Substitution Approach in Carbon Dioxide Emission Reduction Evaluation: Case Study on Geothermal Power Station Project Plan – Ďurkov (Košice Basin, Slovakia)

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Abstract—Application of substitution approach (fossil fuels heat and power production duty essential in high CO₂ emissions is replaced by low-emissions based geothermal source in the same process at the same intensity) in CO₂ emission reduction potential analysis for proposed cogeneration Ďurkov power station project is presented in the paper. Project can contribute with yearly 49 891 tCO₂ of gross (a sum of 26 811 tCO₂ from a heat and 23 080 tCO₂ from a power production) or 49 587 tCO₂ of real carbon dioxide savings. According to 40-years projected lifespan, achievable cumulative gross savings can reach 1,995 MtCO₂ or 1,99 MtCO₂ of real carbon dioxide bulk mitigated.

Index Terms—Carbon dioxide savings, Ďurkov power station project, geothermal energy, implementation approach.

I. INTRODUCTION

Recent concern in environmental aspects of increasing energy demand, responding to global scientific and public consensus on disturbances in natural CO₂ cycle, triggers actions and policies regarding renewable energy sources introduction into primary energy mix worldwide.

Pioneer studies in 1965 – 1969 defined the Ďurkov area as the most appropriate for geothermal power production in Slovakia [1]. However, there is no project that operates nowadays. Besides high T.D.S. content in brine, conflicts of interests or technical limitations, any existence of geothermal power station reflects typical feature of complex projects – high investment costs and initial economical uncertainties [2]. CO₂ savings derived environmental subsidies become relevant in project economical considerations.

Submission evaluates CO₂ mitigation potential applying substitution approach for a cogeneration based – ORC geothermal power plant project in the Ďurkov area. Presented results can contribute on forthcoming enviro-economical studies once the project applies for global CO₂ credits market. Authors try to explain methodology and provide essential basement and implications for preliminary environmental and cost-effectiveness analysis in akin projects worldwide.

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II. KOŠICE BASIN – CLIMATE AND PRIMARY ENERGY MIX

A. Climate

Located in the SE part of the East Slovakian Basin, the Košice Basin is dominant in climate conditions of warm regions, split into moderately humid (south) and moderately dry subregions (north), all surrounded from the east and west with moderately warm, humid, highland-type subregion [3] (Fig. 1), defining 220 heating days and 9.5 °C mean annual temperature [4].

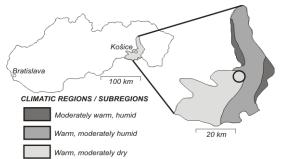


Fig. 1. The Košice Basin – schematic sketch and climatic regions.

B. Primary Energy Mix – Electricity and Heat Supply

Slovak Republic, high-advanced economy is still fossil fuels oriented, regarding a heat and electricity supply for industry or municipalities, where renewables cover 19,8 % of power and less than 7 % of heat production only (Table I) [5]. In the Košice Basin, considering district urban heat and power supply, fossil fuels control the whole market (Table II) [6].

TABLE I: PRIMARY ENERGY MIX – HEAT AND POWER SUPPLY (SLOVAKIA)

Primary energy	Black coal	N. Gas	Oil	Renewables
Heat	23 %	53 %	12 %	7 %
Power	15 %	6 %	1 %	19,8 %

TABLE II: PRIMARY ENERGY MIX – HEAT AND POWER SUPPLY (KOŠICE B.) Primary energy Black coal N. Gas Oil Renewables Heat 85 % 15 % - Power 60 % 28 % 12 % -

III. ĎURKOV GEOTHERMAL POWER STATION PROJECT

Geothermal sources in the Ďurkov area associate with Mesozoic carbonates at depths of 1250 - 2600 m [7], where temperature varies 100 - 150 °C (trend increases SE-wards). By now, three wells (GTD-1, GTD-2, GTD 3) are in a trial operation [8] identifying high saline fluids with total dissolved solids at 20 - 35 g.l⁻¹ and 0.07 g.l⁻¹ of free CO₂ [9].

Recent power station project plans to operate geothermal power plant with 2 exploitation (GTD-2, GTD-3) and 1 reinjection (GTD-1) wells at total 115 kg.s⁻¹ extraction rate and wellhead pressure of 1,4 MPa [10]. Call for energy efficiency improvements predefined the project to operate as cogenerating – a power production waste heat is then used in optimized district heating grid. High geothermal salinity limits the station to operate as binary (Organic Rankine Cycle based). While in a regard to national directives the power production counts the whole year, the district heating is optimized for 220 days – a number that corresponds to required mean temperature interval of -13°C to +13 °C.

Output parameters are outdoor temperature and comfortable indoor temperature in the district heating controlled thus vary in time as extracted brine mass diverts for bypass to provide preheating high enough for a heat supply. While at minimum critical temperature ($T_{out} = -13 \, ^{\circ}\text{C}$) the heat potential duty reaches 15 844 kW_{th} and power turbine output counts 1 654 kW_e, at maximum temperature ($T_{out} = 13 \, ^{\circ}\text{C}$) the heat output decreases to 6 628 kW_{th} and power produced in the turbine turns to 3100 kW_e (tab. III) However, turbine of installed power output over 3 394 kW_e is required according to maximum output calculated for T_{out} of $2-4 \, ^{\circ}\text{C}$ [11].

TABLE III: POWER PLANT PROJECT – OUTPUT DESIGN CRITERIA VS. TOUT

T _{out} (°C)	Heat output (kW _{th})	Power output (kW _e)
-13	15 884	1 654
0	10 764	3 358
3	9 788	3 394
13	6 628	3 100
17	-	2 840

Based on efficiency analysis of turbine inlet pressures and power output, a most proper working fluid for power turbine is n-Pentane, even of considerably higher costs in comparison to other fluids (e.g. Isobutane). N-Pentane allows the turbine to keep stable efficiency of 85 %. District heating system uses fresh water as a working fluid in a cycle [12].

If we accept a system to operate constant as a base-load, power capacity of 26,1 GW $_{\rm he}$ and heat capacity of 83 GW $_{\rm hth}$ are yearly obtainable for a public supply. Later in calculations, both outputs enter relations for CO $_2$ reduction – mitigation evaluation as energy duty.

IV. METHODOLOGY

Several methods for CO_2 emission reduction evaluation are introduced into praxis nowadays – e.g. [13], [14], mostly derived from peak-load analysis and substitution. The Ďurkov project, however, operates as base-load. Consequently, here is the reduction understood as a mitigation process [4], resulting from emittive fossil fuels substitution either in a heat and power production by low emittive renewable – geothermal, in the same process at the same intensity [15].

Let us state the gross savings (CO_{2g}) in combined heat and power production are bound to covered energy duty (Q_{ed}), local primary energy mix (P_{pem}) defining substitution rate for each fossil fuel, and fossil fuels emission factor (EF_{ff}) – (1)

$$CO_{2g} = \sum \left(Q_{ed} \cdot P_{pem} \cdot EF_{ff} \right) \tag{1}$$

where: CO_{2g} – yearly gross savings ($tCO_2.yr^{-1}$), Q_{hp} – heat and power duty ($TJ.yr^{-1}$ or $MWe.yr^{-1}$), P_{pem} – primary energy mix proportion (-), EF_{ff} – carbon dioxide emission factor of fossil fuels ($tCO_2.TJ^{-1}$ or $tCO_2.MWe^{-1}$).

Operation of geothermal power plant defines emissions produced $-CO_{2p}(2)$ during its run, controlled by duty of both processes (Q_{ed}) and emission factor of geothermal fluid (EF_{geo}) calculated from hydrogeochemical sampling:

$$CO_{2p} = \sum \left(Q_{ed} \cdot EF_{geo} \right) \tag{2}$$

where: CO_{2p} – yearly CO_2 produced at the station (tCO_2 .yr⁻¹), Q_{hp} – heat and power duty ($TJ.yr^{-1}$ or $MWe.yr^{-1}$), EF_{geo} – emission factor of geothermal source ($tCO_2.TJ^{-1}$ or $tCO_2.MWe^{-1}$)

Subtraction of CO_2 produced from gross savings itinerary results in yearly real carbon dioxide savings – CO_{2r} (3):

$$CO_{2r} = CO_{2g} - CO_{2p}$$
 (3)

where: CO_{2r} – yearly real carbon dioxide savings (tCO_2 .yr⁻¹), CO_{2g} – yearly gross CO_2 savings (tCO_2 .yr⁻¹), CO_{2p} – yearly CO_2 savings produced at the site (tCO_2 .yr⁻¹).

If the average lifetime (LT_{gp}) of cogeneration projects at 40 years is accepted [6], real savings expected at the end of operation period are projected as cumulative – CO_{2r} c (4):

$$CO_{2r_c} = CO_{2r} \cdot LT_{gp} \tag{4}$$

where: $CO_{2r_{-}c}$ – cumulative real savings (tCO₂), CO_{2r} – yearly real CO₂ savings (tCO₂.yr⁻¹), LT_{hp} – lifetime (yr)

Substitution of yearly gross savings into (4) with preserved lifetime LT_{gp} turns to cumulative gross savings (CO_{2g_c}). A ratio of real cumulative over gross cumulative savings expresses in reduction effectiveness η_R (5) [16]:

$$\eta_{R} = \left(\frac{CO_{2r_{-}c}}{CO_{2g_{-}c}}\right).100\tag{5}$$

where: η_R – reduction effectiveness (%), CO_{2r_c} – cumulative real savings, CO_{2g_c} – cumulative gross savings.

V. RESULTS AND COMMENTS

A. Carbon Dioxide Savings

Substitution approach expects the power station project to supply energies constantly 24 hours a day, as in a case of conventional combined heat – and - power plants of a base-load service.

In both processes, the substituted bulk of energy duty equals 100 % with proportion related to primary energy mix for heat and power (Table II). In a heat production savings, the accepted duty (Q_{dh}) of 83 GW_{hth} equals 298, 4 TJ yearly the project is able to cover. Substitution of PEM and emission factors typical for Slovak Republic [17] - [18] (Table IV) into (1) defines yearly gross CO₂ savings from a heating section of 26 811 tCO₂.yr⁻¹, as a result of partial coal (24 349 tCO₂.yr⁻¹) and natural gas (2 461 tCO₂.yr⁻¹) removal (Fig. 2)

TABLE IV: EMISSION FACTORS AND GROSS CARBON DIOXIDE SAVINGS

Fossil fuels	Emission factor [t.TJ ⁻¹]	Emission factor [t.MW _h ⁻¹]	CO _{2g} (heat) [tCO ₂ .yr ⁻¹]	CO_{2g} (power) [$tCO_2.yr^{-1}$]
Total coal	96	1,04	24 349	16 255
Natural gas	55	0,55	2 461	4 011
Oil products	-	0,9	-	2 813
Geothermal	0,27	0,002	-	-

Analogously according to (1) in a power production section, substitution of related emission factors (Table IV) and proportion factors (Table II) for partial yearly gross CO_2 reduction turns to total 23 080 t CO_2 .yr⁻¹ removal potential as a sum of partial emissions avoided from substitution of different fossil fuels (Table IV). A sum of bulk reduction from heat and power production defines then total yearly gross savings – CO_{2g} of 49 891 t CO_2 .yr⁻¹ (Fig. 2).

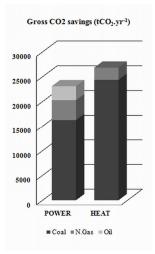


Fig. 2. Graphic display of partial gross CO_2 savings in power and heat production

Observed contrasts in partial CO₂ savings clearly reflect proportion of fossil fuels on heat and power production as well as correspond to various emission factors.

Each installation and operation of geothermal power plant defines a need for CO_2 related to utilizing of geothermal fluids definition. The carbon dioxide produced (2) then reflects hydrochemistry of thermal fluids, essentially free CO_2 compound and functions energy duty the fluid covers in a heat ($Q_{ed} = 298,4$ TJ) and power ($Q_{ed} = 26\,050$ MW_{he}) production with calculated [19] emission factor of thermal fluid for both processes (table IV). Solution of (2) gives then $132 \text{ t.CO}_2.\text{yr}^{-1}$ of carbon dioxide produced at the station (CO_{2p}) as a sum of partial emissions on a heat production ($80tCO_2.\text{yr}^{-1}$) and power production ($52\ tCO_2.\text{yr}^{-1}$) side.

With total yearly gross savings ($CO_{2g} = 49~891~tCO_2.yr^{-1}$) and in-situ emissions produced during utilization ($CO_{2p} = 132~tCO_2.yr^{-1}$) predicted, solution of (3) defines then real carbon dioxide emissions mitigated (CO_{2r}) itinerary at a level of 49 578 t $CO_2.yr^{-1}$. As emissions potentially produced at the station represent 0,2 % from a bulk saved, the gap is almost negligible and the fluid is considered emissions- inactive [15].

Recent design of combined heat and power geothermal plants expects projects to operate at least for 40 years [20], a period that is set as lifespan (LT_{gp}) to enter calculations of

cumulative gross (CO_{2g_c}) and real (CO_{2r_c}) CO_2 savings(4). Relation understands cumulative savings as itinerary of emissions the project mitigated at the end of operation, and calculates with both, gross (CO_{2g}) and real (CO_{2r}) bulks. As a result, 1,995 MtCO₂ of gross cumulative or 1,990 MtCO₂ of real cumulative savings are expected for the project (Fig. 3, table V) in case the system operates constantly as expected for a base-load supply.

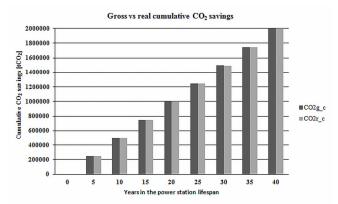


Fig. 3. Screen of cumulative real CO₂ savings

TABLE V: SUMMARIZING TABLE ON CARBON DIOXIDE SAVINGS

Value	Gross CO ₂ savings [MtCO ₂]	Real CO ₂ savings [MtCO ₂]	Power production [GW _h]	Heat production [TJ]
Yearly	0,0498	0,04975	26,1	298,4
Cumulative	1,995	1,990	1 044	11 936

B. Environmental Economics Considerations

Every geothermal project consideration meets unique limits regarding economical investment aspects. Investment costs in power-plant projects compose of a) exploration and resource confirmation, b) borehole drilling campaign, c) surface facilities and infrastructure emplacement and d) power plant design [21]. If we assume overall installation costs for a project for both, power and heat production at -6400 €.kW⁻¹, and add to an investment analysis expected operation and maintenance costs at 190 €.kWe⁻¹.yr⁻¹ [22], with optimized installed plant for 40 years projected lifespan at installed capacity of 3 500 kWe and heat production installed capacity of 16 MW_{th}, investment costs may roughly reach 64,6 mil. €. This is an amount potential developer (private or national-owned) should consider in preliminary economic feasibility studies. By a contrast, a mean selling price of 0,03 €.kWh⁻¹ for electricity and 15 €.GJ⁻¹ can be expected in local conditions [23]. Additionally, with yearly real carbon dioxide savings known (49 578 tCO₂), project can apply for environmental government subsidies regarding a CO₂ carbon credit market at a level of $6 \in t^{-1}$ [5]. Yearly environmental subsidies then can contribute with 0,3 mil. € on benefits side. A simple payback period calculated is then 2,32 years. However, such an analysis is clearly preliminary and detailed study is needed, where yearly incomes will depend on initial energy production and then break-away energy prices.

C. National Reflections – Towards the EU Road Map National targets for EU member countries regarding

introduction of renewables into primary energy mix in heat and power production defined proportion the Slovak Republic is supposed to achieve in 2020 for 14 % on heat and 31 % on power production [24]. Set-up targets are mandatory to meet under optional legal and financial penalties.

By now, renewables share 7 % on heat and 19,8 % on power (large hydro included) or 2,3 % (without large hydro plants) [5].

In case the project will operate, yearly power supply for a grid will reach 26.1 GW_{he} . In primary energy mix we subtract the electricity produced from recent proportion of fossil fuels according to their share in electricity sector. As the total electricity generated yearly counts 26.155 GW_{he} , geothermal project power supply will take 0.1 %. Then, proportion of renewables will increase for 19.9 % (large hydro included) or 2.4 % (without large hydro).

Actual geothermal yearly heat production in Slovakia reaches 144 TJ defining its 0,3 % proportion on total national heat supply (42 210 TJ). Constant co-generated geothermal heat delivery from a project into a mix calculated for 298,4 TJ yearly, balanced with energy mix related subtraction of coal and gas in a heat delivery, will lead to increase of geothermal proportion up to 1,05 % and increase of renewables share on heat production from 7,04 % to 7,8 % (Fig. 4).

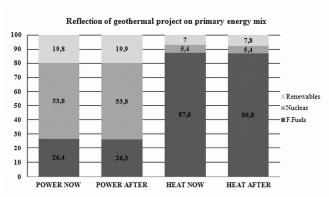


Fig. 4. Impact of geothermal system implementation for a power and heat supply renewable contribution towards the EU road map.

Observed increase of renewables proportion on heat and power national market imply the geothermal sector may not be able to cover the gap between recent situation and targets in the EU road map individually. However, while the Košice Basin is among three perspective localities for a geothermal power supply [25], thus possibilities of growth in geothermal power are rather unlikely, 26 areas perspective for geothermal heat production are identified [26] with a total thermal potential of 6 653 MW_{th} [27], providing a background high enough for rapid improvements. Then, every national progress towards the EU road map targets is a question of government financial and technical support – supposed-to-be motivated by moral, legal and environmental merits.

D. Limitations and Adds

Authors accent the study is a background for potential ongoing detailed research. Additional approach is definitely needed considering operation characteristics of geothermal, combined heat and power binary plant projected, as well as detailed economic and environmental-economic analysis of a market is necessary. Data used in calculations of carbon

dioxide savings are kept constant in time, however, they may seasonally vary.

VI. CONCLUSIONS

The substitution approach for carbon dioxide savings evaluation is presented in the paper on a case study on actual considered geothermal power plant project in the Ďurkov area, Košice Basin, eastern Slovakia. Later on, results are nominally analyzed and reflected regarding project environmental economics and impact for a national primary energy mix scheme towards the EU road map set-up targets.

Essential philosophy of the approach understands reduction as a mitigation-substitution process, within that CO_2 intensively emittive fossil fuels are replaced with a renewable source of low CO_2 emissions intensity in the same process and nominal duty. Analyzed model of a power plant operates as binary and base-load at combined, heat-and-power principle.

Introduction of the power plant into the heat and power grid may contribute with overall yearly gross 49 891 tCO₂ mitigated, out of that 28 811 tCO₂ refer to fossil fuels substitution in a heat and 23 080 tCO₂ to power production sector (corresponding to actual fossil fuels regional energy mix proportion). Use of geothermal fluids leads to yearly potential in-situ emissions of carbon dioxide evaluated for 132 tCO₂.yr⁻¹ characterizing fluid as carbon-inactive. After subtraction of emissions produced from a gross itinerary, yearly real CO₂ savings calculated drop negligibly down to 49 578 tCO₂. If the 40 years lifespan of a geothermal project is accepted, cumulative savings at the end of a period increase up to 1,995 tCO2 of gross or 1,990 tCO2 of real bulk reduced. Carbon dioxide emission reduction potential then reflects in potential environmental subsidies at yearly rate of 0,3 mil. €, contributing on a project's payback period shortening.

Even of proven environmental impact and relatively low (preliminary) calculated payback period (2,32 years), introduction of projected plan producing 26,1 GW $_{\rm he}$ of power and 298,4 TJ of heat yearly will not dramatically effect national primary energy mix. Observed 0,1 % upturn in renewables proportion on power and 0,8 % on a heat production will not solve a nations' rough path to meet EU set-up targets regarding renewables proportion on energy mix.

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Miroslava Popovičová Was born in 1985 in Košice, graduated in Thermal Energy and Gas Industry program at Dept. of Furnaces and Thermal Technology at the Technical University of Košice in 2008 awarded with a Bc. (B.Sc.) degree. After that she successfully graduated in Geothermal energy specialization at the RES | The School for Renewable Energy Science, Akureyri, Iceland in 2010, achieving the M.S. (M.Sc.) degree, prior to graduation as Ing.

(M.S., M.Sc.) in Energy study program at Dept. of Furnaces and Thermal Technology at the Technical University of Košice in 2010. Since September 2010 she is an internal Ph.D. student at Dept. Of Furnaces and Thermal

Technology in study program of Energy, with a focus on design and criteria optimalization of ORC – binary based geothermal systems.

Her primary research activities relate to definition, optimization and modeling of design criteria for binary and cogeneration-operated geothermal power plants, with a most of the scope set at the Košice Basin. Affine to her research topics, she published or submitted several papers about the topic.

Dipl. Eng. Popovičová is a member of Dept. of Furnaces and Thermal Technology as internal doctoral student, being active in research and lecturing.



Ladislav Tometz was born in Košice (Slovakia) in 1953 graduated and was awarded with the Dipl. Eng. (M.Sc.) degree in Mining geology at the Faculty of Mining, Technical University of Košice. After the study he spent fifteen years in praxis and applied research, focused at hydrogeology, environmental geology and engineering geology. In 1995 he became a lecturer at the Department of Geology and Mineralogy – Technical University of Košice. Later in

2000, Ladislav Tometz successfully gained his Ph.D in Environmental geology and Hydrogeology. In 2008 he was appointed the Associate Professor in hydrogeology, environmental geology and engineering geology.

His publications focus at environmental threat, pollution or redevelopment of hydrogeological environment and shallow soils, regional evaluation of hydraulic rock properties and groundwater movement. A most of published works scope, however, utilization, source management or evaluation and preservation of shallow to deep groundwater reservoirs.

Assoc. Prof. Tometz was a head of Department of Geology and Mineralogy (predecessor of current Institute of Geosciences) at the Technical University of Košice in 2002 – 2007. Now he is active as a chair in Slovak Hydrogeological Association and a corresponder and reviewer of the Groundwater Journal (the journal of Slovak Hydrogeological Association). Since awarded with the PhD., he also became stable member of examining commission for Bachelor's, Master's and PhD programs at the Technical University of Košice and the Commenius University in Bratislava. As the Associate Professor, he is a Ministry of Education acknowledged supervisor in undergraduate, graduate and post-graduate programs at the Technical University of Košice.