial \eta} f_1 \\ \xi_3 + \mu_2 - \frac{\partial \sigma_1}{\partial \eta} f_1 - \frac{\partial \sigma_1}{\partial \xi_1} (\xi_2 + \mu_1) \\ \vdots \\ \xi_m + \mu_{m-1} - \frac{\partial \sigma_{m-2}}{\partial \eta} f_1 - \frac{\partial \sigma_{m-2}}{\partial \xi_1} (\xi_2 + \mu_1) \\ \quad - \dots - \frac{\partial \sigma_{m-2}}{\partial \xi_{m-2}} (\xi_{m-1} + \mu_{m-2}) \\ \sigma_m + \mu_m - \frac{\partial \sigma_{m-1}}{\partial \eta} f_1 - \frac{\partial \sigma_{m-1}}{\partial \xi_1} (\xi_2 + \mu_1) \\ \quad - \dots - \frac{\partial \sigma_{m-1}}{\partial \xi_{m-1}} (\xi_m + \mu_{m-1}) \end{pmatrix},$$

$$F_2(z, \zeta_1, \theta) = \begin{pmatrix} f_2 \\ \varphi_1 - \frac{\partial \sigma_0}{\partial \eta} f_2 \\ \varphi_2 - \frac{\partial \sigma_1}{\partial \eta} f_2 - \frac{\partial \sigma_1}{\partial \xi_1} \varphi_1 \\ \vdots \\ \varphi_{m-1} - \frac{\partial \sigma_{m-2}}{\partial \eta} f_2 - \frac{\partial \sigma_{m-2}}{\partial \xi_1} \varphi_1 \\ \quad - \dots - \frac{\partial \sigma_{m-2}}{\partial \xi_{m-2}} \varphi_{m-2} \\ \varphi_m - \frac{\partial \sigma_{m-1}}{\partial \eta} f_2 - \frac{\partial \sigma_{m-1}}{\partial \xi_1} \varphi_1 \\ \quad - \dots - \frac{\partial \sigma_{m-1}}{\partial \xi_{m-1}} \varphi_{m-1} \end{pmatrix},$$

$$P(z) = \begin{pmatrix} p_0 \\ p_1 - \frac{\partial \sigma_0}{\partial \eta} p_0 \\ p_2 - \frac{\partial \sigma_1}{\partial \eta} p_0 - \frac{\partial \sigma_1}{\partial \xi_1} p_1 \\ \vdots \\ p_{m-1} - \frac{\partial \sigma_{m-2}}{\partial \eta} p_0 - \frac{\partial \sigma_{m-2}}{\partial \xi_1} p_1 \\ \quad - \dots - \frac{\partial \sigma_{m-2}}{\partial \xi_{m-2}} p_{m-2} \\ p_m - \frac{\partial \sigma_{m-1}}{\partial \eta} p_0 - \frac{\partial \sigma_{m-1}}{\partial \xi_1} p_1 \\ \quad - \dots - \frac{\partial \sigma_{m-1}}{\partial \xi_{m-1}} p_{m-1} \end{pmatrix}.$$

Applying (7) to system (12) with  $\zeta_1 \equiv 0$  results in

$$\frac{\partial \bar{S}_m}{\partial z} (F_1 + Pw) + \|y\|^2 - \varepsilon_m^2 \|w\|^2 \leq -l_m \|z\|^2, \quad (13)$$

where  $\bar{S}_m(z, \theta) = S_m(\eta, \xi_1, \dots, \xi_m, \theta)$ .

**Step 3.** Since the coordinate transformation (11) is a global diffeomorphism, the robust  $H_\infty$  control problem for system (1) is solvable if the robust  $H_\infty$  control problem for system (12) is solvable. It is obvious that system (12) is in strict triangular form. Therefore, we can realize the robust  $H_\infty$  control for system (12) by a recursive application of lemma 2. To this end, let constants  $\varepsilon_{m+1}, \dots, \varepsilon_{m+n}$  satisfy  $\varepsilon_m < \varepsilon_{m+1} < \dots < \varepsilon_{m+n} = \gamma$ ,  $\beta_0(z) = 0$  and  $\zeta_{n+1} = v$  and consider the following system for  $t = 1, \dots, n$ ,  
 $\sum_t :$

$$\begin{aligned}
\dot{z} &= F_1(z, \theta) + F_2(z, \zeta_1, \theta)\zeta_1 + P(z, \theta)w, \\
\dot{\zeta}_1 &= \zeta_2 + \phi_1(\eta, \xi, \sigma_m, \zeta_1, \theta) \\
&\quad + q_1(\eta, \xi, \sigma_m, \zeta_1, \theta)w, \\
&\vdots \\
\dot{\zeta}_t &= \zeta_{t+1} + \phi_t(\eta, \xi, \sigma_m, \zeta_1, \dots, \zeta_t, \theta) \\
&\quad + q_t(\eta, \xi, \sigma_m, \zeta_1, \dots, \zeta_t, \theta)w, \\
y &= h(\eta, \xi_1, \theta) + d(\eta, \xi_1, \theta)w.
\end{aligned} \tag{14}$$

Introduce a global change of coordinates

$$\begin{aligned}
\bar{\zeta}_j &= \zeta_j - \beta_{j-1}(z, \zeta_1, \dots, \zeta_{j-1}), \\
j &= 1, \dots, t,
\end{aligned}$$

and let

$$z_{t-1} = [z^T, \bar{\zeta}_1, \dots, \bar{\zeta}_{t-1}]^T.$$

System  $\sum_t$  can be rewritten in the form of (8) with the state  $(z_{t-1}, \bar{\zeta}_t)$  and a control input  $\zeta_{t+1}$ , and (9) is satisfied. Using lemma 2, we know that there exist a control law

$$\zeta_{t+1} = \beta_t(z, \zeta_1, \dots, \zeta_t)$$

with  $\beta_t(0, 0, \dots, 0) = 0$  and a storage function

$$\begin{aligned}
S_{m+t}(z, \zeta_1, \dots, \zeta_t, \theta) \\
= S_m + \frac{1}{2}(\zeta_1 - \beta_0)^2 + \dots + \frac{1}{2}(\zeta_t - \beta_{t-1})^2,
\end{aligned}$$

such that for  $\sum_t$  it holds that

$$\begin{aligned}
\dot{S}_{m+t} + \|y\|^2 - \varepsilon_{m+t}^2 \|w\|^2 \\
\leq -l_{m+t}(\|z\|^2 + (\zeta_1 - \beta_0)^2 + \dots + (\zeta_t - \beta_{t-1})^2)
\end{aligned}$$

for some constant  $l_{m+t} > 0$ .

When  $t = n$  we have

$$\begin{aligned}
\dot{S}_{m+n} + \|y\|^2 - \gamma^2 \|w\|^2 \\
\leq -l_{m+n}(\|z\|^2 + (\zeta_1 - \beta_0)^2 \\
+ \dots + (\zeta_n - \beta_{n-1})^2),
\end{aligned} \tag{15}$$

where

$$\begin{aligned}
S_{m+n}(z, \zeta_1, \dots, \zeta_n, \theta) \\
= S_m + \frac{1}{2}(\zeta_1 - \beta_0)^2 + \dots + \frac{1}{2}(\zeta_n - \beta_{n-1})^2.
\end{aligned} \tag{16}$$

From (15), we have

$$\begin{aligned}
\dot{S}_{m+n} \leq -l_{m+n}(\|z\|^2 + (\zeta_1 - \beta_0)^2 \\
+ \dots + (\zeta_n - \beta_{n-1})^2) + \gamma^2 \|w\|^2.
\end{aligned} \tag{17}$$

From (15)~(17), it is known that  $S_{m+n}(z, \zeta_1, \dots, \zeta_n, \theta)$  is a Class  $K_\infty$  function for

$\forall \theta \in \Omega$  and system (12) is input-to-state stable with respect to the disturbance input  $w$ , and we have

$$\begin{aligned}
\int_0^\infty y^T(\tau)y(\tau)d\tau \leq \gamma^2 \int_0^\infty w^T(\tau)w(\tau)d\tau \\
+ \beta(z^0, \zeta_1^0, \dots, \zeta_n^0, \theta),
\end{aligned} \tag{18}$$

$\forall \theta \in \Omega$ ,

where

$$\beta(z^0, \zeta_1^0, \dots, \zeta_n^0, \theta) = S_{m+n}(z^0, \zeta_1^0, \dots, \zeta_n^0, \theta)$$

with initial value  $(z^0, \zeta_1^0, \dots, \zeta_n^0)$ . So the robust  $H_\infty$  control problem for system (12) is solvable. It is easily seen that the controllers

$$u = \sigma_m(\eta, \xi_1, \dots, \xi_m),$$

and

$$v = \beta_n(z, \zeta_1, \dots, \zeta_n),$$

solve the robust control problem for system (1). Thus we complete the proof of theorem 1.  $\square$

#### 4. EXAMPLE

As an illustration of the above design method, consider a simple nonlinear system of the form

$$\begin{aligned}
\dot{\eta} &= -\eta + \eta\xi^2 + \eta\zeta, \\
\dot{\xi} &= u + \xi\sin(\theta(\eta + \xi)) + 0.25w + \zeta, \\
\dot{\zeta} &= v + w, \\
y &= \eta + 0.5w,
\end{aligned} \tag{19}$$

where  $\eta, \xi, \zeta \in R$ , and the constant unknown parameter  $\theta \in [-50, 50]$ . Note that the  $\eta$ -subsystem contains not only  $\xi$  but also  $\zeta$ , and the system is not in the strict triangular structure. We will design a nonlinear state feedback controller for system (19) such that the closed-loop system is input-to-state stable and the  $L_2$ -gain from  $w$  to  $y$  is not larger than  $\sqrt{2}$ .

System (19) is in the form of Eq. (1). It just contains the  $\eta_2$ -subsystem. Thus,  $W_1 = 0$ ,  $\alpha_1 = 0$ ,  $\gamma_0 = 0$ ,  $k_1 = 0$ . Choose  $\mu(\eta_2) \equiv 0$ ,  $W_2 = 0.5\eta_2^2$ . It is easily verified that Assumptions 1~3 are satisfied and theorem 1 holds. By using the procedure adopted in theorem 1, we obtain storage function

$$S_3(\eta, \zeta, \zeta, \theta) = \eta^2 + \frac{1}{2}\xi^2 + \frac{1}{2}\zeta^2,$$

and controller

$$\begin{aligned}
u &= -2\eta^2\xi - 2\xi, \\
v &= -2\eta^2 - \xi - 2\zeta.
\end{aligned} \tag{20}$$

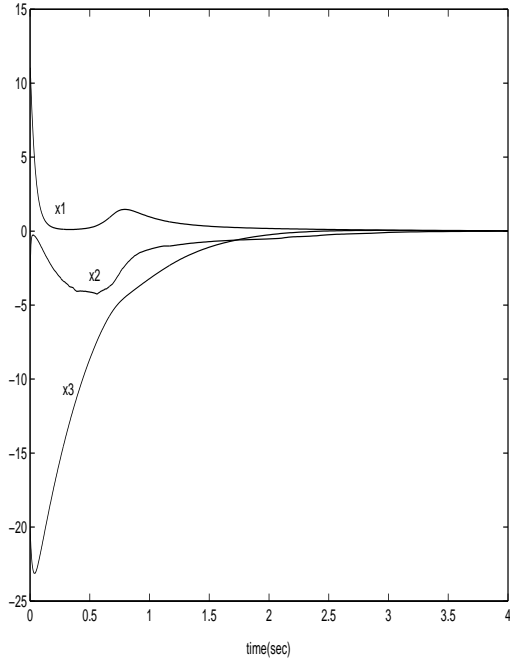


Fig. 1. state response of the resulting closed-loop system with  $w \equiv 0$  and  $\theta = 50$ ,  $\eta = x1$ ,  $\xi = x2$ ,  $\zeta = x3$ .

For the closed-loop system (19),(20), it holds that

$$\dot{S}_3 + \|y\|^2 - 2\|w\|^2 \leq -\frac{3}{4}\eta^2 - \frac{3}{4}\xi^2 - \zeta^2$$

for  $\forall \theta \in [-50, 50]$ .

Thus, controller (20) solves the robust  $H_\infty$  control problem for system (19). Fig. 1 shows the state response of the resulting closed-loop system with zero disturbance and  $\theta = 50$ .

## 5. CONCLUSIONS

We have discussed the robust  $H_\infty$  control problem for a class of multi-input non-minimum-phase nonlinear systems with parameter uncertainty. A system of this class consists of several subsystems with both special feedback and feedforward interconnections and it may not be in strict triangular form. A robust  $H_\infty$  controller, which ensures that the closed-loop system is input-to-state stable with respect to the disturbance input and has a prescribed  $L_2$ -gain for all admissible parameter uncertainties, is obtained by using an extension of backstepping.

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