

Electronic Supplementary Information for:
**Dynamics and polarization of superparamagnetic chiral
nanomotors in a rotating magnetic field**

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I. Rotation matrix

We use the definition of the three Euler angles φ , θ and ψ following Ref. [1]. The components of any vector \mathbf{W} in the body-fixed coordinate system (BCS) and in the laboratory coordinate system (LCS) are determined from the relation $\mathbf{W}^{BCS} = \mathbf{R} \cdot \mathbf{W}$, where \mathbf{R} is the rotation matrix. The rotation matrix is expressed explicitly via the Euler angles [2]

$$\mathbf{R} = \begin{pmatrix} c_\varphi c_\psi - s_\varphi s_\psi c_\theta & s_\varphi c_\psi + c_\varphi s_\psi c_\theta & s_\psi s_\theta \\ -c_\varphi s_\psi - s_\varphi c_\psi c_\theta & -s_\varphi s_\psi + c_\varphi c_\psi c_\theta & c_\psi s_\theta \\ s_\varphi s_\theta & -c_\varphi s_\theta & c_\theta \end{pmatrix},$$

where we use the compact notation, $s_\psi = \sin \psi$, $c_\theta = \cos \theta$, etc.

II. Approximate rotational viscous resistance coefficients of a helix

We approximate the rotational viscous resistance coefficients of a helical propeller by the corresponding values for a prolate spheroid approximating the helix. Let a and b be, correspondingly, the longitudinal (along the symmetry axis) and transversal semi-axes of the spheroid. The respective viscous resistances due to rotation about the symmetry axis and in perpendicular direction read [3]

$$\kappa_{\parallel} = 2\eta V n_{\perp}^{-1}, \quad \kappa_{\perp} = 2\eta V \frac{a^2 + b^2}{a^2 n_{\parallel} + b^2 n_{\perp}}, \quad (\text{S1})$$

where η is the dynamic viscosity of the liquid, V is the spheroid volume, n_{\parallel} and $n_{\perp} = (1 - n_{\parallel})/2$ are the depolarizing factors of the spheroid. For the prolate spheroid with $a > b$ and eccentricity $e = \sqrt{1 - b^2/a^2}$ the depolarizing factor along the symmetry axis reads [4]

$$n_{\parallel} = \frac{1 - e^2}{e^3} \left(\frac{1}{2} \ln \frac{1 + e}{1 - e} - e \right). \quad (\text{S2})$$

III. Particle-based numerical algorithm

The numerical procedure used to compute the various components of the viscous resistance tensor is based on multipole expansion scheme [5]. The filament is constructed from nearly touching N rigid spheres (“shish-kebab” filament) having the same radius $r = 1$. The no-slip condition at the surface of all spheres is enforced rigorously via the use of direct

transformation between solid spherical harmonics centered at origins of different spheres. The method yields a system of $\mathcal{O}(N\mathcal{L}^2)$ linear equations for the expansion coefficients and the accuracy of calculations is controlled by the number of spherical harmonics (i.e. truncation level), \mathcal{L} , retained in the series. This approach has been applied before for modeling low-Reynolds-number swimmers, e.g., rotating helix [6, 7] and undulating filament [8].

The spheres composing the helical filament are partitioned along the backbone of the filament $\mathbf{X}(s)$ (see Eq. (21) and Fig. S1) so that the distance between centers of neighboring spheres is set to $2.02r$. The motion of the i th sphere composing a helix can be decomposed into translation \mathbf{U}_i and rotation $\boldsymbol{\omega}_i$ about its center, as $\mathbf{V}_i = \mathbf{U}_i + \boldsymbol{\omega}_i \times \mathbf{r}_i$ with \mathbf{r}_i being the radius vector with origin at the center of i th sphere. For any prescribed rigid-body-motion of the helix, $\{\mathbf{U}_i, \boldsymbol{\omega}_i\}$ are determined uniquely. For instance, for computing the components of the resistance tensor, such as $\xi_{\parallel}, \kappa_{\parallel}$ and \mathcal{B}_{\parallel} , associated with translation U and rotation ω about the x_3 -axis, one has $\boldsymbol{\omega}_i = \mathbf{e}_3 \omega$ and $\mathbf{U}_i = U \mathbf{e}_3 + \omega \mathbf{e}_3 \times \mathbf{R}_i$, where \mathbf{R}_i is a position vector to the i th sphere center.

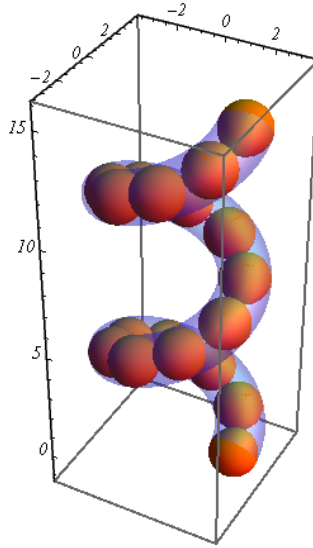


FIG. S1. Illustration of particle-based “shish-kebab” 2-turn helix approximating the regular helix with circular cross section of radius $r = 1$ (transparent blue) with helical radius $R = 2.5$ and pitch angle $\Theta = 65^\circ$.

IV. Demagnetizing factors of infinitely long elliptic cylinder

The demagnetizing factor N of infinitely long cylinder with an elliptic cross-section with corresponding semi-axes \hat{a} and \hat{b} was reported in Ref. [9]:

$$N = (2\pi)^{-1} \left[4 \arctan \frac{\hat{a}}{\hat{b}} + \frac{2\hat{b}}{\hat{a}} \ln \frac{\hat{b}}{\hat{a}} + \left(\frac{\hat{a}}{\hat{b}} - \frac{\hat{b}}{\hat{a}} \right) \ln \left(1 + \frac{\hat{b}^2}{\hat{a}^2} \right) \right].$$

At $\hat{a} > \hat{b}$ it determines the demagnetization factor N_1 along the short axis. The demagnetizing factor N_2 can be found either by the permutation $\hat{a} \leftrightarrow \hat{b}$ or from the equality $N_1 + N_2 = 1$. For the regular helix with circular cross-section $N_1 = N_2 = 1/2$.

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