

Electronic Supporting Information (ESI) to accompany by:

Metal-Organic Frameworks with Potential for Energy- Efficient Adsorptive Separation of Light Hydrocarbons

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1. MOF structures investigated for the light hydrocarbon separations

Table S1 summarizes the structural data on 19 different MOFs synthesized in this study for the purpose of evaluating their efficacies in separation of light hydrocarbon mixtures. The chosen MOFs cover a wide range of framework types, such as ones with open metal sites (e.g. **MgMOF-74**, **CoMOF-74**, **CuBTC**), mixed metallo-ligands (M'MOFs), etc. *Figure S1* presents the single-crystal structures of some typical MOFs such as **CuBTC**, **UTSA-20**, **MOF-505** (isostructural with **PCN-16**, **NOT-101** and **NOTT-102**), and **UMCM-150**. The organic linkers used to construct MOFs investigated are shown in *Scheme S1*.

Table S1. Structural data on the different MOFs evaluated in this study for C₁/C₂/C₃ separation.

MOFs	Langmuir surface area [m ² g ⁻¹]	Pore volume [cm ³ g ⁻¹]	Framework density [kg m ⁻³]
CoMOF-74	1448.5 ^a	0.5146	1169
MgMOF-74	1668.5 ^a	0.6071	909
CuBTC (= HKUST-1)	2139.1 ^a	0.7634	879
MOF-505	1703.7 ^a	0.6086	926.5
PCN-16	2809.7 ^a	0.9987	717.9
UMCM-150	3330.4 ^a	1.2086	635.7
NOTT-101	2929.8 ^a	1.0485	683.8
NOTT-102	3590.1 ^a	1.2807	587.2
UTSA-20	1894.1 ^a	0.6745	909.6
UTSA-33a	1024.1 ^a	0.3673	993
UTSA-34a	937.0 ^a	0.3336	889.8
UTSA-34b	1532.6 ^a	0.5419	840.4
UTSA-35a	875.0 ^a	0.3133	1046
M'MOF-2a	939 ^b	0.301	997
M'MOF-3a	551 ^b	0.165	1023
M'MOF-4a		0.289	1126
M'MOF-5a		0.126	1039
M'MOF-6a		0.216	1078
M'MOF-7a		0.045	1037

a) Calculated from N₂ adsorption isotherm at 77 K; b) Calculated from CO₂ adsorption isotherm at 196 K.

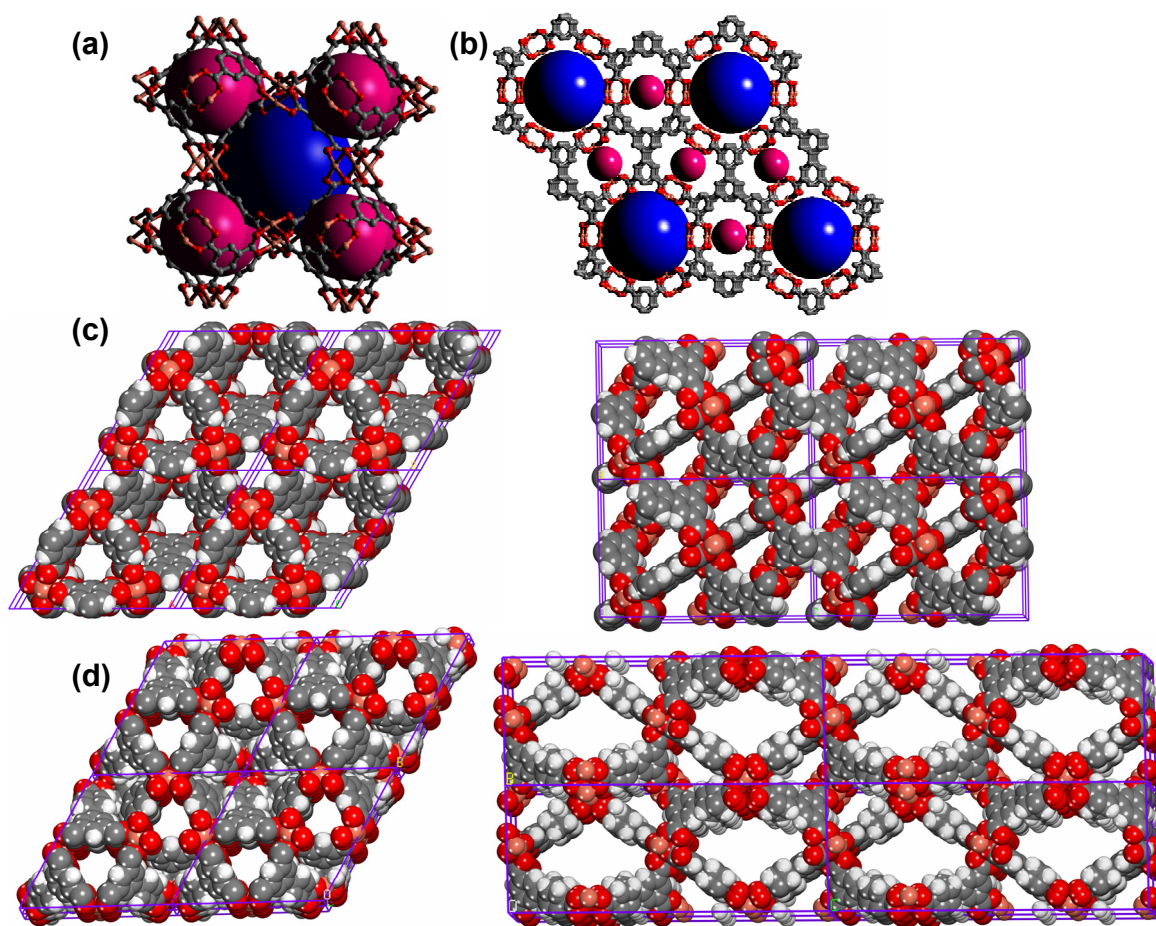
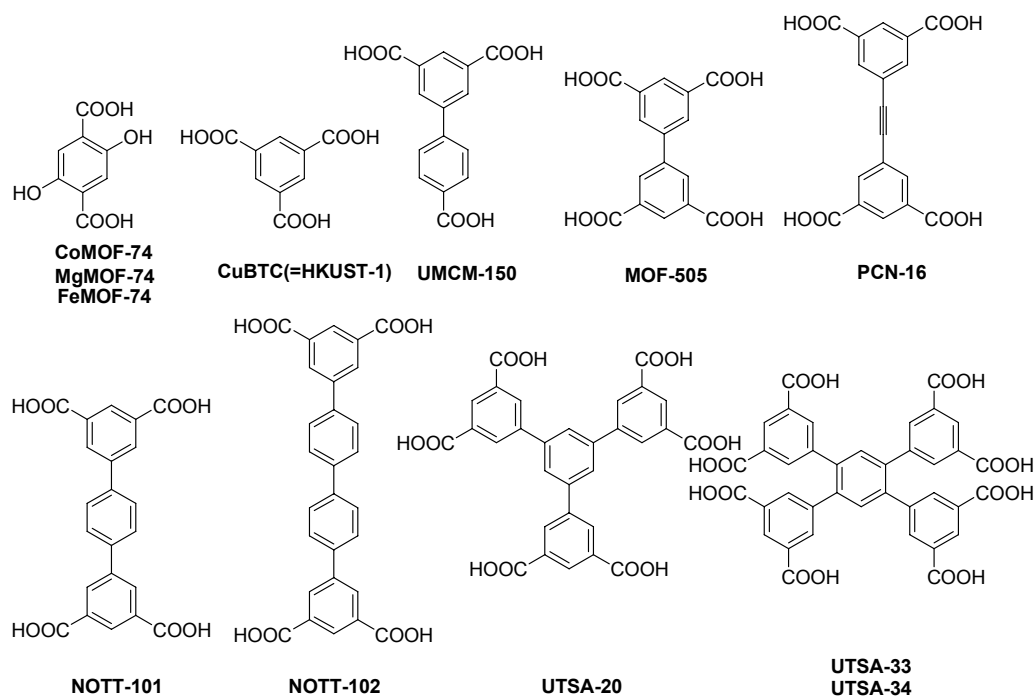


Figure S1. The X-ray single-crystal structures of **CuBTC** (a), **UTSA-20** (b), **MOF-505** (c), and **UMCM-150** (d).



Scheme S1. The organic linkers used to construct the MOFs investigated.

2. Details of synthesis of MOFs

CoMOF-74,¹ MgMOF-74,^{2, 3} CuBTC (= HKUST-1),⁴ MOF-505,⁵ PCN-16,^{6, 7} UMCM-150,⁸ NOTT-101,⁹ NOTT-102,⁹ UTSA-20,¹⁰ UTSA-33,¹¹ UTSA-34,¹² UTSA-35,¹³ M'MOF-2,¹⁴ M'MOF-3,¹⁴ M'MOF-4,¹⁵ M'MOF-5,¹⁵ M'MOF-6,¹⁵ and M'MOF-7¹⁵ were prepared according to the corresponding reported references. The experimental powder X-ray diffraction (PXRD) patterns are in good agreement with the simulated PXRD patterns (*Figure S2*). Their detailed synthetic procedures and activation profiles are given below.

CoMOF-74: 2,5-dihydroxyterephthalic acid (H₄dobdc, 19.3 mg, 97.4 μmol, Aldrich) and Co(NO₃)₂·6H₂O (95.1 mg, 326.8 μmol, Acros) were mixed and dispersed in DMF/EtOH/H₂O (v/v/v, 1:1:1, 8.0 mL) in a vial (20 mL). The suspension was sonicated until homogeneous. The vial was capped tightly and placed in an oven at 100 °C. After 24 h, the vial was removed from the oven and allowed to cool to room temperature. The microcrystals were collected and washed with DMF. The sample was solvent-exchanged with dry methanol at least 10 times, and vacuumed at room temperature for 24 h, and then at 200 °C for 24 h and finally at 250 °C for 8 h to generate the activated sample.

MgMOF-74: 2,5-dihydroxyterephthalic acid (H₄dobdc, 22.2 mg, 112.0 μmol, Aldrich) and Mg(NO₃)₂·6H₂O (95.0 mg, 370.5 μmol, Acros) were mixed and dispersed in DMF/EtOH/H₂O (v/v/v, 15/1/1, 10.0 mL) in a vial (20 mL). The suspension was sonicated until homogenous. The vial was capped tightly and placed in an oven at 125 °C. After 20 h, the vial was removed from the oven and allowed to cool to room temperature. The resulting yellow microcrystals were collected and washed with DMF. The sample was solvent-exchanged with dry methanol at least 10 times. The solvent was removed under high vacuum at room temperature for 24 h, and then at 200 °C for 24 h and finally at 250 °C for 8 h, yielding the activated sample.

CuBTC: A solution of Cu(NO₃)₂·2.5H₂O (124.0 mg, 533.1 μmol, Aldrich) and 1,3,5-benzenetricarboxylic acid (H₃btc, 74.0 mg, 352.1 μmol, Aldrich) in the mixed solvents of DMF/EtOH/H₂O (v/v/v, 1/1/1, 18.0 mL) in a capped vial (20 mL) was kept at 75 °C for 24 h to give green cubic microcrystalline crystals. The fresh sample was guest-exchanged with dry acetone, and outgassed under high vacuum at room temperature for 24 h, and then at 120 °C until the degassed rate is 5 μmHg min⁻¹ to generate the activated sample.

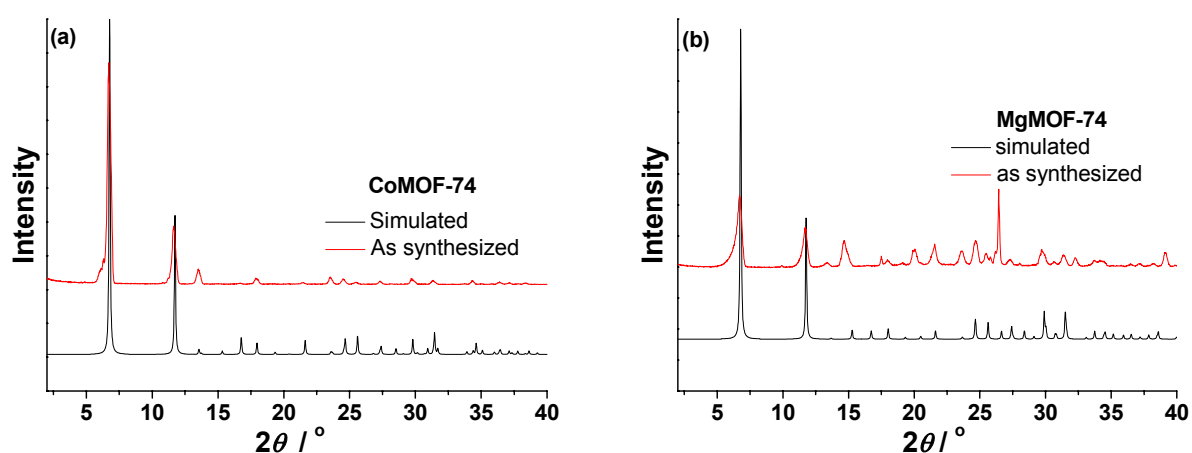
MOF-505: Biphenyl-3,3',5,5'-tetracarboxylic acid (H₄bptc, 50.0 mg, 151.4 μmol) and Cu(NO₃)₂·2.5H₂O (100.0 mg, 429.9 μmol, Aldrich) were mixed and dispersed in DMF/1,4-dioxane/H₂O (v/v/v, 2/1/1, 15.0 mL). The resulting slurry mixture turned clear upon addition of 2 drops of aqueous HCl (37%). The solution was heated at 80 °C for 72 hrs. The fresh sample was solvent-exchanged with dry acetone, and vacuumed at room temperature for 24 h, and then at 120 °C until the degassed rate is 5 μmHg min⁻¹ to yield the activated **MOF-505**.

PCN-16: A mixture of 5,5'-(1,2-ethynediyl)bis(1,3-benzenedicarboxylic acid) (H_4ebdc , 10.0 mg, 28.2 μmol), $\text{Cu}(\text{NO}_3)_2 \cdot 2.5\text{H}_2\text{O}$ (20.0 mg, 86.0 μmol , Aldrich) and 2 drops of HBF_4 (48-50%, fisher) in 1.5 mL of N,N' -dimethylacetamide (DMA) was placed in a vial (20 mL). The vial was capped tightly and placed in an oven at 75 °C for 72 h. The resulting crystals were collected and washed with DMA. The fresh sample was solvent-exchanged with dry methanol, and vacuumed at room temperature for 24 h, and then at 100 °C until the degassed rate is 5 $\mu\text{mHg min}^{-1}$ to yield the activated **PCN-16**.

UMCM-150: Biphenyl-3,4',5-tricarboxylic acid (H_3bpt , 50.0 mg, 174.7 μmol) and $\text{Cu}(\text{NO}_3)_2 \cdot 2.5\text{H}_2\text{O}$ (98.0 mg, mol, 421.3 μmol , Aldrich) were dissolved in DMF/1,4-dioxane/ H_2O (v/v/v, 4/1/1, 15 mL). The solution was placed in a tightly capped vial (20 mL) and heated at 85 °C for 6 h. The crystals were collected and washed with fresh DMF. The sample was solvent-exchanged with dry acetone, and outgassed at room temperature for 24 h, and then at 100 °C until the degassed rate is 5 $\mu\text{mHg min}^{-1}$ to yield the activated **UMCM-150**.

NOTT-101: Terphenyl-3,3'',5,5''-tetracarboxylic acid (H_4tptc , 50.00 mg, 123.0 μmol) and $\text{Cu}(\text{NO}_3)_2 \cdot 2.5\text{H}_2\text{O}$ (100.0 mg, 429.9 μmol , Aldrich) were mixed and dispersed in DMF/1,4-dioxane/ H_2O (v/v/v, 2/1/1, 15.0 mL). The resulting slurry turned clear upon addition of 2 drops of aqueous HCl (36%). The solution was heated to 80 °C and kept at this temperature for 3 days. The sample was solvent-exchanged with dry acetone, and vacuumed at room temperature for 24 h, and at 100 °C until the degassed rate is 5 $\mu\text{mHg min}^{-1}$ to yield the activated **NOTT-101**.

NOTT-102: Quaterphenyl-3,3''',5,5'''-tetracarboxylic acid (H_4qptc , 50.0 mg, 103.6 μmol) and $\text{Cu}(\text{NO}_3)_2 \cdot 2.5\text{H}_2\text{O}$ (100.0 mg, 429.9 μmol , Aldrich) were mixed and dispersed in DMF/1,4-dioxane/ H_2O (v/v/v, 2/1/1, 15.0 mL). The resulting slurry turned clear upon addition of 2 drops of aqueous HCl (36%). The solution was heated to 80 °C and kept at this temperature for 3 days. The sample was solvent-exchanged with dry acetone, and vacuumed at room temperature for 24 h, and then at 100 °C until the degassed rate is 5 $\mu\text{mHg min}^{-1}$ to yield the activated **NOTT-102**.



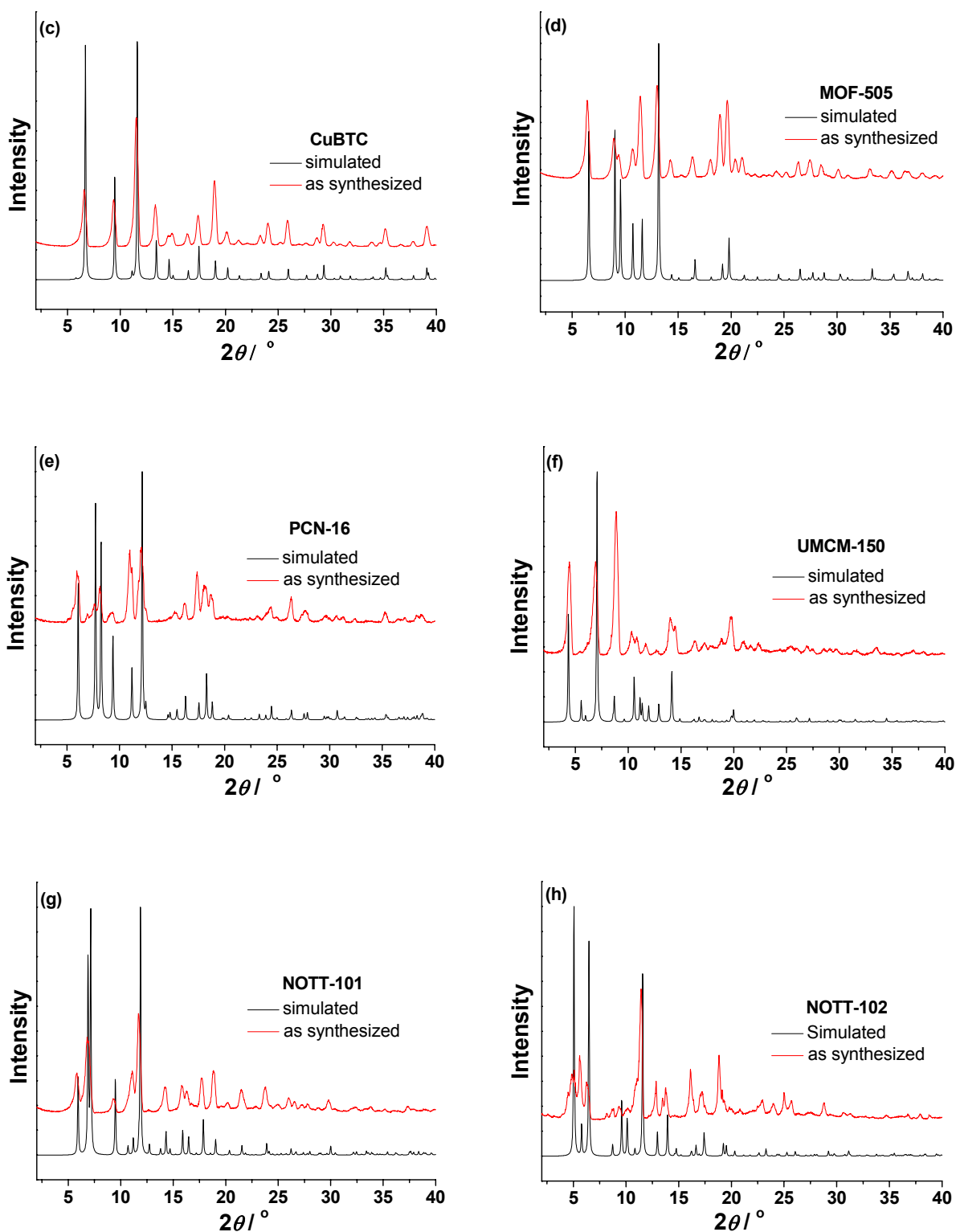
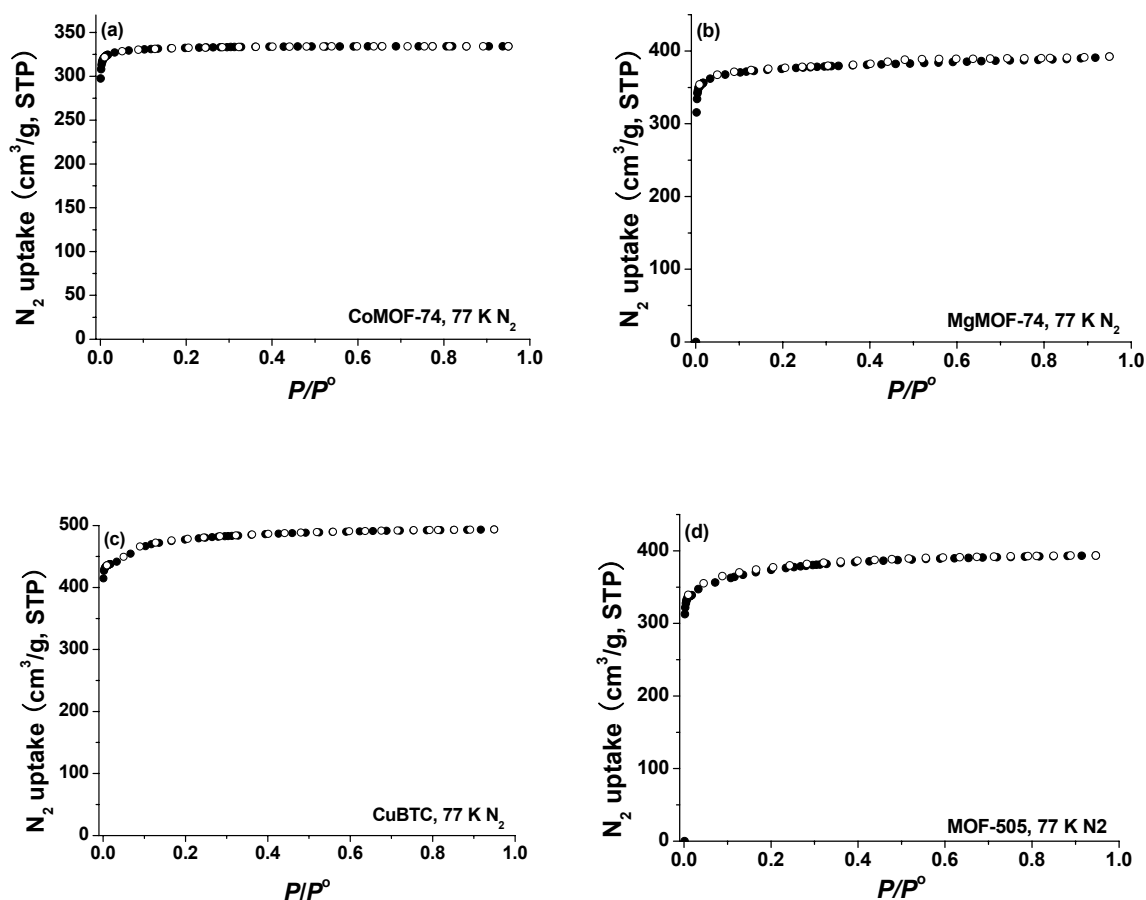


Figure S2. PXRD patterns of CoMOF-74 (a), MgMOF-74 (b), CuBTC (c), MOF-505 (d), PCN-16 (e), UCMC-150 (f), NOTT-101 (g), and NOTT-102 (h).

3. Measurement of pure-component isotherms of light hydrocarbons in different MOFs

A Micromeritics ASAP 2020 surface area analyzer was used to measure gas sorption isotherms. C_2H_2 (atomic absorption grade) was purchased from western international gas & cylinders Inc.; C_2H_4 (2.5 N), C_2H_6 (2.0 N) were purchased from conley gas ltd.; CH_4 (3.7 N), C_3H_6 , and C_3H_8 were purchased from Praxair Inc. and used as received. 100-150 mg of the samples were used in gas sorption measurements and maintained at 77 K with liquid nitrogen, at 273 K with an ice–water bath. As the center–controlled air conditioner was set up at 23 °C, a water bath was used for adsorption isotherms at 296 K.

Before measurement of sorption isotherms of light hydrocarbons, their N_2 isotherms at 77 K were also examined (*Figure S3*), and are in good agreement with the reported data except for **NOTT-101** and **NOTT-102**. Our measured surface areas for **NOTT-101** and **NOTT-102** are higher than those reported by Lin et al,⁹ and are in good agreement with the values obtained from the single-crystal data. The surface areas and pore volumes determined from N_2 isotherms at 77 K were summarized in *Table S1*. *Figures S4-22* present CH_4 , C_2H_2 , C_2H_4 , and C_2H_6 sorption isotherms for all MOFs investigated in the paper. C_3H_6 and C_3H_8 isotherms for **CoMOF-74** are also included in *Figure S4*.



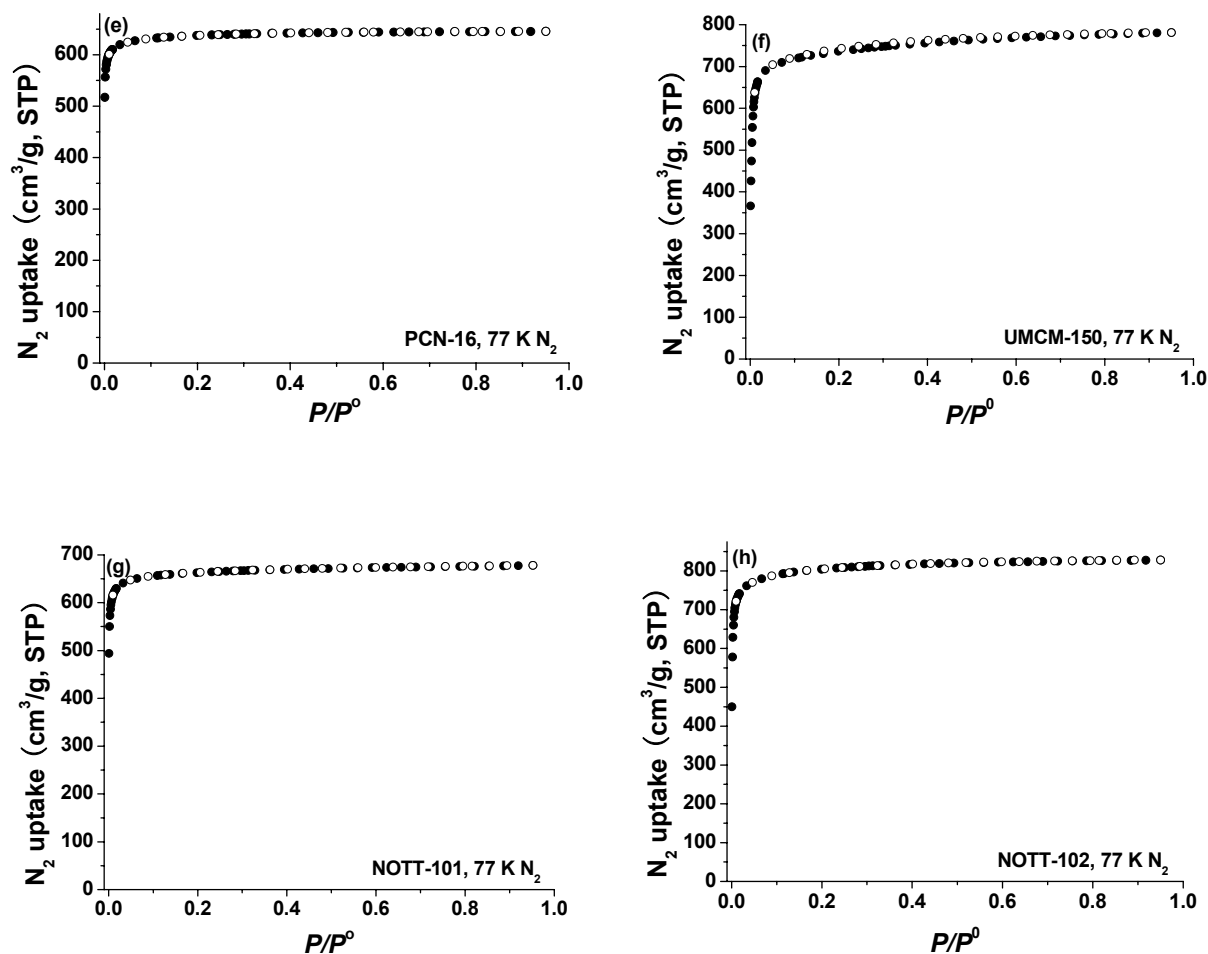


Figure S3. N₂ sorption isotherms of CoMOF-74 (a), MgMOF-74 (b), CuBTC (c), MOF-505 (d), PCN-16 (e), UMCM-150 (f), NOTT-101 (g), and NOTT-102 (h) at 77 K. Solid symbols: adsorption, open symbols: desorption.

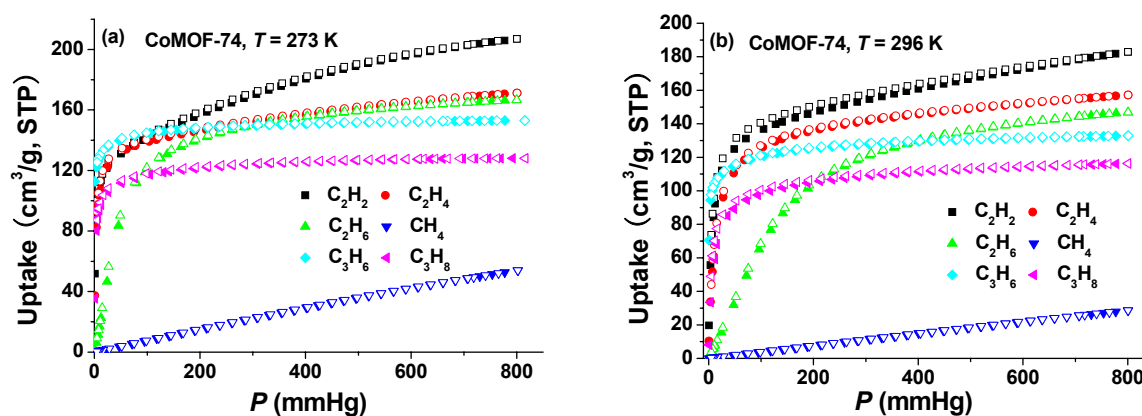


Figure S4. C₂H₂, C₂H₄, C₂H₆, and CH₄ sorption isotherms of CoMOF-74 at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

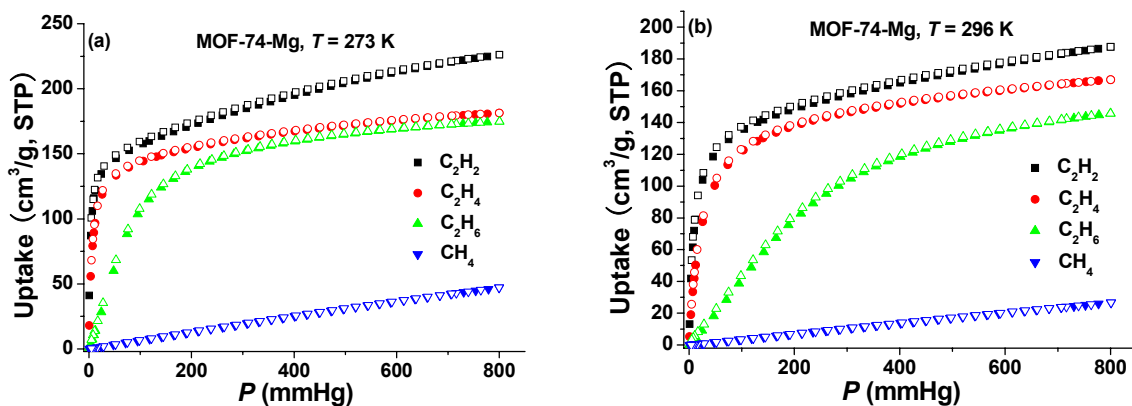


Figure S5. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of **MgMOF-74** at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

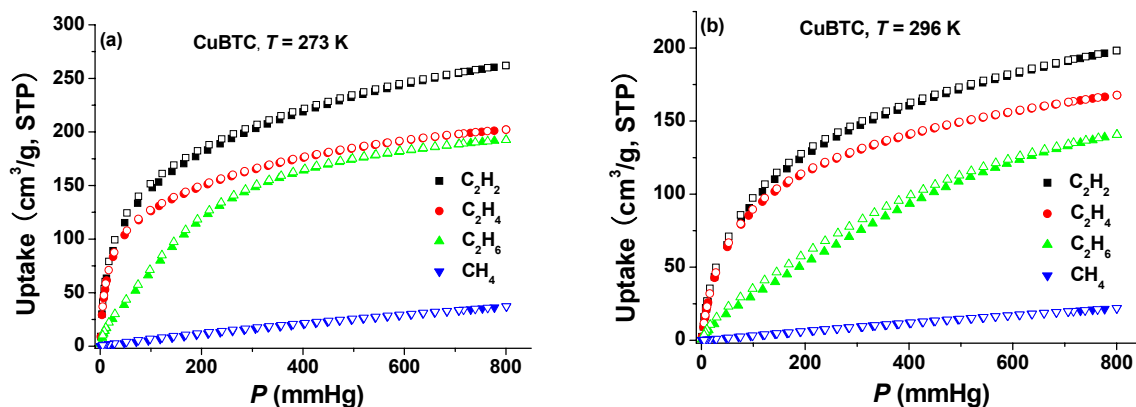


Figure S6. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of **CuBTC** at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

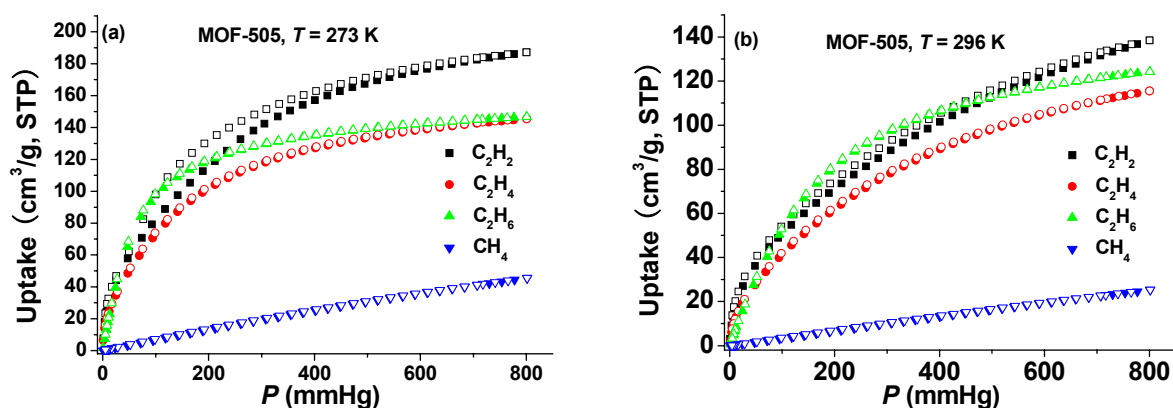


Figure S7. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of **MOF-505** at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

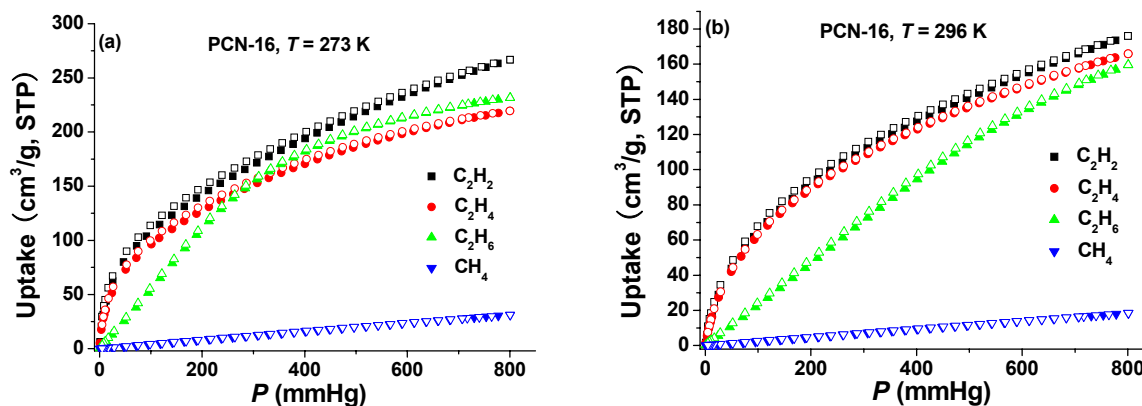


Figure S8. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of PCN-16 at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

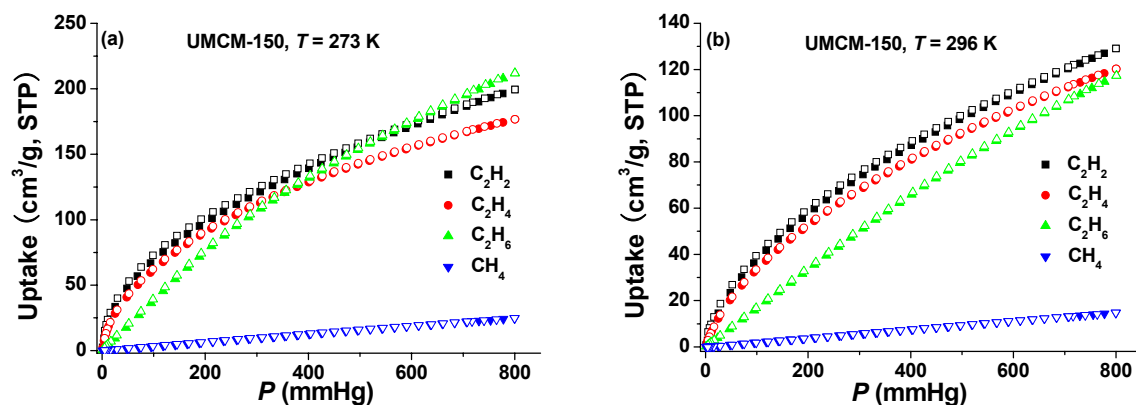


Figure S9. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of UMCM-150 at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

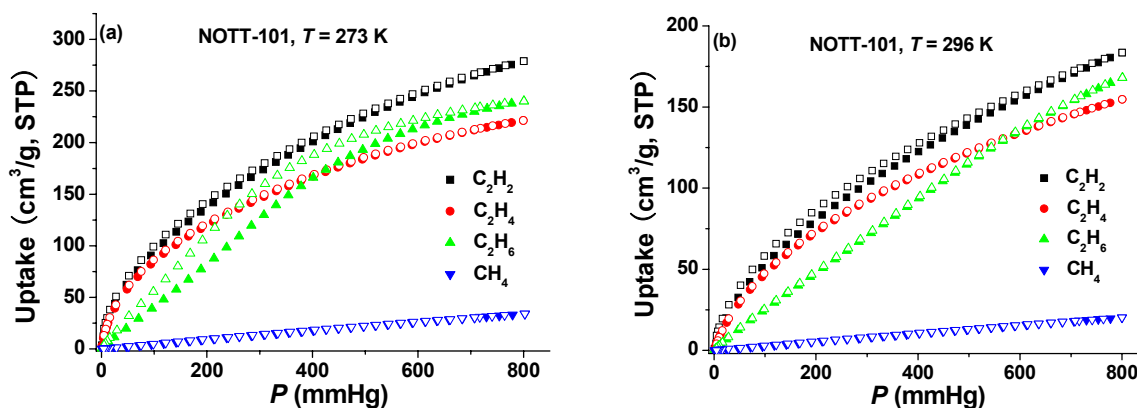


Figure S10. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of NOTT-101 at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

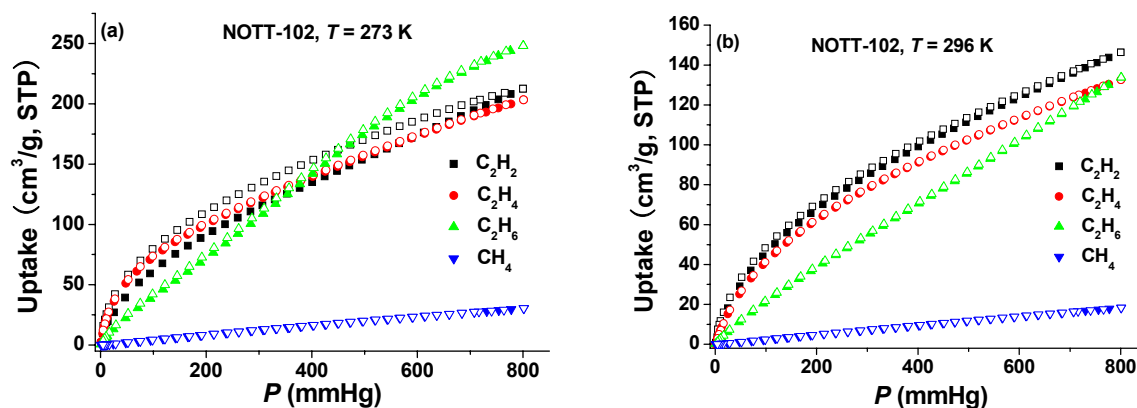


Figure S11. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of NOTT-102 at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

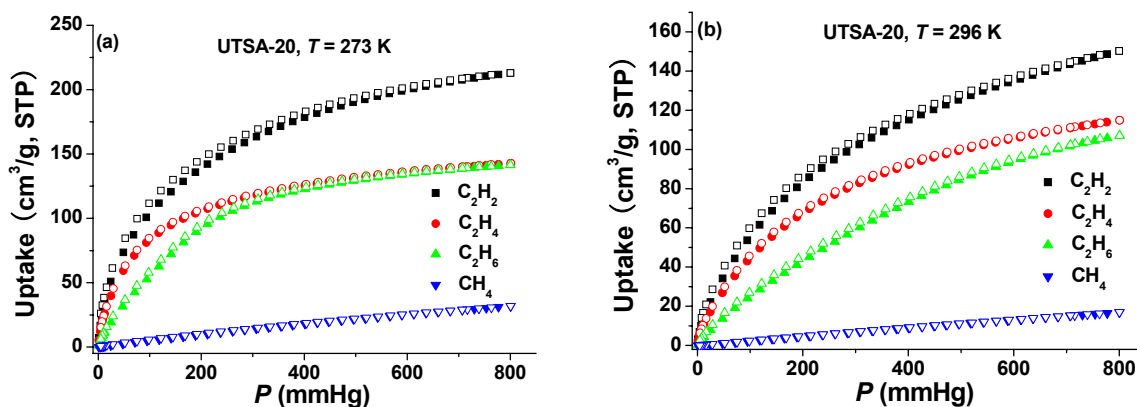


Figure S12. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of UTSA-20 at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

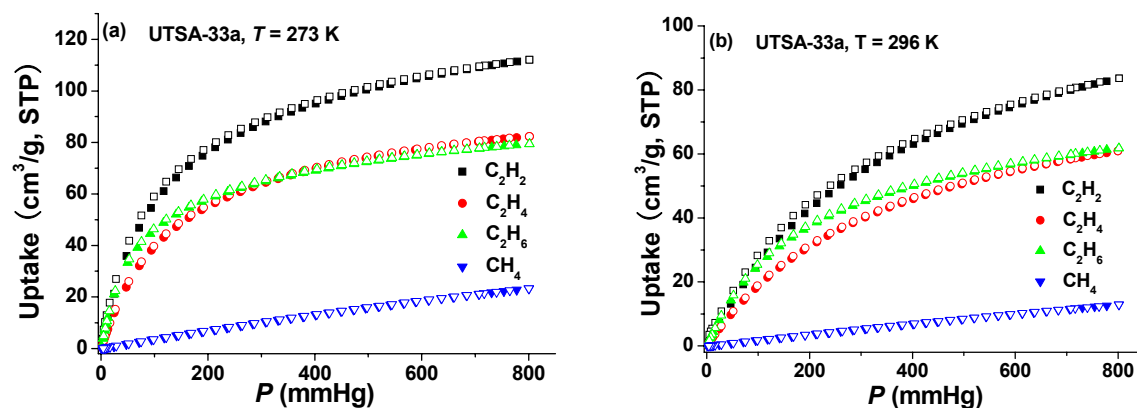


Figure S13. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of UTSA-33a at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

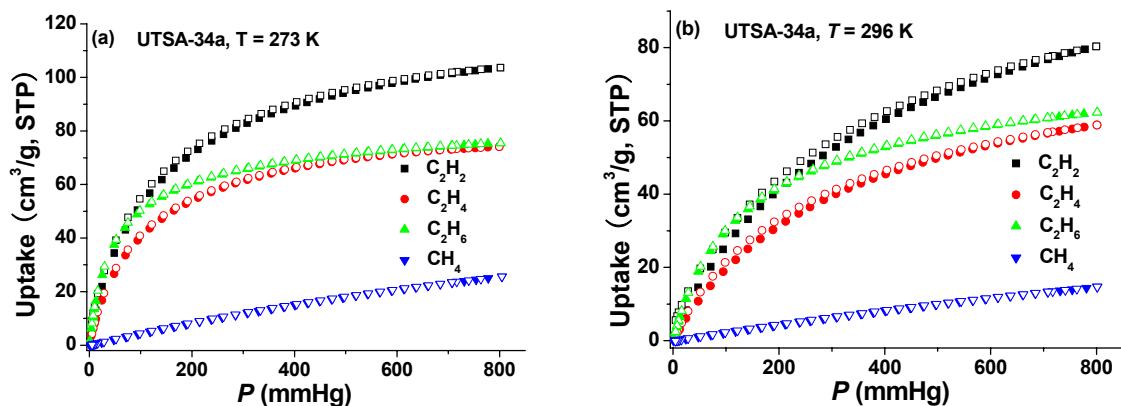


Figure S14. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of UTSA-34a at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

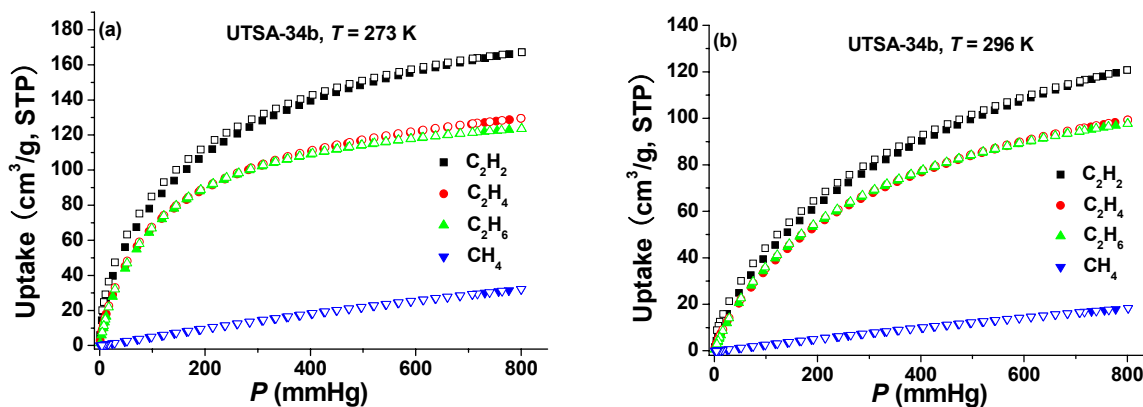


Figure S15. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 isotherms of UTSA-34b at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

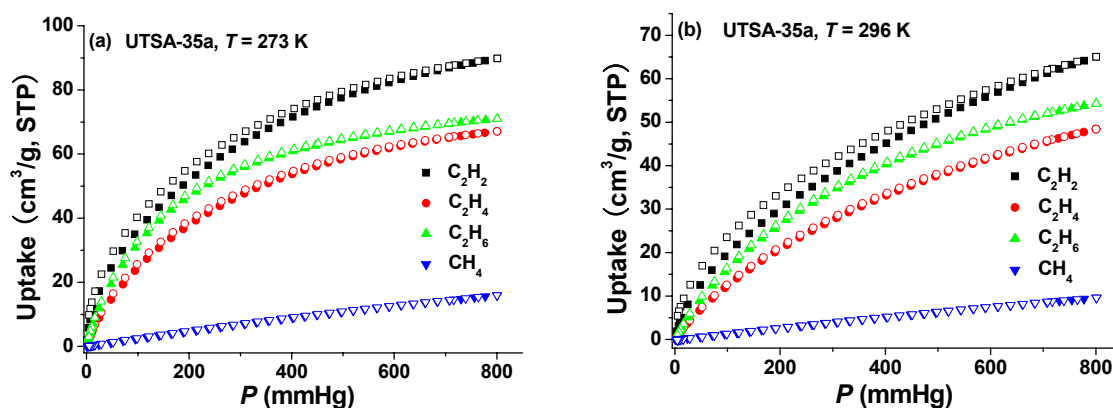


Figure S16. C_2H_2 , C_2H_4 , C_2H_6 , and CH_4 sorption isotherms of UTSA-35a at 273 K (a), and 296 K (b). Solid symbols: adsorption, open symbols: desorption.

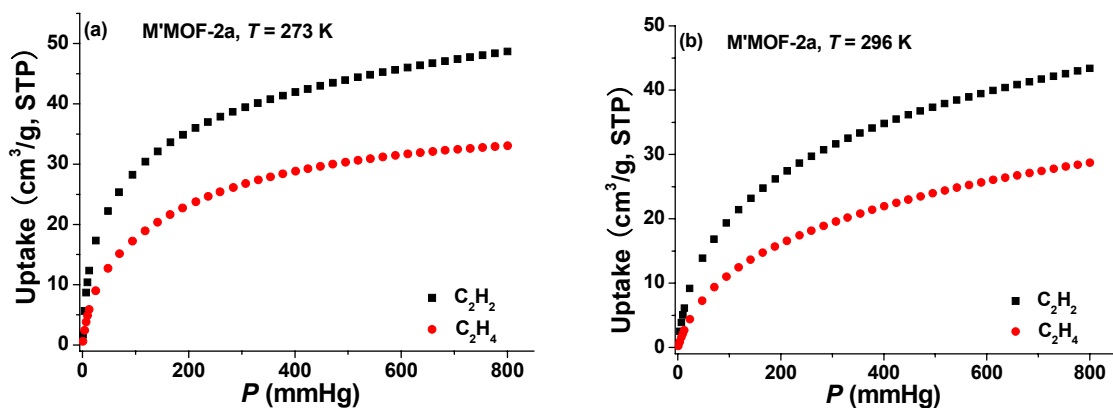


Figure S17. C₂H₂ and C₂H₄ adsorption isotherms of M'MOF-2a at 273 K (a), and 296 K (b).

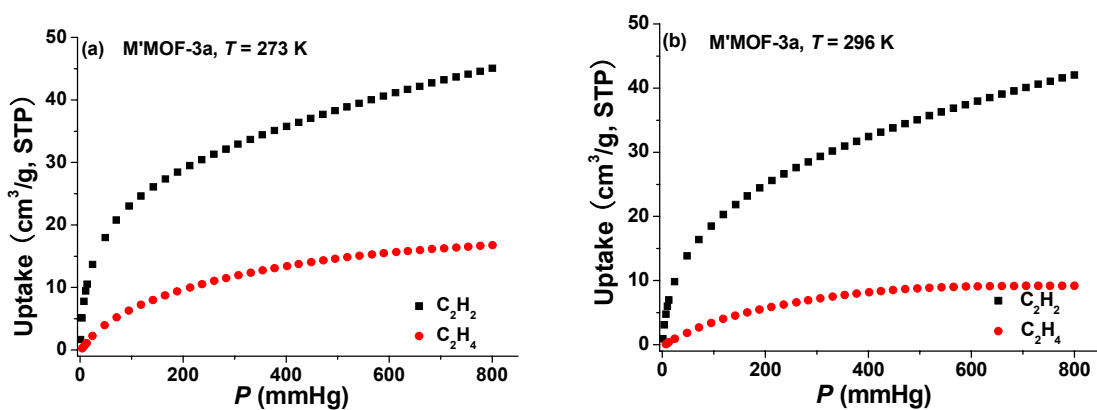


Figure S18. C₂H₂ and C₂H₄ adsorption isotherms of M'MOF-3a at 273 K (a), and 296 K (b).

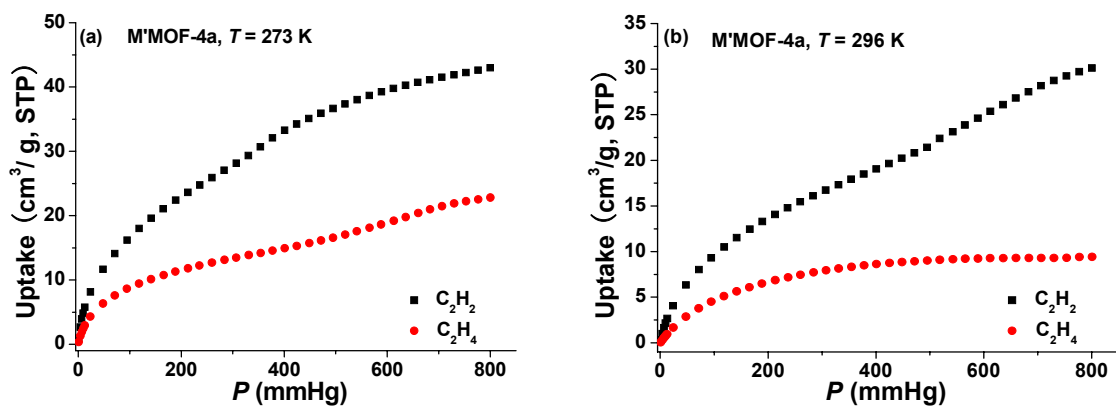


Figure S19. C₂H₂ and C₂H₄ adsorption isotherms of M'MOF-4a at 273 K (a), and 296 K (b).

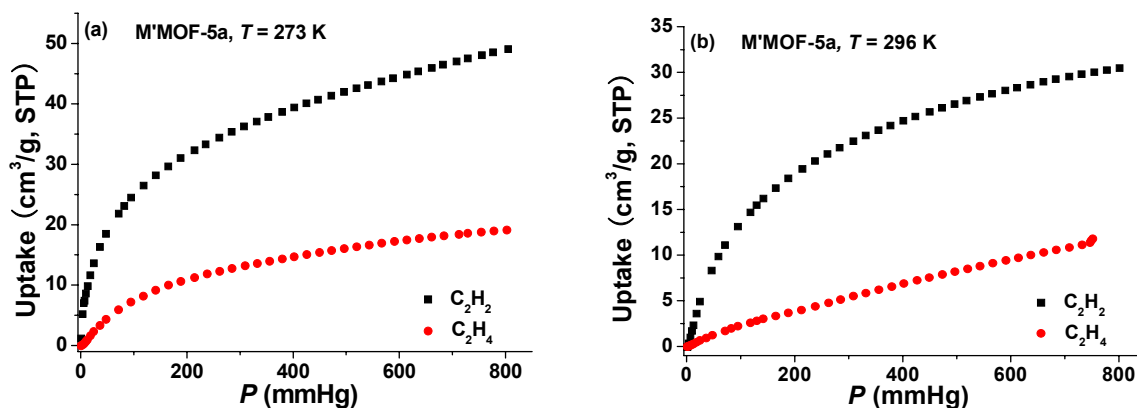


Figure S20. C₂H₂ and C₂H₄ adsorption isotherms of M'MOF-5a at 273 K (a), and 296 K (b).

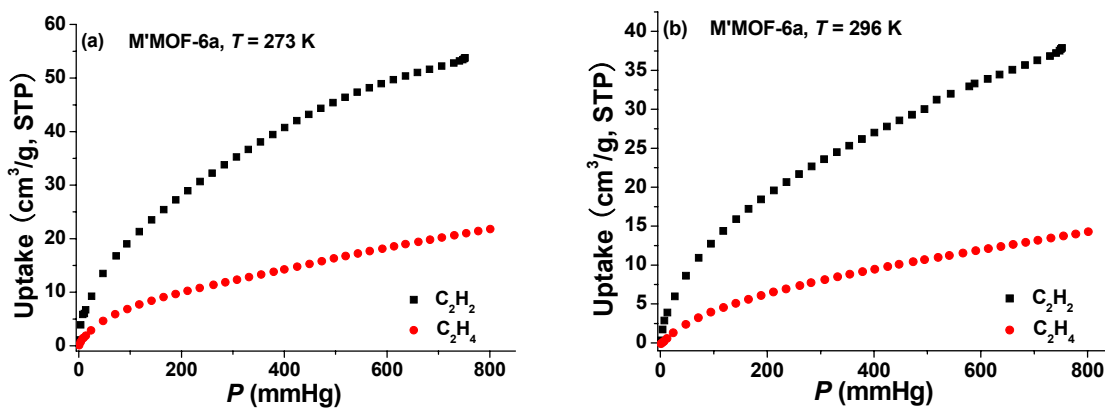


Figure S21. C₂H₂ and C₂H₄ adsorption isotherms of M'MOF-6a at 273 K (a), and 296 K (b).

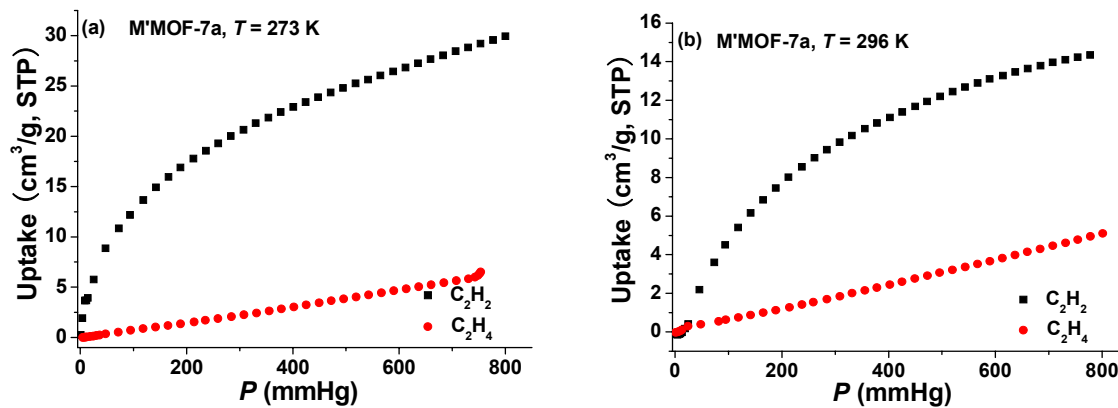


Figure S22. C₂H₂ and C₂H₄ adsorption isotherms of M'MOF-7a at 273 K (a), and 296 K (b).

4. Fitting of pure component isotherms

The measured experimental data on pure component isotherms for the 19 different MOFs, listed in *Table S1*, were first converted to absolute loading using the Peng-Robinson equation of state for estimation of the fluid densities. The pore volumes used for this purpose are those specified in *Table S1*.

The pure component isotherm data for CH₄, C₂H₂, C₂H₄, C₂H₆, C₃H₆, and C₃H₈, expressed in terms of *absolute* loadings, were fitted with the dual-site Langmuir-Freundlich isotherm model

$$q = q_{A,sat} \frac{b_A p^{v_A}}{1 + b_A p^{v_A}} + q_{B,sat} \frac{b_B p^{v_B}}{1 + b_B p^{v_B}} \quad (1)$$

with T -dependent parameters b_A , and b_B

$$b_A = b_{A0} \exp\left(\frac{E_A}{RT}\right); \quad b_B = b_{B0} \exp\left(\frac{E_B}{RT}\right) \quad (2)$$

The fitted parameter values for the 19 different MOFs, listed in *Table S1*, are presented in *Tables S3-S21*.

5. Pure component isotherm data from literature sources used in our evaluations of different MOFs

For evaluation of the light hydrocarbon separations with materials other than those synthesized and measured in our own investigations (as listed in *Table S1*), we have evaluated the performance of other MOFs, zeolites etc. using a variety of literature sources. *Table S2* provides the structural data for these additional adsorbents that have been evaluated in our study.

Table S2. Structural data on other materials evaluated in this study for light hydrocarbons separation for comparison purposes.

Adsorbents	Surface area [m ² g ⁻¹]	Pore volume [cm ³ g ⁻¹]	Framework density [kg m ⁻³]
NaETS-10			1968
NaX zeolite	950	0.280	1421
FeMOF-74		0.626	1126
NiMOF-74		0.582	1194
FeMIL-100	2300	1.2	593
ZIF-8	1781	0.515	924

FeMOF-74

For evaluation of the light hydrocarbon separations with **FeMOF-74** (= **CPO-27-Fe** = $\text{Fe}_2(\text{dobdc})$), the experimental pure-component isotherm data for ethyne, ethylene, ethane, methane, propylene, and propane at 318 K, 333 K, and 353 K. are reported by Bloch et al.¹⁶ The measured isotherms reported in their experiments were refitted with T -dependent dual-site Langmuir-Freundlich parameters; these are provided in *Table S22*. For **FeMOF-74**, the separation performance is evaluated at 318 K, the lowest temperature used in their experiments.

MgMOF-74 isotherm data of Bao et al.^{17, 18} and **Dietzel et al.**¹⁹

Bao et al.¹⁸ report experimental isotherm data for CH_4 at 278 K, 298 K, and 318 K in **MgMOF-74** (= **CPO-27-Mg** = $\text{Mg}_2(\text{dobdc})$). Dietzel et al.¹⁹ report isotherm measurements for CH_4 at 283 K, 298K, 313 K, and 343 K in **MgMOF-74**. Our own experimental isotherm data for CH_4 , measured at 273 K, and 296 K are in excellent agreement with these two data sets; this agreement is demonstrated by the observation that fitting individual data sets yields practically the same set of parameter values as by fitting the combined data sets from the three investigations. The dual-site Langmuir parameters for CH_4 , obtained by fitting all three data sets are reported in *Table S20*.

Bao et al.¹⁷ report the results of experimental isotherms for C_2H_4 , C_2H_6 , C_3H_6 and C_3H_8 in **MgMOF-74** at 278 K, 298 K, and 318 K. Our experimental isotherm data for C_2H_4 , and C_2H_6 are in excellent agreement with their data set; this agreement is demonstrated by the observation that fitting individual data sets yields practically the same set of parameter values as by fitting the combined data sets from the two investigations. The dual-site Langmuir-Freundlich fit parameters for C_2H_4 , C_2H_6 , C_3H_6 and C_3H_8 , obtained by fitting both sets of data are reported in *Table S20*.

CoMOF-74 isotherm data of Matzger et al.²⁰

Our experimental isotherm data for C_2H_4 and C_2H_6 at 296 K in **CoMOF-74** (= **CPO-27-Co** = $\text{Co}_2(\text{dobdc})$) are in good agreement with those presented in the US patent of Matzger et al.²⁰ (measured at 298 K); the fitted parameters reported in *Table S21* are obtained by fitting both data sets.

The Matzger patent²⁰ also presents pulse breakthrough experimental curves for $\text{C}_2\text{H}_4/\text{C}_2\text{H}_6$ and $\text{C}_3\text{H}_6/\text{C}_3\text{H}_8$ mixtures using **CoMOF-74**. Our breakthrough simulations for pulse inputs are compared with their breakthrough curves for experimental validation; here the parameters used are those reported in *Table S21*.

CuBTC for separation of mixtures containing propylene, and propane

For evaluation of the separation of $\text{C}_3\text{H}_6/\text{C}_3\text{H}_8$ mixtures we use the experimental isotherm data in the paper of Yoon et al.²¹, measured at temperatures of 303 K, 313 K, 323 K, 333 K, and 353 K. These experimental data were re-fitted with the set of parameters specified in *Table S23*.

Yoon et al.²¹ also report the results of breakthrough experiments that are used to validate our breakthrough simulation methodology; see below.

FeMIL-100

For comparison of the propylene/propane separation characteristics of **FeMIL-100**, experimental isotherm data at 303 K available in the paper by Yoon et al.²² were fitted with a single-site Langmuir-Freundlich isotherm model. It is noteworthy that the pure component experimental data are available up to pressures of 7 kPa. Extrapolation to 100 kPa is therefore not justified. The calculations presented here are only up to a total pressure of 20 kPa. The single-site Langmuir-Freundlich fit parameters for propylene and propane isotherms in **FeMIL-100** at 303 K are given in *Table S24*.

NaX zeolite

For evaluation of the ethylene/ethane separation characteristics of **NaX** zeolite, the experimental data of Hyun and Danner²³, determined at temperatures $T = 298$ K, and 323 K were fitted with a dual-site Langmuir-Freundlich isotherm model. The parameters are provided in *Table S25*.

For propylene and propane adsorption in **NaX** zeolite, the data provided in Table 4 of the paper by Lamia et al.²⁴ were used; the parameter fits for $T = 298$ K, and 318 K are specified in *Table S26*.

NaETS-10

For evaluation of the ethylene/ethane separation characteristics of **NaETS-10** zeolite, the experimental isotherm data reported by Anson et al.²⁵ were used. The parameter values are provided in *Table S27*.

ZIF-8

ZIF-8 has been suggested for ethylene/ethane and propylene/propane separations,²⁶⁻²⁸ but the performance of this material is based on diffusion effects, and not on the basis of adsorption strengths. We examine the separation performance of **ZIF-8** based on the data available in the literature sources.²⁶⁻²⁸

6. Packed bed adsorber breakthrough calculation methodology

It is now well recognized that the separation characteristics of a Pressure Swing Adsorption (PSA) unit is dictated by a *combination* of adsorption selectivity and uptake capacity.²⁹⁻³¹ For a rational choice of adsorbents for mixture separation, we need to have a proper method of evaluation that combines the selectivity and capacity metrics in a manner that is a true reflection of the separation performance of a PSA unit. For this purpose, we perform transient breakthrough calculations following the methodologies developed and described in earlier works.^{29, 32-34}

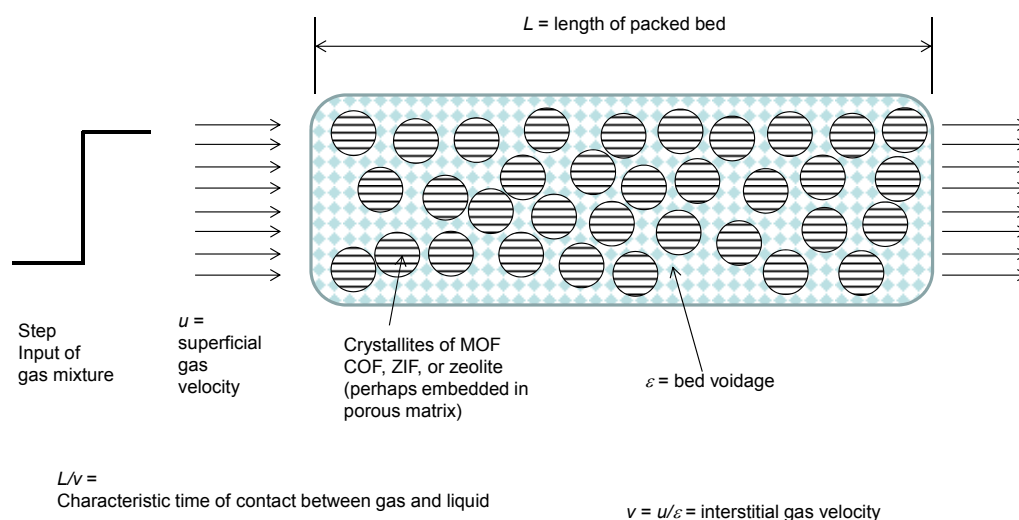


Figure S23. A schematic diagram of a packed bed adsorber.

Figure S23 shows a schematic of a packed bed adsorber bed of length L , packed with MOF, ZIF, COF, or zeolite crystals. Assuming plug flow of a n -component gas mixture through a fixed bed maintained under isothermal conditions, the partial pressures in the gas phase at any position and instant of time are obtained by solving the following set of partial differential equations for each of the species i in the gas mixture.^{33, 35-40}

$$\frac{1}{RT} \frac{\partial p_i(t, z)}{\partial t} = -\frac{1}{RT} \frac{\partial (v(t, z) p_i(t, z))}{\partial z} - \frac{(1 - \varepsilon)}{\varepsilon} \rho \frac{\partial \bar{q}_i(t, z)}{\partial t}; \quad i = 1, 2, \dots, n \quad (3)$$

In equation (3), t is the time, z is the distance along the adsorber, ρ is the framework density, ε is the bed voidage, v is the interstitial gas velocity, and \bar{q}_i is the *spatially averaged* molar loading within the crystallites of radius r_c :

$$\bar{q}_i(t, z) = \frac{3}{r_c^3} \int_0^{r_c} q_i(t, z) r^2 dr \quad (4)$$

Summing equation (4) over all n species in the mixture allows calculation of the *total average* molar loading of the mixture within the crystallite

$$\bar{q}_t(t, z) = \sum_{i=1}^n \bar{q}_i(t, z) \quad (5)$$

The *interstitial* gas velocity is related to the *superficial* gas velocity by

$$v = \frac{u}{\varepsilon} \quad (6)$$

Summing equation (3) over the n species present in the mixture, we obtain

$$\frac{1}{RT} p_i \frac{\partial(v(t,z))}{\partial z} = -\frac{(1-\varepsilon)}{\varepsilon} \rho \frac{\partial \bar{q}_i(t,z)}{\partial t} \quad (7)$$

where we have involved the assumption of negligible pressure drop, i.e.

$$\frac{\partial p_i}{\partial z} = 0 \quad (8)$$

The molar loadings at the *outer surface* of the crystallites, i.e. at $r = r_c$, are calculated on the basis of adsorption equilibrium with the bulk gas phase at partial pressures p_i at that position z and time t . The adsorption equilibrium can be calculated on the basis of the Ideal Adsorbed Solution Theory (IAST) of Myers and Prausnitz.⁴¹ In applying the IAST, it is necessary to have reliable fits of the pure component isotherm data over a wide range of pressures; for this purpose, the dual-site Langmuir-Freundlich isotherm (1) are suitable for all guest molecules considered in this study. Intra-crystallite diffusion limitations will result in radial gradients of molar loadings within each crystallite particle, and we need to quantify these gradients.

For convenience, a set of equations describing the fixed bed adsorber are summarized in *Figure S24*. *Figure S25* provides a summary of key assumptions made in the adsorber simulations. *Figure S26* provides a summary of key numerical aspects of adsorber simulations. *Figure S27* presents a schematic diagram showing adsorption equilibrium thermodynamics using IAST.

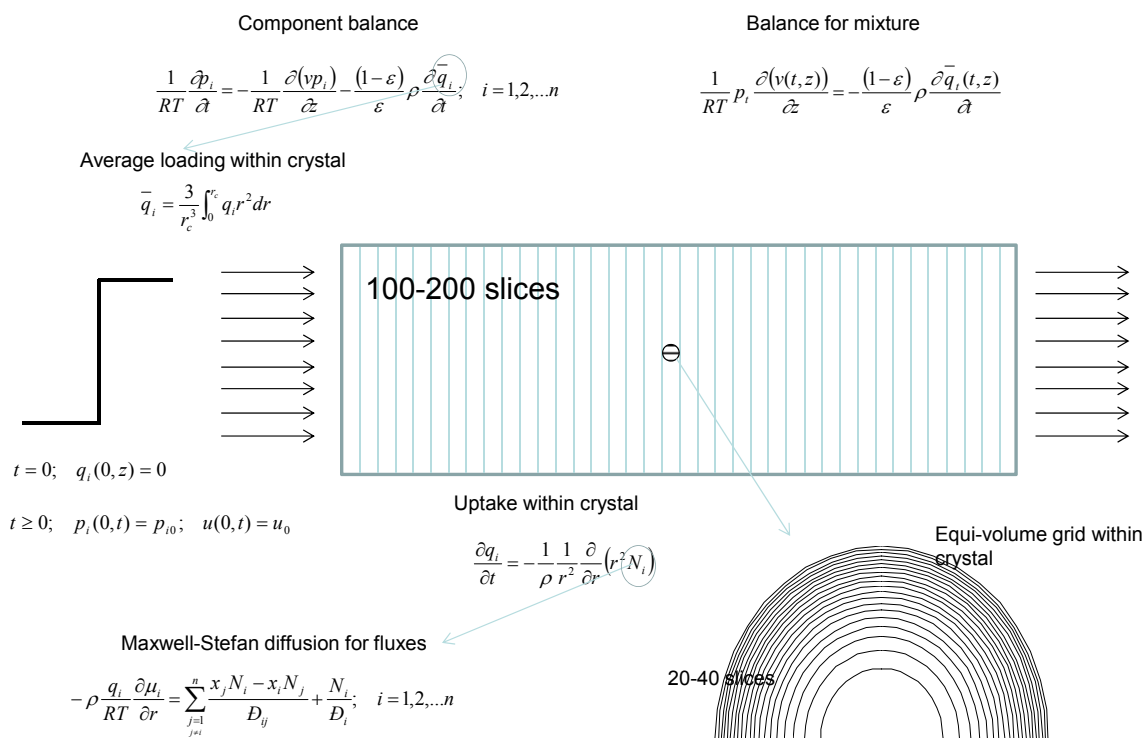


Figure S24. A summary of model equations describing a packed bed adsorber, along with discretization scheme.

- Negligible pressure drop, i.e. constant pressure
- Isothermal conditions, no heat effects
- Plug flow of gas mixture, i.e. no radial distribution of velocities and no axial dispersion
- At (t,z) , the outer surface of the MOF crystallite is in thermodynamic equilibrium with the surrounding gas mixture at the corresponding position
- Adsorption equilibrium determined by rigorous IAST calculations using dual-Langmuir-Freundlich fits of measured experimental isotherms
- Diffusion within the crystallite is described by rigorous Maxwell-Stefan diffusion model for mixtures, accounting for correlation effects using MD simulations for the degree of correlations

Figure S25. A summary of key assumptions made in the adsorber simulations.

- 100-200 slices in adsorber
- 20-50 equi-volume elements within crystal for uptake simulations
- Combination of discretized PDEs and algebraic IAST results in a set of differential algebraic equations (DAEs)
- DAEs solved using Runge-Kutta, along with efficient sparse matrix solver incorporating the Bulirsch-Stoer extrapolation
- The evaluation of the sparse Jacobian is by analytical expressions, making the computation times typically smaller than 200 s

Figure S26. A summary of key numerical aspects of adsorber simulations.

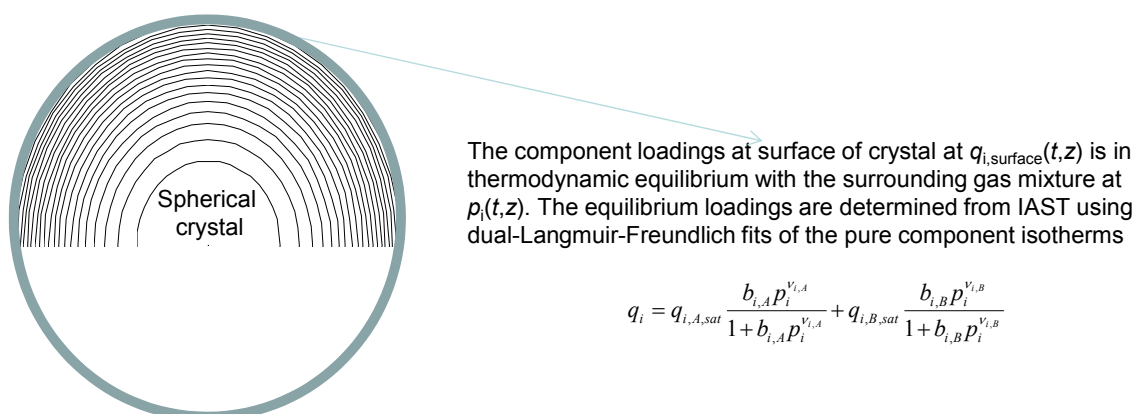


Figure S27. A schematic diagram showing adsorption equilibrium calculations using IAST.

Intra-crystalline diffusion and the Maxwell-Stefan equations

The radial distribution of molar loadings, q_i , within each crystallite is obtained from a solution of a set of differential equations describing the uptake within a crystallite:

$$\frac{\partial q_i}{\partial t} = -\frac{1}{\rho} \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 N_i) \quad (9)$$

The fluxes N_i , in turn, are related to the radial gradients in the chemical potentials, $\partial\mu_i/\partial r$, by the Maxwell-Stefan (M-S) formulation of intra-crystalline diffusion.^{33, 42-44}

$$-\rho \frac{q_i}{RT} \frac{\partial \mu_i}{\partial r} = \sum_{\substack{j=1 \\ j \neq i}}^n \frac{x_j N_i - x_i N_j}{D_{ij}} + \frac{N_i}{D_i}; \quad i = 1, 2, \dots, n \quad (10)$$

where the mole fractions of the adsorbed phase, x_i , are defined as

$$x_i = \frac{q_i}{q_1 + q_2 + \dots + q_n} = \frac{q_i}{q_t} \quad i = 1, 2, \dots, n \quad (11)$$

The D_i characterizes species i – wall interactions in the broadest sense. In many cases the D_i corresponds to the value of the pure component i ; consequently, this can be estimated from unary permeation data. In some cases where molecular clustering occurs, the D_i in the mixture can be lower than that of pure components.^{45, 46} The D_{ij} is exchange coefficient representing interaction between components i with component j . At the molecular level, the D_{ij} reflects how the facility for transport of species i correlates with that of species j . Conformity with the Onsager reciprocal relations prescribes

$$D_{ij} = D_{ji} \quad (12)$$

In the M-S formulation (10) the exchange coefficients D_{ij} account for slowing-down effects, that are of vital importance in mixture diffusion.⁴⁷

The chemical potential gradients in equation (10) can be related to the more conventional gradients of molar loadings by defining thermodynamic correction factors Γ_{ij}

$$\frac{q_i}{RT} \frac{\partial \mu_i}{\partial r} = \sum_{j=1}^n \Gamma_{ij} \frac{\partial q_j}{\partial r}; \quad \Gamma_{ij} = \frac{q_i}{p_i} \frac{\partial p_i}{\partial q_j}; \quad i, j = 1, 2, \dots, n \quad (13)$$

The elements of thermodynamic correction factors, Γ_{ij} , can be determined by differentiation of the dual-site Langmuir-Freundlich isotherm (1).

Figure S28 summarizes the Maxwell-Stefan diffusion equations used to describe intra-crystalline diffusion.

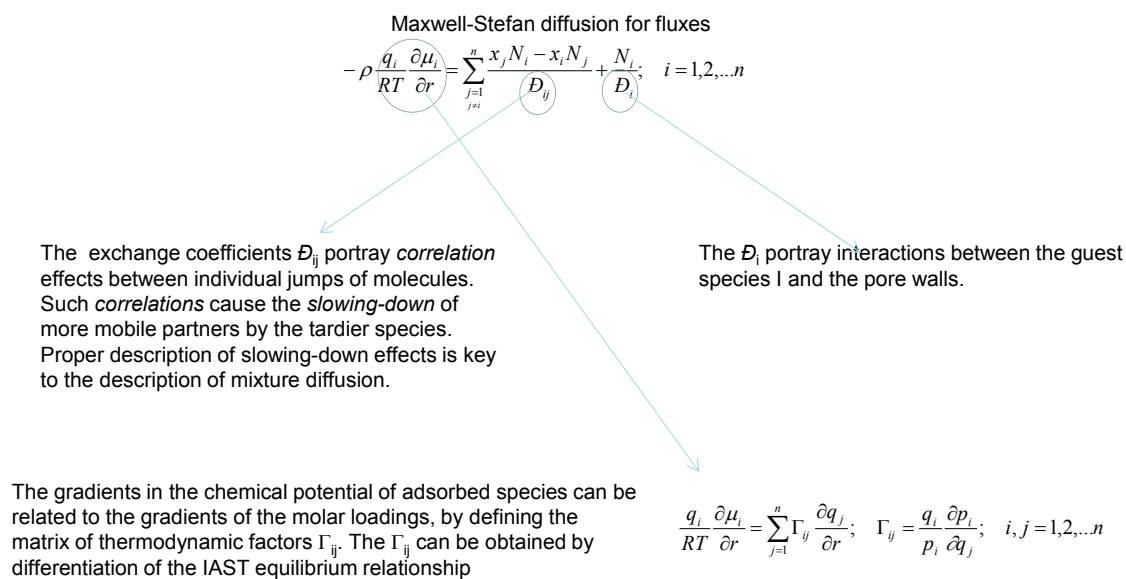


Figure S28. A schematic summary of the Maxwell-Stefan diffusion equations.

Fixed bed adsorber simulations with step inputs

In industrial practice, the most common operation is with to use a step-wise input of hydrocarbon mixtures to be separation into an adsorber bed that is initially free of adsorbates, i.e. we have the initial condition

$$t = 0; \quad q_i(0, z) = 0 \quad (11)$$

At time, $t = 0$, the inlet to the adsorber, $z = 0$, is subjected to a step input of the n -component gas mixture and this step input is maintained till the end of the adsorption cycle when steady-state conditions are reached.

$$t \geq 0; \quad p_i(0, t) = p_{i0}; \quad u(0, t) = u_0 \quad (12)$$

where u_0 is the superficial gas velocity at the inlet to the adsorber.

Figure S29a provides a schematic representation of the step input simulations. In all breakthrough calculations presented below, the following parameter values were used for all simulation data presented in this work: $L = 0.12$ m; $\varepsilon = 0.75$; $u = 0.00225$ m s⁻¹. It is to be noted that the actual values of these parameters have no bearing on the results for the production capacity presented later in this document. The simulation results for transient breakthrough are presented in our investigation in terms of a *dimensionless* time, τ , defined by dividing the actual time, t , by the characteristic time, $\frac{L\varepsilon}{u_0}$.

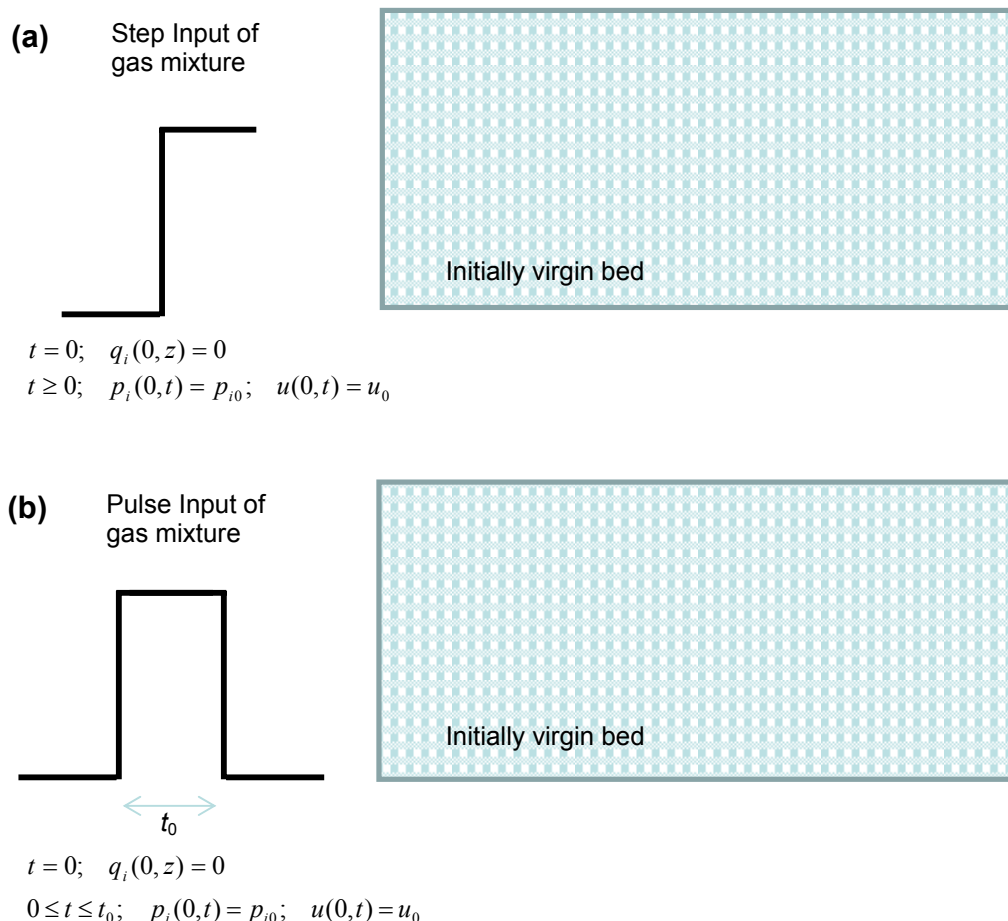


Figure S29. Two different types of breakthrough simulations. (a) step input of hydrocarbon mixtures to an initially virgin bed of adsorbent materials. (b) pulse chromatographic input of hydrocarbon mixtures.

Fixed bed adsorber simulations with pulse inputs

Besides the breakthrough simulations with a step-input (12), we also carried out simulations for a packed bed adsorber with injection of a short duration pulse of the mixture to be separated. This type of simulation is particularly useful to demonstrate the fractionating capability of adsorbents. In the US patent of Matzger et al.²⁰, pulse chromatographic experimental data are presented for **CoMOF-74** and **NiMOF-74** to demonstrate their potential for fractionation of ethylene/ethane and propylene/propane mixtures. For simulation of pulse chromatographic separations, we use the corresponding set of inlet conditions

$$0 \leq t \leq t_0; p_i(0, t) = p_{i0}; u(0, t) = u_0 \quad (13)$$

where the time for duration of the pulse is t_0 . These pulse chromatographic simulations have the advantage of making the “fractionating” capability of a specific MOF to become evident visually.

Figure S29b provides a schematic representation of the pulse input simulations. For the pulse chromatographic simulations, the following parameter values were used, as before, $L = 0.12$ m; $\varepsilon = 0.75$; $u = 0.00225$ m s⁻¹, together with a pulse duration $t_0 = 10$ s.

Discretization and numerical procedures

Equations (3) and (9) are first subjected to finite volume discretization. Typically, the adsorber length L is divided into 100 or more slices. Each crystallite, assumed to be spherical, is divided into 10-20 equi-volume slices. The number of slices in each case is determined by checking that the obtained breakthrough results do not change on increasing it. In the cases where strong diffusional limitations are present, the intra-particle gradients of concentrations are steep and about 20-40 equi-volume slices within each crystallite need to be taken into consideration. Combination of the discretized PDEs along with the algebraic IAST equilibrium model, results in a set of differential-algebraic equations (DAEs), which are solved using BESIRK.⁴⁸ BESIRK is a sparse matrix solver, based on the semi-implicit Runge-Kutta method originally developed by Michelsen,⁴⁹ and extended with the Bulirsch-Stoer extrapolation method.⁵⁰ Use of BESIRK improves the numerical solution efficiency in solving the set of DAEs. The evaluation of the sparse Jacobian required in the numerical algorithm is largely based on analytic expressions.³³ Further details of the adsorber model, along with the numerical procedures used in this work, are provided by Krishna and co-workers.^{33, 34, 51} Typical computation times for a binary gas mixture breakthrough are less than 500 s, allowing such transient adsorber calculations to be routinely used for screening purposes. For strong diffusional limitations, the computation times will increase due to increased number of intra-crystalline computational grids.

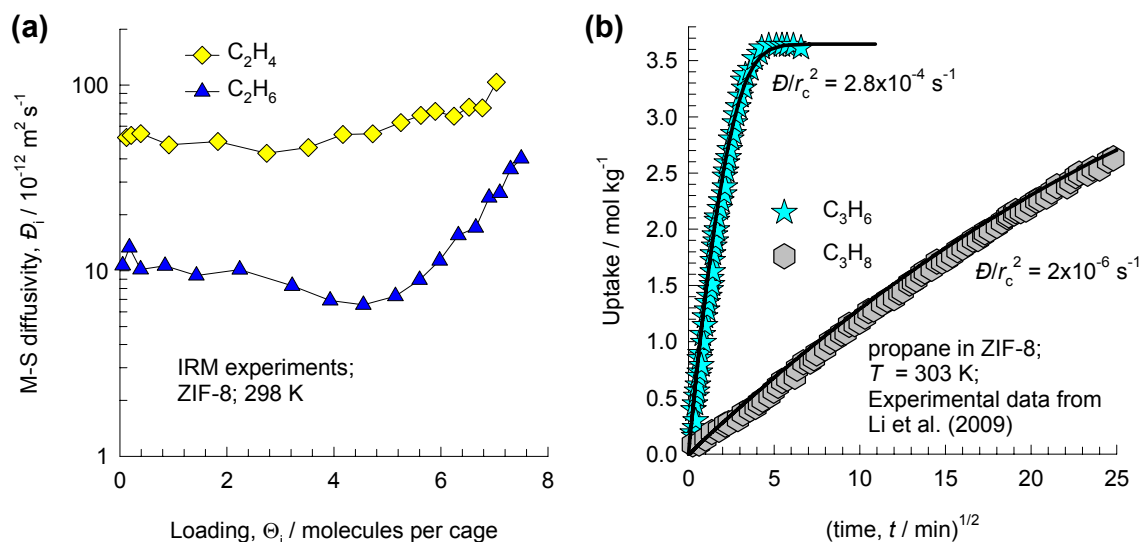


Figure S30. (a) Maxwell-Stefan diffusivities of C_2H_4 , and C_2H_6 in **ZIF-8** at 298 K, measured by Infra-Red Microscopy.^{26, 52-54} (b) Uptake of C_3H_6 , and C_3H_8 within **ZIF-8** crystallites, measured at 303 K by Li et al.²⁷ The continuous solid lines are obtained from numerical solution of (4) and (9) using the parameter values as indicated for propylene and propane. Note: for **ZIF-8**, a loading of 1 molecule per cage corresponds to 0.73 mol/kg.

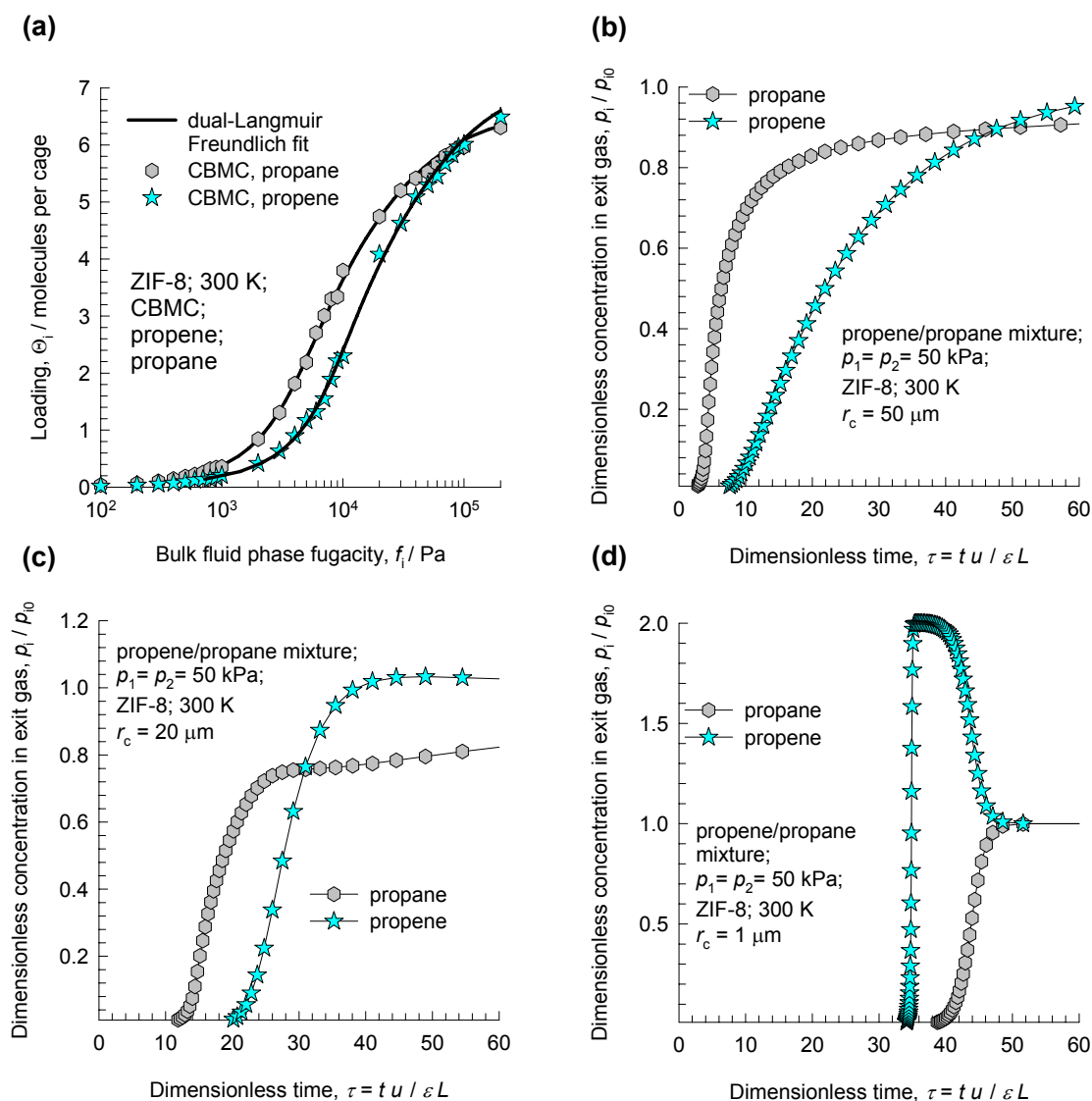


Figure S31. (a) Configurational-Bias Monte Carlo (CBMC) simulations⁵³ of the isotherms of C_3H_6 , and C_3H_8 in **ZIF-8** at 300 K. (b-d) Transient breakthrough simulations for *equimolar* mixtures of C_3H_6 , and C_3H_8 in packed bed adsorber operating at a total pressure of 100 kPa and 300 K, packed with **ZIF-8** crystallites with radii r_c of (b) $50 \mu\text{m}$, (c) $20 \mu\text{m}$, and (d) $1 \mu\text{m}$. In the breakthrough simulations the values of the M-S diffusivities for C_3H_6 , and C_3H_8 are taken to be $D_i = 5 \times 10^{-13} \text{ m}^2 \text{ s}^{-1}$, and $1 \times 10^{-14} \text{ m}^2 \text{ s}^{-1}$, respectively. The simulations are carried out assuming constant diffusivity values, and neglecting thermodynamic correction factors on the diffusivity values.

Influence of diffusivities, and crystallite sizes

For use in packed bed adsorbers, the crystallites of MOFs, or ZIFs, typically with radii r_c in the range $50 \mu\text{m} - 200 \mu\text{m}$ are embedded into a macro-porous supporting (binder) material before being packed into an adsorber. The larger the crystallite size, the greater the influence of diffusion on the breakthrough characteristics.

The inclusion of diffusional effects is essential for alkene/alkane separations that are primarily based on diffusional, also termed “kinetic”, selectivities. A good example of this is the separation of propylene and propane with **ZIF-8**. **ZIF-8** has the SOD zeolite topology and has cages separated by windows that are 3.26 Å in size. Small, subtle, differences in bond-lengths and bond angles cause the diffusivities of alkenes to be significantly lower than those of the corresponding alkanes. This is illustrated in the data of intra-crystalline diffusivities in **ZIF-8** obtained with Infra-Red Microscopy (IRM); see *Figure S30a*. The data show that the C₂H₄/C₂H₆ diffusion selectivity, in favor of C₂H₆, is in the range of 5 – 6, depending on the loading. Li et al.²⁷ report experimental data on uptake of C₃H₆, and C₃H₈ in **ZIF-8** crystals; see *Figure S30b*. We note that the uptake of C₃H₆ proceeds much faster than for C₃H₈. The combination of equations (4) and (9) allows the determination of the transient uptake of components within MOF crystallites to be calculated. The measured uptake curves could be matched by choosing the values of $\frac{D_i}{r_c^2} = 2.8 \times 10^{-4} \text{ s}^{-1}$, and $2 \times 10^{-6} \text{ s}^{-1}$, for C₃H₆ and C₃H₈, respectively. The diffusion selectivity value of 140 in the uptake experiments of Li et al.²⁷

The size of the crystallites that are embedded within the particles in the packed bed, has a significant bearing on the breakthrough characteristics of **ZIF-8**. In order to demonstrate the “kinetic” nature of the separation we carried out breakthrough simulations at 300 K, for a step-input of C₃H₆/C₃H₈ 50/50 gas mixtures at a total pressure of 100 kPa. The adsorption of C₃H₆ is poorer than that of C₃H₈ within **ZIF-8**; this is demonstrated by the Configurational-Bias Monte Carlo (CBMC) simulations⁵³ of the isotherms of C₃H₆, and C₃H₈ in **ZIF-8** at 300 K; the data is presented in *Figure S31a*. The dual-Langmuir Freundlich fits of the pure component isotherms were used, along with IAST calculations to determine the mixture adsorption equilibria. In the breakthrough simulations the values of the M-S diffusivities for C₃H₆, and C₃H₈ are taken to be $D_i = 5 \times 10^{-13} \text{ m}^2 \text{ s}^{-1}$, and $1 \times 10^{-14} \text{ m}^2 \text{ s}^{-1}$, respectively. The simulation results for an adsorber bed packed with **ZIF-8** crystallites of crystallite radii r_c of 50 μm, 20 μm, and 1 μm are shown in Figures 31b,c,d. For $r_c = 50 \text{ μm}$, the breakthrough of C₃H₈ occurs earlier because of the significantly lower diffusivity of the alkane. At the other extreme, for $r_c = 1 \text{ μm}$ the breakthrough of C₃H₆ occurs earlier because for this particle size the value of $\frac{D_i}{r_c^2}$ is large enough to ensure that intra-crystalline gradients are absent and the entire crystallite particle can be considered to be in thermodynamic equilibrium with the surrounding bulk gas phase at that time t , and position z of the adsorber

$$\bar{q}_i(t, z) = q_i(t, z) \quad (14)$$

The loadings $q_i(t, z)$ can be determined by application of the IAST for equilibrium with the bulk gas phase at the partial pressures $p_i(t, z)$.

For MOFs with more “open” structures such as **MgMOF-74**, **CoMOF-74**, **FeMOF-74**, **CuBTC** and also for **NaX** zeolite, the intra-crystalline diffusivities are about 1-3 orders of magnitude higher than for **ZIF-8**. For all such “open” structures, the influence of intra-crystalline diffusion is not of significant importance in determining the breakthroughs in fixed bed adsorbers. Equation (14) presents a good representation of the breakthrough characteristics of such “open” structures that emerge as promise candidates for separation of light hydrocarbons. We now validate this conclusion by comparison with available experimental data.

7. Validation of simulation methodology for transient breakthrough in fixed bed adsorbers

Before proceeding with using breakthrough simulations, invoking Equation (14) to investigate the separation characteristics of different MOFs, we seek validation of the suggested methodology with published experimental data.

Propylene/Propane breakthrough in CuBTC adsorber at 313 K

We consider the transient breakthrough characteristics of C_3H_6 , and C_3H_8 mixtures in a packed bed of **CuBTC** crystallites as reported in the experiments of Yoon et al.²¹ for a temperature of 313 K; see *Figure S32a*. The transient breakthrough characteristics are reasonably well represented by breakthrough simulations in which intra-crystalline diffusion effects are considered to be negligible and Equation (14) is invoked; witness the comparisons between experiments and simulations presented.

We now analyze in further detail the influence of intra-crystalline diffusion on the transient breakthrough characteristics with **CuBTC**. For this purpose, we need the values of the intra-crystalline diffusivities. Wehring et al.⁵⁵ report experimental data on self-diffusivities of C_3H_6 , and C_3H_8 within crystals of **CuBTC** in Table 2 of their paper. At a temperature of 313 K, the diffusivities for C_3H_6 , and C_3H_8 are calculated to be $D_i = 1.7 \times 10^{-11} \text{ m}^2 \text{ s}^{-1}$, and $2 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$, respectively. These values are about 2 orders of magnitude higher than the corresponding values for **ZIF-8**. It is also remarkable that the diffusivity value for C_3H_6 is lower than for C_3H_8 . The reason for this can be traced to the higher binding energy of C_3H_6 compared to that for C_3H_8 . The isosteric heats of adsorption, $-Q_{st}$, can be taken to a reflection of the binding energy. The values of the isosteric heats of adsorption, $-Q_{st}$, for C_3H_6 and C_3H_8 in **CuBTC** are 43 and 31 kJ mol^{-1} , respectively (see Table 2 of Wehring et al.⁵⁵).

In *Figure S32b* two scenarios for breakthrough simulation results are compared. The first scenario is the same as the one presented in *Figure 32a*, corresponding to equilibrium behaviors, without the influence of intra-crystalline diffusion. The second scenario is one in which the intra-crystalline

diffusion is accounted for in which the values of the M-S diffusivities for C_3H_6 , and C_3H_8 are taken to $D_i = 1.7 \times 10^{-11} \text{ m}^2 \text{ s}^{-1}$, and $2 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$, respectively. The crystallite radius r_c is assumed to be $400 \mu\text{m}$; this represents the largest crystallite size that is likely to be used in practice. The two sets of simulations yield virtually identical values for breakthrough times. Inclusion of intra-crystalline diffusion makes the breakthrough of propylene slightly more diffuse *after* breakthrough has occurred. The conclusion to be drawn here is that the assumption of thermodynamic equilibrium is a good one to make in practice, and invoking the assumption Equation (14) is sufficient to capture the separation performance of fixed bed adsorbers for hydrocarbons separations with MOFs that have “open” structures, i.e. with large pore volumes.

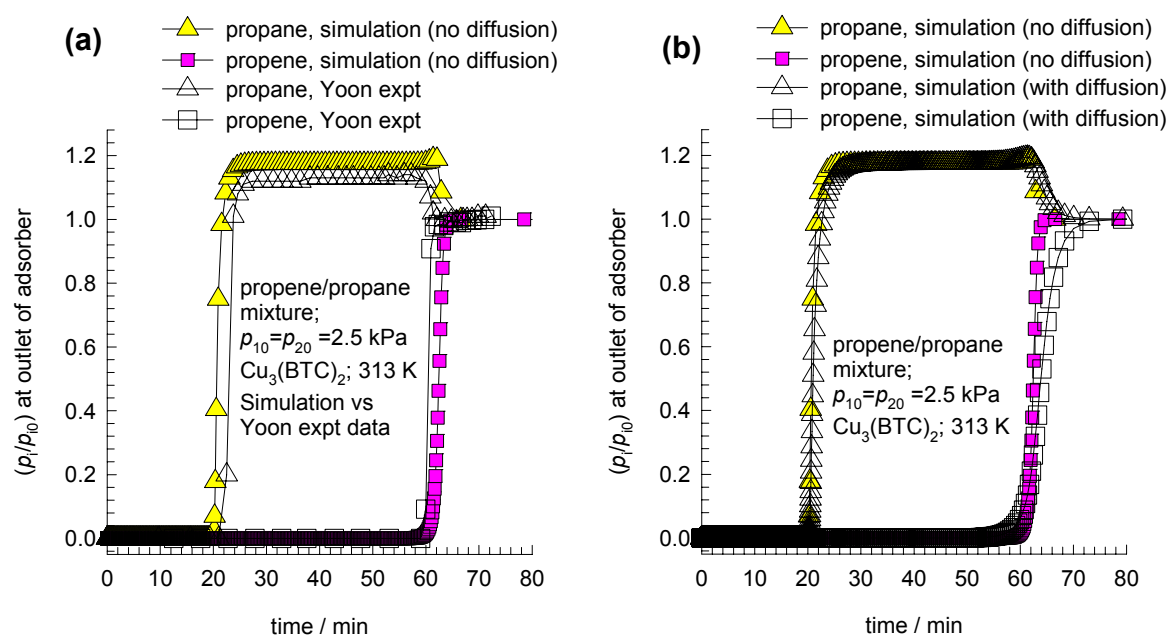


Figure S32. (a) Comparison of experimentally determined transient breakthrough for *equimolar* mixtures of C_3H_6 , and C_3H_8 in packed bed adsorber operating at a total pressure of 100 kPa and 313 K, packed with **CuBTC** crystallites with *equilibrium based* simulations. The experimental data and chosen conditions are those presented by Yoon et al.²¹ The inlet partial pressures of C_3H_6 , and C_3H_8 are 2.5 kPa each; the remainder of the gas is made up of helium. In the breakthrough simulations the intra-crystalline diffusion is considered to be negligible and the assumption specified by Equation (14) is invoked. (b) Here two scenarios for breakthrough simulation results are compared. The first scenario is the same as the one presented in (a), corresponding to equilibrium behaviors, without the influence of intra-crystalline diffusion. The second scenario is one in which the intra-crystalline diffusion is accounted for in which the values of the M-S diffusivities for C_3H_6 , and C_3H_8 are taken to $D_i = 1.7 \times 10^{-11} \text{ m}^2 \text{ s}^{-1}$, and $2 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$, respectively. The crystallite radius r_c is assumed to be $400 \mu\text{m}$. The simulations are carried out assuming constant diffusivity values, and neglecting thermodynamic correction factors on the diffusivity values.

Propylene/Propane breakthrough in FeMOF-74 adsorber at 318 K

In our investigations, **MgMOF-74**, **CoMOF-74**, and **FeMOF-74** emerge as the best materials for use in the wide variety of separations of light hydrocarbons. For any given guest molecule, the diffusivities

in each such structure will be nearly the same because the channel dimensions are virtually identical, corresponding to 1 nm. In the works of Bao et al.^{17, 18}, the diffusivities of uptake of a variety of guest molecules CO₂, CH₄, C₂H₄, C₂H₆, C₃H₆, and C₃H₈ in **MgMOF-74** were measured. As illustration, the transient uptake data for C₂H₄, C₂H₆, C₃H₆, and C₃H₈ in **MgMOF-74** at 298 K is shown in *Figure S33a*. In agreement with the data for **CuBTC** presented by Wehring et al.⁵⁵, the diffusivity of the alkenes, are found to be lower than those of the corresponding alkane with the same C number. For example, the values of $\frac{D_i}{r_c^2}$ for C₃H₆, and C₃H₈ are $\frac{D_i}{r_c^2} = 3.14 \times 10^{-3} \text{ s}^{-1}$, and $3.26 \times 10^{-3} \text{ s}^{-1}$, for C₃H₆ and C₃H₈, respectively. We note that the value for C₃H₈ is about 3 orders of magnitude higher than the corresponding value for ZIF-8 obtained in the uptake experiments of Li et al.²⁷ The rationale for the lower diffusivity of the alkene in **MgMOF-74**, as compared to the alkane, can be traced to the fact that the alkene has a stronger binding energy, and consequently the higher “sticking” tendency leads to a lower diffusivity, as deduced from MD simulations in MgMOF-74.^{51, 56} This explanation can be verified by plotting the values of $\frac{D_i}{r_c^2}$ as a function of the isosteric heats of adsorption, $-Q_{st}$, obtained in the limit of zero-loadings; see *Figure S33b*. The Q_{st} are those calculated in our work, and presented in *Figure 2* of the manuscript, in limit of zero-loading.

Breakthrough experiments were carried out by Bloch et al.¹⁶ in a 4 mm tube packed with **FeMOF-74** crystallites; details of the experimental set-up and conditions are provided in the Supplementary Material accompanying their publication. The experimental breakthrough curves are in good agreement with simulations in which intra-crystalline diffusional effects are ignored, and equation (14) is invoked. The simulated transient gas composition profiles are in good agreement with the experimentally determined ones in *Figure S34*; this provides validation of the simulation methodology in which intra-crystalline diffusion effects are considered to be negligible.

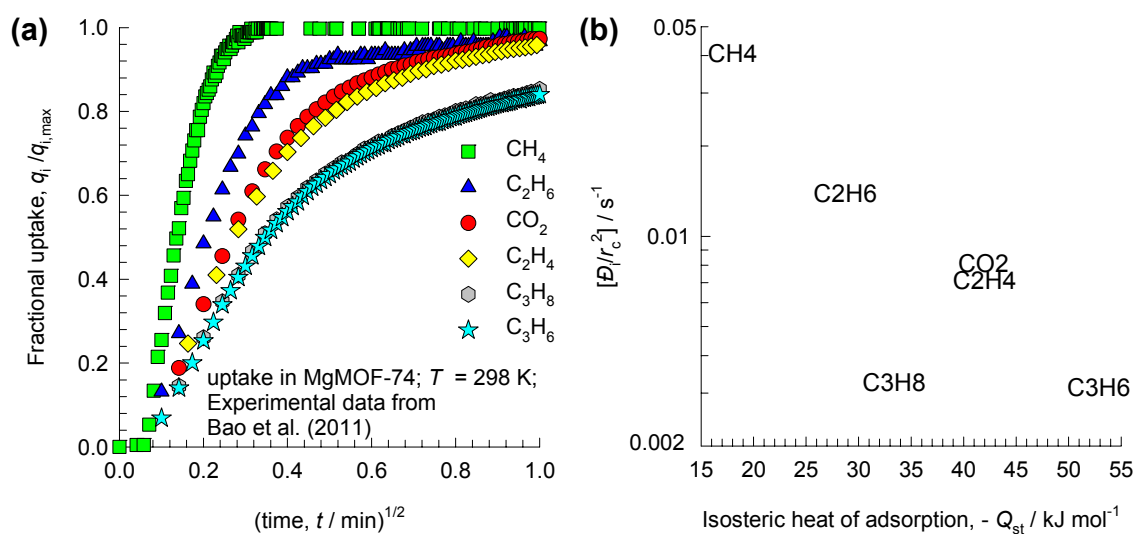


Figure S33. (a) Transient uptake of CH₄, CO₂, C₂H₄, C₂H₆, C₃H₆, and C₃H₈ in **MgMOF-74** at 298 K. The plotted data are from the experiments reported by Bao et al.^{17, 18} (b) The values of $\frac{D_i}{r_c^2}$ of a variety of guest molecules CO₂, CH₄, C₂H₄, C₂H₆, C₃H₆, and C₃H₈ in **MgMOF-74** plotted as a function of the isosteric heats of adsorption, Q_{st} . The data for $\frac{D_i}{r_c^2}$ are those reported in the works of Bao et al.^{17, 18} at a temperature of 298 K. The Q_{st} are those calculated in our work, and presented in *Figure 2* of the manuscript, in the limit of zero-loading. The Q_{st} data for CO₂ are obtained from the work of Mason et al.⁵⁷

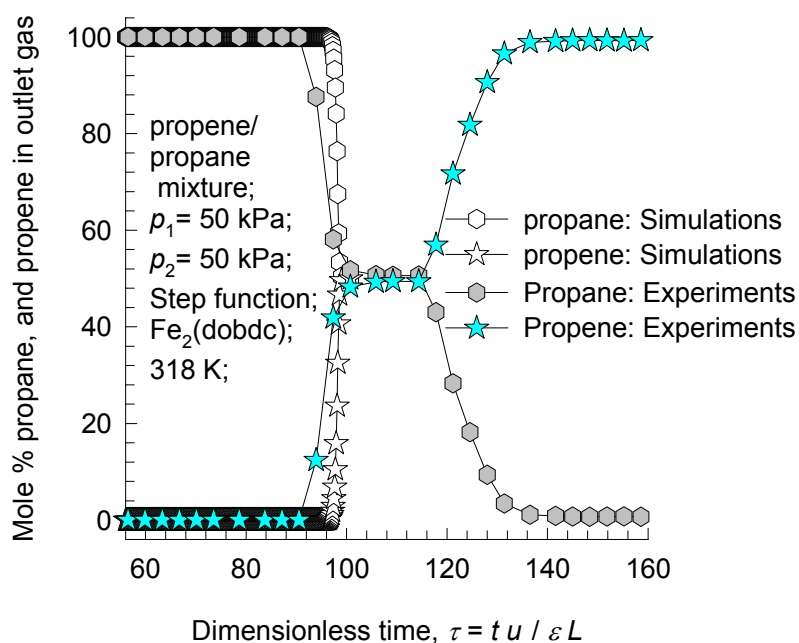


Figure S34. Comparison of experimentally determined transient breakthrough of an equimolar propylene/propane mixture in an adsorber bed packed with **FeMOF-74** at 318 K and a total pressure of 100 kPa with simulations in which the assumption specified by Equation (14) is invoked. Breakthrough experiments, reported by Bloch et al.¹⁶ were carried out in a 4 mm tube packed with 375 mg of **FeMOF-74** crystallites. The crystallites were packed within 120 mm of the tube length, i.e. $L = 0.12$ m. The x -axis is the dimensionless time, obtained by dividing the actual time by the characteristic contact time, $\frac{L\epsilon}{u_0}$.

Pulse chromatographic separations of alkene/alkane mixtures with **CoMOF-74**

The US patent awarded to Matzger et al.²⁰ presents pulse breakthrough experimental curves for separation of C_2H_4/C_2H_6 and C_3H_6/C_3H_8 mixtures in fixed beds packed with **CoMOF-74**; their data are reproduced in *Figure S35*.

These data clearly demonstrate the capability of **CoMOF-74** for fractionation of both mixtures. The corresponding pulse chromatographic simulations are shown in *Figure S36*. These simulations, using our isotherm data fits along with the assumption of negligible diffusional limitations is able to reproduce, albeit qualitatively, all the essential features of the pulse breakthroughs reported in the US patent.

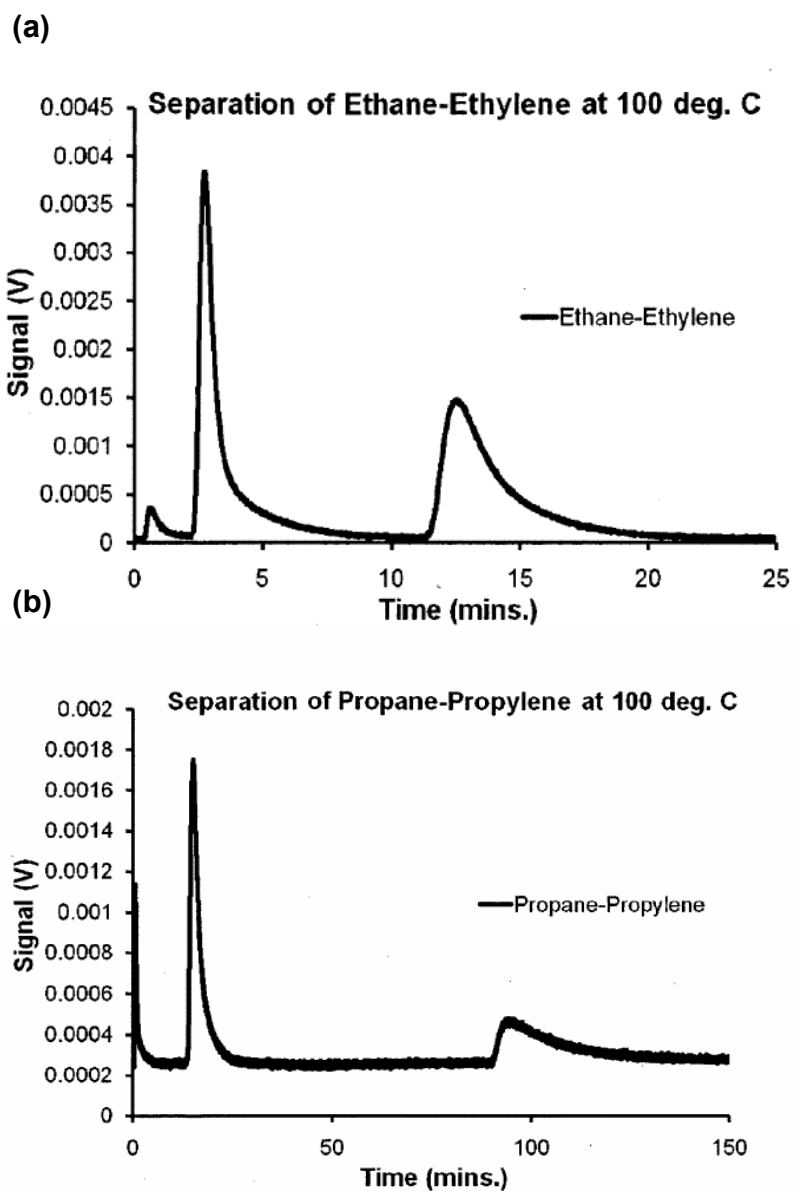


Figure S35. Pulse chromatographic experiments for (a) ethylene/ethane, and (b) propylene/propane separations as reported in the US patent awarded to Matzger et al.²⁰ The column is packed with CoMOF-74. No further details are provided in the patent.

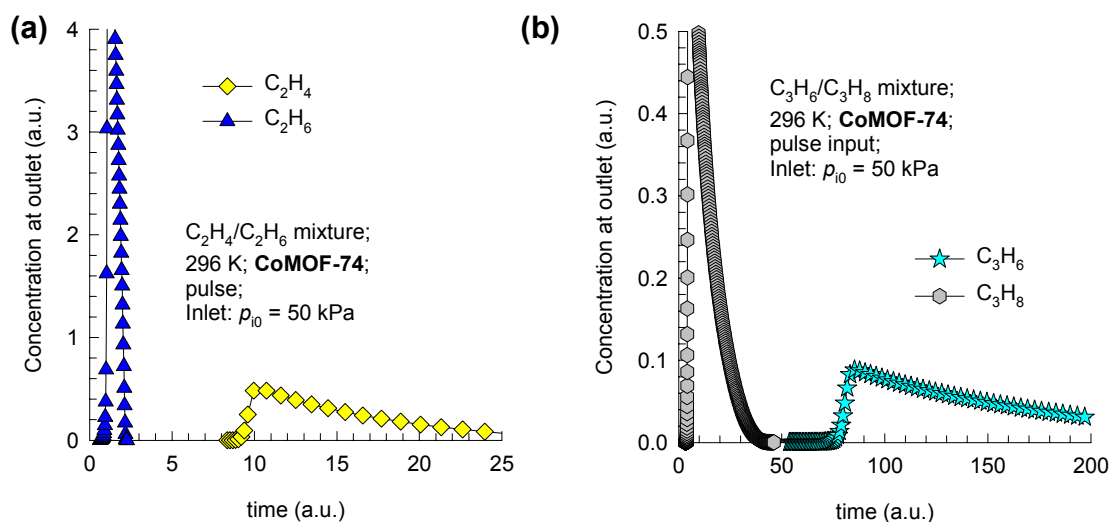


Figure S36. Pulse chromatographic simulations, neglecting intra-crystalline diffusion, for (a) ethylene/ethane and (b) propylene/propane separations with CoMOF-74. The inlet partial pressures in the pulse are taken to be 50 kPa each. Since the experimental details in the US patent awarded to Matzger et al.²⁰ are not provided, we have scaled the time scale to match the corresponding times shown in Figure S35.

8. Notation

b_A	dual-Langmuir-Freundlich constant for species i at adsorption site A, $\text{Pa}^{-\nu_i}$
b_B	dual-Langmuir-Freundlich constant for species i at adsorption site B, $\text{Pa}^{-\nu_i}$
D_i	Maxwell-Stefan diffusivity, $\text{m}^2 \text{s}^{-1}$
D_{ij}	M-S exchange coefficient, $\text{m}^2 \text{s}^{-1}$
L	length of packed bed adsorber, m
n	number of species in the mixture, dimensionless
N_i	molar flux of species i , $\text{mol m}^{-2} \text{s}^{-1}$
p_i	partial pressure of species i in mixture, Pa
p_{i0}	partial pressure of species i at inlet to fixed bed, Pa
p_t	total system pressure, Pa
q_i	component molar loading of species i , mol kg^{-1}
\bar{q}_i	<i>spatially averaged</i> component molar loading of species i , mol kg^{-1}
q_t	total molar loading in mixture, mol kg^{-1}
$q_{\text{sat},A}$	saturation loading of site A, mol kg^{-1}
$q_{\text{sat},B}$	saturation loading of site B, mol kg^{-1}
Q_{st}	isosteric heat of adsorption, J mol^{-1}
r	radial direction coordinate, m
r_c	radius of crystallite, m
R	gas constant, $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$
S_{ads}	adsorption selectivity, dimensionless
t	time, s

t_0	duration of pulse, s
T	absolute temperature, K
u	superficial gas velocity in packed bed, m s^{-1}
u_0	superficial gas velocity at inlet to packed bed, m s^{-1}
v	interstitial gas velocity in packed bed, m s^{-1}
x_i	mole fraction of species i in adsorbed phase, dimensionless
z	distance along the adsorber, m

Greek letters

ε	voidage of packed bed, dimensionless
Γ_{ij}	thermodynamic factors, dimensionless
ϕ	fractional pore volume, dimensionless
μ_i	molar chemical potential, J mol^{-1}
ν	exponent in dual-Langmuir-Freundlich isotherm, dimensionless
ρ	framework density, kg m^{-3}
τ	time, dimensionless
τ_{break}	breakthrough time, dimensionless

Subscripts

0	referring to conditions at inlet to adsorber
i	referring to component i
A	referring to site A
B	referring to site B
t	referring to total mixture

9. References

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Table S3. Dual-site Langmuir-Freundlich fit parameters for **CuBTC** (= **HKUST-1** = $\text{Cu}_3(\text{btc})_2$).

	Site A				Site B			
	$q_{A,\text{sat}}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,\text{sat}}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	5.4	1.29×10 ⁻¹¹	40	1	10.4	4.26×10 ⁻¹¹	29	1
C ₂ H ₄	5.1	1.38×10 ⁻¹¹	40	1	6.6	4.59×10 ⁻¹⁰	23.6	1
C ₂ H ₆	11.4	3.81×10 ⁻¹¹	31	1				
CH ₄	7.4	1.15×10 ⁻⁹	17.7	1				

Table S4. Dual-site Langmuir-Freundlich fit parameters for **MOF-505**.

	Site A				Site B			
	$q_{A,\text{sat}}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,\text{sat}}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	1.2	7.96×10 ⁻¹⁰	34.2	1	9.8	7.62×10 ⁻¹¹	29	1
C ₂ H ₄	0.64	3.35×10 ⁻¹²	48	1	7	1.34×10 ⁻¹⁰	29	1
C ₂ H ₆	7.1	1.02×10 ⁻¹⁰	31.5	1				
CH ₄	10.8	3.34×10 ⁻¹⁰	20	1				

Table S5. Dual-site Langmuir-Freundlich fit parameters for **PCN-16**.

	Site A				Site B			
	$q_{A,\text{sat}}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,\text{sat}}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	3.4	3.09×10 ⁻¹²	43.5	1	20.5	9×10 ⁻¹¹	25.5	1
C ₂ H ₄	2.8	1.82×10 ⁻¹¹	39.4	1	12.6	1.03×10 ⁻⁹	21.3	1
C ₂ H ₆	19.8	1.98×10 ⁻¹⁰	25	1				
CH ₄	31	5.03×10 ⁻¹⁰	15.5	1				

Table S6. Dual-site Langmuir-Freundlich fit parameters for **UMCM-150**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	2	2.97×10 ⁻¹²	42.6	1	16.7	1.72×10 ⁻¹⁰	24	1
C ₂ H ₄	1.4	1.37×10 ⁻¹²	44.6	1	12	2.86×10 ⁻¹⁰	24	1
C ₂ H ₆	24.6	1.28×10 ⁻¹⁰	24.4	1				
CH ₄	20.6	7.66×10 ⁻¹⁰	15	1				

Table S7. Dual-site Langmuir-Freundlich fit parameters for **NOTT-101**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	2	2.58×10 ⁻¹¹	38.3	1	21	1.58×10 ⁻¹⁰	25	1
C ₂ H ₄	2.3	5.43×10 ⁻¹²	41	1	14	2.95×10 ⁻¹⁰	24	1
C ₂ H ₆	32	2.37×10 ⁻⁹	17.5	1				
CH ₄	14	1.04×10 ⁻⁹	16	1				

Table S8. Dual-site Langmuir-Freundlich fit parameters for **NOTT-102**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	2.5	2.21×10 ⁻⁸	21	1	66	1.24×10 ⁻⁹	15.5	1
C ₂ H ₄	2.7	4.48×10 ⁻¹²	41	1	23	2.28×10 ⁻¹⁰	22	1
C ₂ H ₆	52	1.44×10 ⁻¹⁰	22.3	1				
CH ₄	9.7	1.29×10 ⁻⁹	16.2	1				

Table S9. Dual-site Langmuir-Freundlich fit parameters for **UTSA-20**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	2.1	2.26×10 ⁻¹¹	39.4	1	10	1.04×10 ⁻¹¹	33.6	1
C ₂ H ₄	0.28	5.39×10 ⁻¹¹	43.8	1	6.67	3.9×10 ⁻¹¹	33	1
C ₂ H ₆	8.1	4.46×10 ⁻¹¹	31	1				
CH ₄	6.1	2.08×10 ⁻¹⁰	21.7	1				

Table S10. Dual-site Langmuir-Freundlich fit parameters for **UTSA-33a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	4	1.8×10 ⁻¹¹	26	1	5	2.18×10 ⁻¹¹	34	1
C ₂ H ₄	3.7	7.2×10 ⁻¹¹	31	1	4.7	1.14×10 ⁻¹³	37	1
C ₂ H ₆	3.1	6.05×10 ⁻¹¹	33	1	1.6	1.19×10 ⁻¹²	35	1
CH ₄	3.3	1.01×10 ⁻¹⁰	20.5	1	3.3	3.64×10 ⁻¹⁰	20.5	1

Table S11. Dual-site Langmuir-Freundlich fit parameters for **UTSA-34a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	1.1	9.68×10 ⁻¹¹	33	1	4.4	2.03×10 ⁻¹¹	33	1
C ₂ H ₄	3.0	4.38×10 ⁻¹¹	33	1	1.6	4.44×10 ⁻¹²	33	1
C ₂ H ₆	2.2	1.18×10 ⁻¹⁰	33	1	1.4	2.2×10 ⁻¹¹	35	1
CH ₄	4.1	4.35×10 ⁻¹⁰	20.6	1				

Table S12. Dual-site Langmuir-Freundlich fit parameters for **UTSA-34b**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_i}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_i}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	8	2.48×10 ⁻¹¹	32	1	1.2	1.75×10 ⁻¹⁴	57	1
C ₂ H ₄	5	1.13×10 ⁻¹⁰	31	1	3.7	6.43×10 ⁻¹³	36	1
C ₂ H ₆	5.6	9.73×10 ⁻¹¹	31	1	0.74	1.33×10 ⁻¹²	36	1
CH ₄	6.8	3.96×10 ⁻¹⁰	20	1				

Table S13. Dual-site Langmuir-Freundlich fit parameters for **UTSA-35a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_i}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_i}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	5.05	9.7×10 ⁻¹¹	28	1	0.5	1.04×10 ⁻⁹	31	1
C ₂ H ₄	4	1.13×10 ⁻¹⁰	28	1	0.5	6.43×10 ⁻¹³	28	1
C ₂ H ₆	3.65	8.45×10 ⁻¹¹	30	1	0.1	9.02×10 ⁻¹⁰	30	1
CH ₄	4	1.12×10 ⁻⁹	17.2	1				
C ₃ H ₆	1.8	3.78×10 ⁻⁹	21.5	1	2.1	3.28×10 ⁻¹⁰	34	1
C ₃ H ₈	1.1	9.37×10 ⁻¹²	36	1	2.25	1.22×10 ⁻¹¹	42	1

Table S14. Dual-site Langmuir-Freundlich fit parameters for **M'MOF-2a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_i}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_i}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₂	1.8	7.18×10 ⁻⁹	19	1	0.8	1.02×10 ⁻¹⁰	36	1
C ₂ H ₄	1.35	2.03×10 ⁻⁹	21.7	1	0.5	1.55×10 ⁻¹⁰	33.4	1

Table S15. Dual-site Langmuir-Freundlich fit parameters for **M'MOF-3a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-ν_i}	E_A kJ mol ⁻¹	ν_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-ν_i}	E_B kJ mol ⁻¹	ν_B dimensionless
C ₂ H ₂	2.66	2.47×10 ⁻⁶	5	0.91	0.81	1.8×10 ⁻⁸	25	0.93
C ₂ H ₄	0.24	3.23×10 ⁻¹⁴	32	1.9	1.93	2.11×10 ⁻¹¹	32	0.825

Table S16. Dual-site Langmuir-Freundlich fit parameters for **M'MOF-4a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-ν_i}	E_A kJ mol ⁻¹	ν_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-ν_i}	E_B kJ mol ⁻¹	ν_B dimensionless
C ₂ H ₂	2.84	5.78×10 ⁻¹¹	28	1	0.32	1.15×10 ⁻¹⁰	36	1
C ₂ H ₄	0.27	2.71×10 ⁻¹²	39	1.2	9.7	5.85×10 ⁻¹³	37	0.81

Table S17. Dual-site Langmuir-Freundlich fit parameters for **M'MOF-5a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-ν_i}	E_A kJ mol ⁻¹	ν_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-ν_i}	E_B kJ mol ⁻¹	ν_B dimensionless
C ₂ H ₂	10.4	8.74×10 ⁻¹³	31	1	1.5	4.91×10 ⁻¹⁴	50	1
C ₂ H ₄	0.96	6.53×10 ⁻¹⁵	46.6	1.2				

Table S18. Dual-site Langmuir-Freundlich fit parameters for **M'MOF-6a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-ν_i}	E_A kJ mol ⁻¹	ν_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-ν_i}	E_B kJ mol ⁻¹	ν_B dimensionless
C ₂ H ₂	0.45	1.33×10 ⁻⁹	30	1	3.8	5.35×10 ⁻¹⁰	22.5	1
C ₂ H ₄	7	2.24×10 ⁻¹⁰	19	1	0.36	1.11×10 ⁻¹⁰	31.5	1

Table S19. Dual-site Langmuir-Freundlich fit parameters for **M'MOF-7a**.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-ν_i}	E_A kJ mol ⁻¹	ν_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-ν_i}	E_B kJ mol ⁻¹	ν_B dimensionless
C ₂ H ₂	2.4	1.02×10 ⁻¹⁵	49.6	1	0.8	1.07×10 ⁻¹³	47	1
C ₂ H ₄	3	6.83×10 ⁻⁸	5.9	1	0.01	1×10 ⁻⁹	7.6	1

Table S20. Dual-site Langmuir-Freundlich fit parameters for **MgMOF-74 (= CPO-27-Mg = Mg₂(dobdc))**.

Our experimental isotherm data for C₂H₄ and C₂H₆ are in excellent agreement with those presented in the paper by Bao et al.¹⁷ (measured at 278 K, 298 K, and 318 K); the fitted parameters reported below are obtained by combining *both* data sets. Our experimental isotherm data for CH₄ are in excellent agreement with those reported by Bao et al.¹⁸ (measured at 278 K, 298 K, and 318 K), and by Dietzel et al.¹⁹ (measured at 283 K, 298K, 313 K, and 343 K); the parameter values are obtained by fitting all *three* data sets. The parameters for C₃H₆ and C₃H₈ are obtained by re-fitting the experimental isotherms of Bao et al.¹⁷ (measured at 278 K, 298 K, and 318 K).

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-ν_i}	E_A kJ mol ⁻¹	ν_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-ν_i}	E_B kJ mol ⁻¹	ν_B dimensionless
C ₂ H ₂	6.3	4.62×10 ⁻¹¹	41	1	8.4	8.43×10 ⁻¹¹	26	1
C ₂ H ₄	3.1	2.15×10 ⁻¹²	28	1.3	6.4	2.11×10 ⁻¹²	45.2	1.07
C ₂ H ₆	8.4	3.28×10 ⁻¹²	34.5	1.2				
CH ₄	11	7.48×10 ⁻¹⁰	18.2	1	5	1.64×10 ⁻¹¹	18.2	1
C ₃ H ₆	7.1	6.32×10 ⁻¹³	55	1.04	1.7	2.17×10 ⁻¹⁴	40	1.44
C ₃ H ₈	1.9	2.22×10 ⁻¹¹	42	0.73	5.9	7.84×10 ⁻¹³	42	1.41

Table S21. Dual-site Langmuir-Freundlich fit parameters for **CoMOF-74** (= **CPO-27-Co** = $\text{Co}_2(\text{dobdc})$).

Our experimental isotherm data for C_2H_4 and C_2H_6 at 296 K are in good agreement with those presented in the papers by Bae et al.⁵⁸ (measured at 298 K), and reported in the US patent of Matzger et al.²⁰ (measured at 298 K); the fitted parameters reported below are obtained by all *three* data sets.

	Site A				Site B			
	$q_{\text{A,sat}}$ mol kg ⁻¹	$b_{\text{A}0}$ Pa ^{-ν_{A}}	E_{A} kJ mol ⁻¹	ν_{A} dimensionless	$q_{\text{B,sat}}$ mol kg ⁻¹	$b_{\text{B}0}$ Pa ^{-ν_{B}}	E_{B} kJ mol ⁻¹	ν_{B} dimensionless
C_2H_2	5.7	1.42×10^{-11}	45	1	9	2×10^{-10}	23.6	1
C_2H_4	5.2	5.23×10^{-10}	19.5	1	6.3	3.16×10^{-11}	41	1
C_2H_6	7.5	2.11×10^{-12}	37	1.2				
CH_4	7	3.74×10^{-11}	24.7	1	12.7	4.15×10^{-10}	17.8	1
C_3H_6	4.9	7.18×10^{-13}	54	1.16	2.3	3.55×10^{-13}	56	0.5
C_3H_8	1.3	3.27×10^{-14}	47	1	4.8	3.97×10^{-12}	47	1

Table S22. Dual-site Langmuir-Freundlich fit parameters for pure ethyne, ethylene, ethane, methane, propylene, and propane isotherms in **FeMOF-74** (= $\text{Fe}_2(\text{dobdc})$) obtained by re-fitting the experimental isotherms of Bloch et al.¹⁶ measured at 318 K, 333 K, and 353 K. These parameters are valid only within the temperature range of 318 K – 353 K; extrapolation to temperatures outside this range is not justified.

	Site A				Site B			
	$q_{\text{A,sat}}$ mol kg ⁻¹	$b_{\text{A}0}$ Pa ^{-ν_{A}}	E_{A} kJ mol ⁻¹	ν_{A} dimensionless	$q_{\text{B,sat}}$ mol kg ⁻¹	$b_{\text{B}0}$ Pa ^{-ν_{B}}	E_{B} kJ mol ⁻¹	ν_{B} dimensionless
C_2H_2	4.8	2.42×10^{-12}	51.4	1.1	3.2	2.07×10^{-10}	33.4	0.89
C_2H_4	1.74	6.51×10^{-12}	38	1.12	4.9	4.16×10^{-13}	53	1.12
C_2H_6	8.42	4.47×10^{-11}	31	1.1				
CH_4	6.7	8.06×10^{-10}	19.6	1				
C_3H_6	5.3	1.42×10^{-20}	97	1.76	1.7	1.29×10^{-10}	33	1.13
C_3H_8	2.1	5.95×10^{-12}	48	0.83	4.3	6.15×10^{-15}	53	1.63

Table S23. Dual-site Langmuir-Freundlich fit parameters for propylene and propane isotherms in **CuBTC** ($= \text{Cu}_3(\text{btc})_2$) using the simultaneous fits of the experimental isotherm data in the paper of Yoon et al.²¹, measured at temperatures of 303 K, 313 K, 323 K, 333 K, and 353 K.

	Site A				Site B			
	$q_{\text{A,sat}}$ mol kg ⁻¹	b_{A0} Pa ^{-v_{A}}	E_{A} kJ mol ⁻¹	v_{A} dimensionless	$q_{\text{B,sat}}$ mol kg ⁻¹	b_{B0} Pa ^{-v_{B}}	E_{B} kJ mol ⁻¹	v_{B} dimensionless
C ₃ H ₆	5.8	1.85×10^{-10}	37.3	0.95	3.25	3.64×10^{-14}	59	1.25
C ₃ H ₈	4.9	1.06×10^{-7}	25	0.62	4.0	1.45×10^{-22}	75	2.43

Table S24. Single-site Langmuir-Freundlich fit parameters for propylene and propane isotherms in **FeMIL-100** at 303 K. The parameter fits are based on fitting the data provided in Figure 2 of the paper by Yoon et al.²²

	$q_{\text{i,A,sat}}$ mol/kg	$b_{\text{i,A}}$ Pa ^{-$v_{\text{i,A}}$}	$v_{\text{i,A}}$ dimensionless
C ₃ H ₆	2.1	6.21×10^{-3}	0.64
C ₃ H ₈	7	1.53×10^{-5}	1

Table S25. Dual-site Langmuir fit parameters for pure ethylene and pure ethane isotherms in NaX zeolite using simultaneous fits the experimental data from Hyun and Danner²³ measured at 273 K, 298 K, and 323 K. The isotherm fits were used to determine the performance of NaX at a temperature of 296 K for comparison with different MOFs.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-v_A}	E_A kJ mol ⁻¹	v_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-v_B}	E_B kJ mol ⁻¹	v_B dimensionless
C ₂ H ₄	0.75	2.09×10 ⁻¹⁰	40	1	2.15	9.28×10 ⁻¹¹	35	1
C ₂ H ₆	2.95	3.07×10 ⁻¹⁰	28.7	1				

Table S26. Dual-site Langmuir fit parameters for propylene and propane isotherms in NaX zeolite at 298 K, and 318 K. The parameter fits are based on re-fitting the data provided in Table 4 of the paper by Lamia et al²⁴.

At 298 K, the parameters are:

	Site A			Site B		
	$q_{i,A,sat}$ mol/kg	$b_{i,A}$ Pa ^{-$v_{i,A}$}	$v_{i,A}$ dimensionless	$q_{i,B,sat}$ mol/kg	$b_{i,B}$ Pa ^{-$v_{i,B}$}	$v_{i,B}$ dimensionless
C ₃ H ₆	1.1	1.28×10 ⁻²	1	1.44	1.03×10 ⁻³	1
C ₃ H ₈	1.1	1.13×10 ⁻³	1	1.1	3.25×10 ⁻⁴	1

At 318 K, the parameters are:

	Site A			Site B		
	$q_{i,A,sat}$ mol/kg	$b_{i,A}$ Pa ^{-$v_{i,A}$}	$v_{i,A}$ dimensionless	$q_{i,B,sat}$ mol/kg	$b_{i,B}$ Pa ^{-$v_{i,B}$}	$v_{i,B}$ dimensionless
C ₃ H ₆	1.1	4.47×10 ⁻³	1	1.44	3.4×10 ⁻⁴	1
C ₃ H ₈	1.1	1.28×10 ⁻⁴	1	1.1	4.44×10 ⁻⁴	1

Table S27. Dual-site Langmuir-Freundlich fit parameters for pure ethylene and ethane isotherms in NaETS-10 zeolite, obtained by re-fitting the Toth isotherm parameters reported by Anson et al.²⁵ These parameters are valid only for 298 K; consequently, no E_A , and E_B parameter values are reported here.

	Site A				Site B			
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ^{-ν_i}	E_A kJ mol ⁻¹	ν_A dimensionless	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ^{-ν_i}	E_B kJ mol ⁻¹	ν_B dimensionless
C ₂ H ₄	0.68	5×10 ⁻²		0.75	1.1	1.0×10 ⁻²		0.6
C ₂ H ₆	1	1.94×10 ⁻³		0.72	0.44	9.96×10 ⁻³		0.85

Table S28. IAST and breakthrough calculations for separation of an equimolar CH₄/C₂H₂/C₂H₄/C₂H₆ mixture at 296 K.

MOFs	IAST calculations		Breakthrough calculations	
	C ₂ H ₆ /CH ₄ Adsorption selectivity	C ₂ H ₂ +C ₂ H ₄ + C ₂ H ₆ Uptake capacity mol L ⁻¹	Dimensionless time interval $\Delta\tau$	99%+ pure CH ₄ produced during $\Delta\tau$ mol L ⁻¹
CoMOF-74	7.77	7.73	74.10	2.13
MgMOF-74	11.61	6.48	49.30	1.70
CuBTC (=HKUST-1)	17.42	6.09	44.50	1.41
MOF-505	16.30	4.63	41.34	1.28
PCN-16	10.73	4.49	34.88	1.05
UMCM-150	9.24	2.83	18.39	0.60
NOTT-101	11.68	4.18	31.27	0.95
NOTT-102	5.81	2.69	9.34	0.31
UTSA-20	15.44	4.46	31.90	1.11
UTSA-33a	14.88	2.69	25.96	0.70
UTSA-34a	19.08	2.37	19.40	0.62
UTSA-34b	16.11	3.49	27.50	0.95
UTSA-35a	13.54	2.20	18.37	0.55

Table S29. IAST and breakthrough calculations for separation of an equimolar C₂H₄/C₂H₆ mixture at $p_1 = p_2 = 50$ kPa, and $T = 296$ K. The data for **FeMOF-74** are at 318 K.

MOFs	IAST calculations		Breakthrough calculations			
			Adsorption cycle: 99%+ pure ethane production		Desorption cycle: 99.5%+ pure ethene production	
	C ₂ H ₄ /C ₂ H ₆ Adsorption selectivity	C ₂ H ₄ Uptake capacity mol L ⁻¹	Dimensionless time interval $\Delta\tau_{\text{ads}}$	C ₂ H ₆ produced during $\Delta\tau_{\text{ads}}$ mol L ⁻¹	Dimensionless time interval $\Delta\tau_{\text{des}}$	C ₂ H ₄ produced during $\Delta\tau_{\text{des}}$ mol L ⁻¹
CoMOF-74	6.45	6.68	42.90	4.97	2379.00	4.47
MgMOF-74	5.63	5.41	35.50	3.97	1195.00	3.72
FeMOF-74	10.79	6.71	45.3	5.43	4506.00	4.98
CuBTC	3.63	4.76	29.63	2.97	525.31	2.60
PCN-16	2.77	0.22	16.04	1.46	255.50	1.32
NOTT-102	3.17	2.22	19.60	1.30	105.73	1.21
UTSA-20	1.96	2.95	10.85	1.06	299.42	0.86
NaX	8.01	3.37	25.03	2.71	1212.44	2.39
NaETS-10	14.78	2.99	22.30	2.42	2163.01	1.45

Table S30. IAST and breakthrough calculations for separation of an equimolar C₃H₆/C₃H₈ mixture at $p_1 = p_2 = 10$ kPa, and $T = 296$ K. The data for **FeMOF-74** is at 318 K. The data for **FeMIL-100** are at 303 K.

MOF	IAST calculations	Breakthrough calculations	
	C ₃ H ₆ /C ₃ H ₈ Adsorption selectivity	Adsorption cycle: 99%+ pure propane production; C ₃ H ₈ produced during $\Delta\tau_{\text{ads}}$ mol L ⁻¹	Desorption cycle: 99.5%+ pure propene production; C ₃ H ₆ produced during $\Delta\tau_{\text{des}}$ mol L ⁻¹
CoMOF-74	8.63	4.38	3.48
MgMOF-74	10.67	4.80	3.27
FeMOF-74	13.68	5.39	3.64
CuBTC	4.95	4.26	3.53
NaX	9.27	2.50	1.40
FeMIL-100	4.33	0.57	0.48

Table S31. IAST and breakthrough calculations for separation of C₂H₂/C₂H₄ mixture containing 1 mol% C₂H₂ at 296 K. The product gas stream contains less than 40 ppm C₂H₂.

MOFs	IAST calculations		Breakthrough calculations	
	C ₂ H ₂ /C ₂ H ₄ Adsorption selectivity	C ₂ H ₂ Uptake capacity mmol L ⁻¹	Dimensionless breakthrough time τ_{break}	C ₂ H ₄ produced during 0 - τ_{break} mmol L ⁻¹
CoMOF-74	1.62	129.84	74.40	89.66
MgMOF-74	2.23	148.44	85.65	103.33
MOF-505	1.45	68.39	40.05	48.00
UTSA-20	1.53	70.61	40.95	48.97
UTSA-33a	1.64	43.73	25.64	30.33
UTSA-34a	1.58	36.46	21.55	25.33
UTSA-34b	1.42	51.52	30.27	36.00
UTSA-35a	2.07	45.36	26.59	31.47
M'MOF-2a	3.12	38.15	22.52	26.53
M'MOF-3a	24.03	99.98	60.37	72.00
M'MOF-4a	14.31	72.23	41.86	50.00
M'MOF-5a	4.94	25.81	15.36	17.80
M'MOF-6a	7.42	48.52	28.95	34.33
M'MOF-7a	7.43	15.99	9.90	11.13